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*Supplement of*

## **From mapped faults to fault-length earthquake magnitude (FLEM): a test on Italy with methodological implications**

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## 1 Additional supporting information (Files uploaded separately)

Dataset-S1-ItalianFaults.kmz

Dataset-S2-Selected\_ITHACA\_faults.txt

Dataset-S3-Selected\_GNTD\_faults.txt

5 Dataset-S4-Selected\_StructuralModel\_faults.txt

Dataset-S5-Selected\_GeologicMap\_faults.txt

Dataset-S6-Selected\_literature\_faults.txt

## 2 Additional supporting figures

FigureS1

10 FigureS2

FigureS3

## 3 Additional supporting figures

TableS1

TableS2

## 15 4 Introduction

**Dataset-S1-ItalianFaults.kmz.** Compressed file (to be opened in Google Earth) containing georeferenced traces from the fault datasets belonging to the collection utilized for this work (see the main text). It is composed by eight layers classified according to colors utilized in Fig. 2 in the main text, i.e.: blue (ITHACA dataset), red (GNDT dataset), pink (faults selected from literature), dark grey (Structural Model of Italy dataset). Each dataset is also classified by the class of confidence (A or B) adopted for calculations and again described in the main text.

**Dataset-S2-Selected\_ITHACA\_faults.txt.** ASCII file containing polylines coordinates (longitude, latitude) at nodes of only those faults selected for calculation from the ITHACA dataset. Each single fault is delimited by the symbol ">" as header.

25 **Dataset-S3-Selected\_GNTD\_faults.txt.** ASCII file containing polylines coordinates (longitude, latitude) at nodes of only those faults selected for calculation from the GNDT dataset. Each single fault is delimited by the symbol ">" as header.

**Dataset-S4-Selected\_StructuralModel\_faults.txt.** ASCII file containing polylines coordinates (longitude, latitude) at nodes of only those fault sselected for calculation from the Structural Model of Italy dataset. Each single fault is delimited by the symbol ">" as header.

**Dataset-S5-Selected\_GeologicMap\_faults.txt.** ASCII file containing polylines coordinates (longitude, latitude) at nodes of only those faults selected for calculation from the Geologic Map of Italy dataset. Each single fault is delimited by the symbol ">" as header.

35 **Dataset-S6-Selected\_literature\_faults.txt.** ASCII file containing polylines coordinates (longitude, latitude) at nodes of only those faults selected for calculation from the literature. Each single fault is delimited by the symbol ">" as header.

**Tables S1 and S2.** Tables containing results of statistical tests of FLEM values on the CSIV1.1 (Table S1) and ISIDe (Table S2) databases. The listed cells (column 1) have a FLEM value (column 2) larger than the related historical/instrumental catalogued

magnitude and pass the Goodness of Fit Test (Wiemer and Wyss, 2000), at 95% confidence level, for the Gutenberg-Richter model, with a b-value equal to 1, and a completeness magnitude  $M_c$  (column 4). The variable N (column 5) marks the number of events in each cell above  $M_c$ . Two tests are done, assuming as null hypothesis a double truncated (DTGR), with FLEM as the maximum magnitude, and an unbounded (UGR) Gutenberg-Richter laws. For both distributions, we keep only cells (marked in boldface) passing the Log-likelihood (LL) test, at 95% confidence level (see text for details). The related p-values ( $p_{LL}$ ) are reported in columns 6 and 9, for DTGR e UGR distributions, respectively. The LL test is passed if  $p_{LL} > 0.05$ . Finally, we apply, on remaining cells, the test proposed by Holschneider et al. (2014), rejecting a FLEM value if the maximum observed magnitude (column 4),  $m_{max}$  is larger than a suitable threshold. This last is computed both on all N events ( $Mt1$ , columns 8 and 10) and, if possible, for events in the last two degrees of magnitudes ( $Mt2$ , column 9 and 11).

## 5 Figures captions

**FigureS1.** Maps (central Italy) of the calculated Fault-Length Earthquake Magnitude (FLEM), for each cell, from the length of class A faults. Black lines are the longest A class faults in each cell. FLEM values are obtained from these faults using L10. Grey filling is used for cells with no data. (a) Grid with square cells 12.5 km in size. (b) Grid with square cells 25 km in size. (c) Grid with square cells 50 km in size.

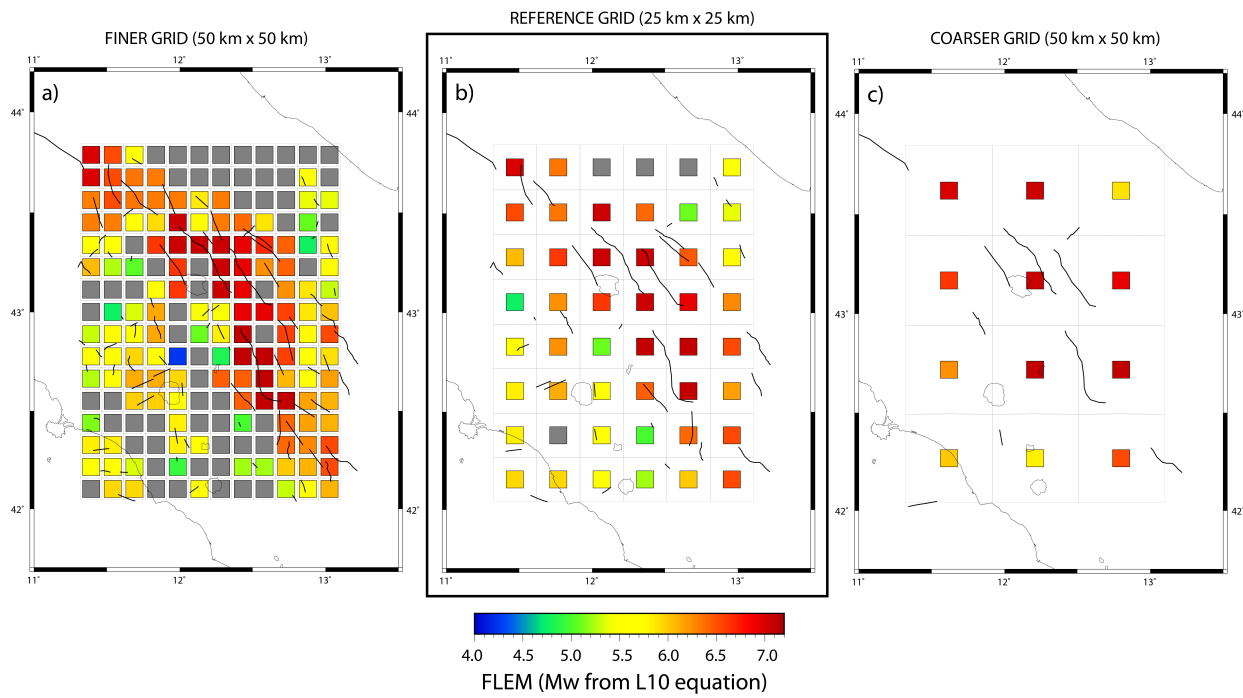
**FigureS2.** Maps (central Italy) of the difference between FLEM values (only from class A faults) and maximum magnitudes from historic or instrumental earthquakes. Black lines are the longest A class faults in each cell. FLEM values are obtained from these faults using L10. Grey filling is used for cells with no data. (a) Grid with square cells 12.5 km in size. (b) Grid with square cells 25 km in size. (c) Grid with square cells 50 km in size.

**FigureS3.** a) FLEM vs. cell diagram referring to FLEMs from cells in Fig. S1. On the abscissas, all cells from NW to SE are aligned. On the ordinates, the corresponding FLEM values are reported. Orange, red, and black colours are for FLEMs from the grids with 12.5, 25, and 50 km sized cells, respectively (Fig. S1). (b) FLEM minus FLEM diagram referring to FLEMs from cells in Fig. S1. Orange line represents, cell by cell, the FLEM from the 50 km grid ( $FLEM_{50km}$ ) minus the FLEM from the 25 km grid ( $FLEM_{25km}$ ). Red line represents, cell by cell, the FLEM from the 12.5 km grid ( $FLEM_{12.5km}$ ) minus the FLEM from the 25 km grid ( $FLEM_{25km}$ ). Black line line represents, cell by cell, the FLEM from the 25 km grid ( $FLEM_{25km}$ ) minus the FLEM from the 25 km grid ( $FLEM_{25km}$ ). The latter one is obviously equal to 0.

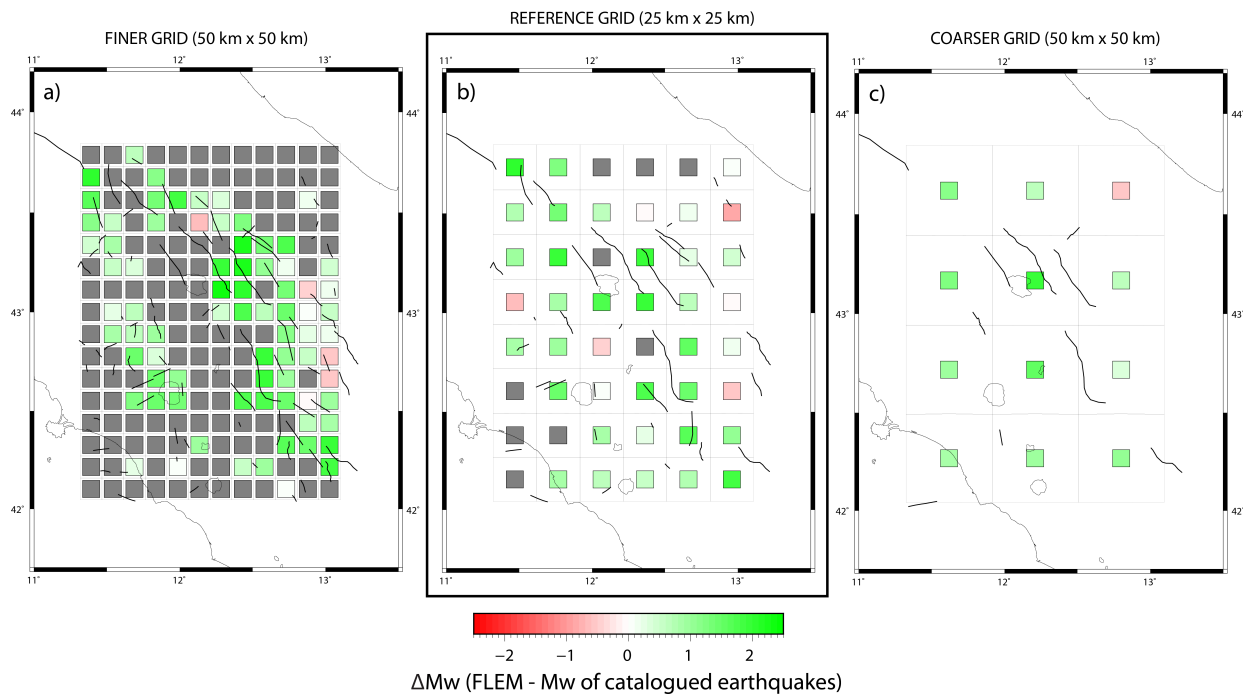
## 6 Table captions

**TableS1.** Test of FLEM values on the CSIV1.1 database.

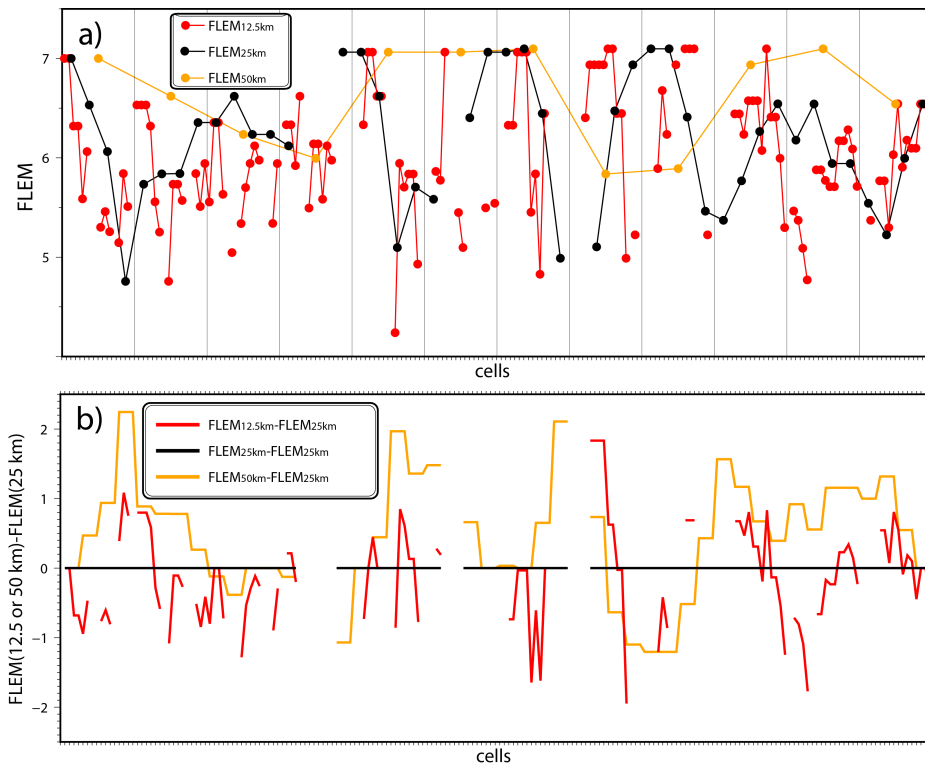
**TableS2.** Test of FLEM values on the ISIDE database.



**FigureS1.**



**FigureS2.**



FigureS3.

CSIv1.1

ID cell	FLEM	Mc	oMmax	N	DTGR			UGR		
					pLL	Mt1	Mt2	pLL	Mt1	Mt2
<b>E13</b>	<b>5.9</b>	<b>2.0</b>	<b>3.4</b>	<b>68</b>	<b>0.0562</b>	<b>5.1</b>		<b>0.0533</b>	<b>5.1</b>	
M13	7.1	1.9	3.0	49	0.0166			0.0160		
N12	7.1	1.9	3.7	72	0.0032			0.0029		
<b>Q14</b>	<b>6.4</b>	<b>1.7</b>	<b>3.5</b>	<b>173</b>	<b>0.0728</b>	<b>5.2</b>		<b>0.0817</b>	<b>5.2</b>	
<b>Q17</b>	<b>5.7</b>	<b>1.8</b>	<b>2.4</b>	<b>24</b>	<b>0.3962</b>	<b>4.4</b>		<b>0.3922</b>	<b>4.5</b>	
Q19	6.1	1.8	3.5	37	0.0002			0.0007		
<b>T15</b>	<b>6.8</b>	<b>2.1</b>	<b>3.7</b>	<b>71</b>	<b>0.0897</b>	<b>5.2</b>		<b>0.0946</b>	<b>5.2</b>	
U14	7.4	2.5	4.4	153	0.0456			0.0480		
<b>U17</b>	<b>7.1</b>	<b>1.7</b>	<b>4.4</b>	<b>216</b>	<b>0.1401</b>	<b>5.3</b>	<b>5.2</b>	<b>0.1392</b>	<b>5.3</b>	<b>5.2</b>
<b>W18</b>	<b>6.5</b>	<b>1.6</b>	<b>5.3</b>	<b>793</b>	<b>1.0000</b>	<b>5.7</b>	<b>5.6</b>	<b>1.0000</b>	<b>5.8</b>	<b>5.7</b>
<b>W19</b>	<b>6.9</b>	<b>1.6</b>	<b>4.3</b>	<b>825</b>	<b>1.0000</b>	<b>5.8</b>	<b>5.7</b>	<b>1.0000</b>	<b>5.8</b>	<b>5.7</b>
<b>W20</b>	<b>7.1</b>	<b>1.6</b>	<b>4.5</b>	<b>569</b>	<b>0.2190</b>	<b>5.6</b>	<b>5.7</b>	<b>0.2126</b>	<b>5.6</b>	<b>5.7</b>
<b>W22</b>	<b>6.4</b>	<b>1.7</b>	<b>3.7</b>	<b>81</b>	<b>0.0768</b>	<b>4.9</b>	<b>4.8</b>	<b>0.0758</b>	<b>4.9</b>	<b>4.8</b>
<b>W24</b>	<b>5.7</b>	<b>1.9</b>	<b>3.7</b>	<b>50</b>	<b>0.0693</b>	<b>4.8</b>		<b>0.0678</b>	<b>4.9</b>	
X18	6.4	1.6	3.0	100	0.0336			0.0392		
X20	6.5	1.7	5.5	1310	0.0400			0.0430		
X39	7.2	2.3	4.1	50	0.0016			0.0008		
Y16	7.8	1.8	3.2	32	0.0044			0.0041		
<b>Y19</b>	<b>6.2</b>	<b>1.6</b>	<b>3.8</b>	<b>200</b>	<b>0.0553</b>	<b>5.2</b>	<b>5.2</b>	<b>0.0506</b>	<b>5.2</b>	<b>5.2</b>
<b>Y20</b>	<b>6.5</b>	<b>1.6</b>	<b>3.8</b>	<b>243</b>	<b>0.9991</b>	<b>5.3</b>	<b>5.2</b>	<b>0.9982</b>	<b>5.3</b>	<b>5.2</b>
Y21	6.3	2.1	4.1	74	0.0017			0.0023		
AA18	7.7	1.7	5.0	106	0.0410			0.0010		
<b>AA25</b>	<b>6.8</b>	<b>2.1</b>	<b>3.1</b>	<b>59</b>	<b>0.6361</b>	<b>5.2</b>		<b>0.6335</b>	<b>5.2</b>	
<b>AB42</b>	<b>6.8</b>	<b>2.2</b>	<b>4.2</b>	<b>179</b>	<b>0.4082</b>	<b>5.7</b>		<b>0.4137</b>	<b>5.7</b>	
AD26	5.7	1.5	4.2	366	0.0036			0.0032		
<b>AD42</b>	<b>5.8</b>	<b>2.2</b>	<b>4.2</b>	<b>181</b>	<b>0.0793</b>	<b>5.5</b>		<b>0.0713</b>	<b>5.7</b>	
<b>AD43</b>	<b>5.4</b>	<b>2.3</b>	<b>4.4</b>	<b>147</b>	<b>0.4897</b>	<b>5.2</b>	<b>5.2</b>	<b>0.4927</b>	<b>5.8</b>	<b>5.6</b>
<b>AE43</b>	<b>6.8</b>	<b>2.3</b>	<b>4.8</b>	<b>&lt;10-45</b>	<b>0.9740</b>	<b>6.4</b>	<b>6.4</b>	<b>0.9761</b>	<b>6.6</b>	<b>6.7</b>
<b>AH32</b>	<b>6.4</b>	<b>1.9</b>	<b>5.6</b>	<b>400</b>	<b>0.4233</b>	<b>5.7</b>	<b>5.5</b>	<b>0.4274</b>	<b>5.8</b>	<b>5.6</b>
<b>AH33</b>	<b>6.4</b>	<b>1.9</b>	<b>3.7</b>	<b>270</b>	<b>0.8254</b>	<b>5.6</b>		<b>0.8311</b>	<b>5.6</b>	

TableS1.

ISIDe

ID cell	FLEM	Mc	oMmax	N	DTGR			UGR		
					pLL	Mt1	Mt2	pLL	Mt1	Mt2
C13	7.2	1.1	4.7	491	0.0075			0.0062		
<b>E12</b>	<b>6.5</b>	<b>1.6</b>	<b>3.8</b>	<b>180</b>	<b>0.2486</b>	<b>5.1</b>	<b>5.1</b>	<b>0.2424</b>	<b>5.1</b>	<b>5.1</b>
E13	5.9	1.8	3.9	180	0.0310			0.0275		
L12	7.1	2	4	105	0.0011			0.0006		
<b>N14</b>	<b>6.2</b>	<b>1.6</b>	<b>4</b>	<b>114</b>	<b>0.2100</b>	<b>4.9</b>	<b>4.9</b>	<b>0.2064</b>	<b>4.9</b>	<b>5.0</b>
<b>O14</b>	<b>6.6</b>	<b>1.3</b>	<b>5.2</b>	<b>1588</b>	<b>0.8986</b>	<b>5.7</b>	<b>5.7</b>	<b>0.9029</b>	<b>5.8</b>	<b>5.8</b>
P7	6.8	1.2	4	96	0.0010			0.0040		
P13	6.6	2.1	4	46	0.0030			0.0042		
<b>P14</b>	<b>6.6</b>	<b>1.5</b>	<b>4.8</b>	<b>547</b>	<b>0.9369</b>	<b>5.5</b>	<b>5.4</b>	<b>0.9346</b>	<b>5.5</b>	<b>5.4</b>
Q11	7.4	2.2	5.3	468	0.0428			0.0455		
<b>Q14</b>	<b>6.4</b>	<b>1.7</b>	<b>3.7</b>	<b>681</b>	<b>0.9992</b>	<b>5.7</b>	<b>5.6</b>	<b>0.9994</b>	<b>5.8</b>	<b>5.7</b>
<b>R11</b>	<b>7.7</b>	<b>2.2</b>	<b>5.9</b>	<b>1187</b>	<b>0.8261</b>	<b>6.5</b>	<b>6.5</b>	<b>0.8249</b>	<b>6.6</b>	<b>6.5</b>
<b>R14</b>	<b>6.6</b>	<b>1.8</b>	<b>4.1</b>	<b>325</b>	<b>0.8453</b>	<b>5.6</b>	<b>5.5</b>	<b>0.8491</b>	<b>5.6</b>	<b>5.6</b>
R16	7	1.7	3.6	79	0.0208			0.0192		
R17	6.2	1.6	4.1	441	0.0064			0.006		
<b>R20</b>	<b>5.7</b>	<b>1.4</b>	<b>2.4</b>	<b>65</b>	<b>0.5513</b>	<b>4.5</b>		<b>0.5594</b>	<b>4.5</b>	
<b>T15</b>	<b>6.8</b>	<b>1.4</b>	<b>4.1</b>	<b>581</b>	<b>0.1350</b>	<b>5.4</b>	<b>5.4</b>	<b>0.1385</b>	<b>5.5</b>	<b>5.4</b>
<b>T20</b>	<b>5.9</b>	<b>1.5</b>	<b>3.4</b>	<b>112</b>	<b>0.9065</b>	<b>4.8</b>		<b>0.9084</b>	<b>4.8</b>	
<b>U15</b>	<b>6.5</b>	<b>1.2</b>	<b>3.9</b>	<b>1082</b>	<b>0.9800</b>	<b>5.5</b>	<b>5.4</b>	<b>0.9822</b>	<b>5.5</b>	<b>5.5</b>
<b>U16</b>	<b>6.8</b>	<b>1.2</b>	<b>3.9</b>	<b>1058</b>	<b>0.9596</b>	<b>5.5</b>	<b>5.5</b>	<b>0.9647</b>	<b>5.5</b>	<b>5.5</b>
<b>U17</b>	<b>7.1</b>	<b>1.4</b>	<b>3.6</b>	<b>134</b>	<b>0.3868</b>	<b>4.8</b>	<b>4.8</b>	<b>0.3847</b>	<b>4.8</b>	<b>4.8</b>
U21	5.9	1.4	4.1	128	0.0036			0.0038		
<b>V16</b>	<b>6.2</b>	<b>1.2</b>	<b>3.8</b>	<b>391</b>	<b>0.3503</b>	<b>5.1</b>	<b>5.0</b>	<b>0.3493</b>	<b>5.1</b>	<b>5.0</b>
<b>V18</b>	<b>7.1</b>	<b>1</b>	<b>3.5</b>	<b>1106</b>	<b>1.0000</b>	<b>5.3</b>	<b>5.2</b>	<b>1.0000</b>	<b>5.3</b>	<b>5.2</b>
<b>W17</b>	<b>6.5</b>	<b>1.3</b>	<b>2.9</b>	<b>1013</b>	<b>1.0000</b>	<b>5.5</b>		<b>1.0000</b>	<b>5.6</b>	
<b>W18</b>	<b>6.5</b>	<b>1.1</b>	<b>4</b>	<b>5431</b>	<b>1.0000</b>	<b>6</b>	<b>5.8</b>	<b>1.0000</b>	<b>6.1</b>	<b>5.9</b>
<b>W19</b>	<b>6.9</b>	<b>1.3</b>	<b>3.3</b>	<b>639</b>	<b>1.0000</b>	<b>5.4</b>		<b>1.0000</b>	<b>5.4</b>	
<b>W20</b>	<b>7.1</b>	<b>1.4</b>	<b>4.2</b>	<b>1343</b>	<b>0.9997</b>	<b>5.8</b>	<b>5.7</b>	<b>0.9996</b>	<b>5.8</b>	<b>5.7</b>
<b>W21</b>	<b>7.1</b>	<b>1.7</b>	<b>3.6</b>	<b>246</b>	<b>0.9683</b>	<b>5.4</b>		<b>0.9706</b>	<b>5.4</b>	
W22	6.4	1.4	3.8	194	0.0394			0.0407		
<b>X20</b>	<b>6.5</b>	<b>1.4</b>	<b>4.6</b>	<b>6218</b>	<b>1.0000</b>	<b>6.2</b>	<b>6.2</b>	<b>1.0000</b>	<b>6.5</b>	<b>6.5</b>
<b>X22</b>	<b>6.5</b>	<b>1.6</b>	<b>3.9</b>	<b>223</b>	<b>0.7886</b>	<b>5.2</b>	<b>5.2</b>	<b>0.7935</b>	<b>5.2</b>	<b>5.2</b>
<b>X23</b>	<b>6.5</b>	<b>1.4</b>	<b>3</b>	<b>200</b>	<b>1.0000</b>	<b>5</b>		<b>1.0000</b>	<b>5.0</b>	
X25	5.7	1.5	3	45	0.0071			0.0061		
Y5	7.3	1.1	3.2	55	0.0014			0.0014		
Y17	7.5	0.9	3.3	408	0.0020			0.0011		
<b>Y19</b>	<b>6.2</b>	<b>1.5</b>	<b>4.7</b>	<b>2796</b>	<b>0.9946</b>	<b>5.9</b>	<b>5.9</b>	<b>0.9946</b>	<b>6.2</b>	<b>6.3</b>
<b>Y20</b>	<b>6.5</b>	<b>1.5</b>	<b>6.1</b>	<b>15544</b>	<b>1.0000</b>	<b>6.4</b>	<b>6.3</b>	<b>1.0000</b>	<b>7.0</b>	<b>6.8</b>
<b>Y21</b>	<b>6.3</b>	<b>1.4</b>	<b>6</b>	<b>13868</b>	<b>1.0000</b>	<b>6.2</b>	<b>6.2</b>	<b>1.0000</b>	<b>6.8</b>	<b>6.8</b>
<b>Y24</b>	<b>6.4</b>	<b>1.8</b>	<b>3.2</b>	<b>69</b>	<b>0.1894</b>	<b>4.9</b>		<b>0.1831</b>	<b>4.9</b>	
<b>Z21</b>	<b>6.5</b>	<b>1.9</b>	<b>3.4</b>	<b>151</b>	<b>0.8860</b>	<b>5.3</b>		<b>0.8916</b>	<b>5.4</b>	



<b>Z23</b>	<b>6.1</b>	<b>1.5</b>	<b>4.2</b>	<b>1676</b>	<b>0.9994</b>	<b>5.8</b>	<b>5.7</b>	<b>0.9992</b>	<b>6.0</b>	<b>6.0</b>
Z25	6.5	1.2	4.7	368	0.0041			0.0042		
<b>AA24</b>	<b>6.4</b>	<b>1.6</b>	<b>3.5</b>	<b>139</b>	<b>0.7212</b>	<b>5.0</b>		<b>0.7192</b>	<b>5.0</b>	
<b>AB24</b>	<b>6.2</b>	<b>1.5</b>	<b>3.8</b>	<b>208</b>	<b>0.2761</b>	<b>5.1</b>	<b>5.0</b>	<b>0.2895</b>	<b>5.1</b>	<b>5.1</b>
<b>AB25</b>	<b>6.8</b>	<b>1.7</b>	<b>3.2</b>	<b>252</b>	<b>0.9449</b>	<b>5.4</b>		<b>0.943</b>	<b>5.4</b>	
<b>AD26</b>	<b>5.7</b>	<b>1.6</b>	<b>4.1</b>	<b>275</b>	<b>0.4015</b>	<b>5.2</b>	<b>5.2</b>	<b>0.4015</b>	<b>5.3</b>	<b>5.3</b>
<b>AD39</b>	<b>7</b>	<b>2.7</b>	<b>4.3</b>	<b>69</b>	<b>0.2315</b>	<b>5.8</b>		<b>0.2331</b>	<b>5.8</b>	
AD42	5.8	1.9	4.3	121	0.0018			0.0026		
<b>AD43</b>	<b>5.4</b>	<b>2.1</b>	<b>3.5</b>	<b>76</b>	<b>0.2330</b>	<b>5.0</b>		<b>0.2323</b>	<b>5.3</b>	
<b>AE29</b>	<b>6.1</b>	<b>1.6</b>	<b>3.7</b>	<b>79</b>	<b>0.2077</b>	<b>4.8</b>	<b>4.6</b>	<b>0.2138</b>	<b>4.8</b>	<b>4.7</b>
<b>AE41</b>	<b>7.1</b>	<b>1.9</b>	<b>4.2</b>	<b>423</b>	<b>0.8959</b>	<b>5.8</b>	<b>5.8</b>	<b>0.8926</b>	<b>5.8</b>	<b>5.8</b>
<b>AE42</b>	<b>6.1</b>	<b>3.1</b>	<b>4.4</b>	<b>49</b>	<b>0.0884</b>	<b>5.8</b>		<b>0.0843</b>	<b>6.1</b>	
AE46	6.4	1.7	3.9	151	0.0073			0.0070		
AF31	6.6	1.2	2.9	64	0.0011			0.0015		
<b>AF39</b>	<b>6.1</b>	<b>2.4</b>	<b>4.5</b>	<b>128</b>	<b>0.9810</b>	<b>5.6</b>	<b>5.6</b>	<b>0.9806</b>	<b>5.8</b>	<b>5.7</b>
<b>AF41</b>	<b>7</b>	<b>1.8</b>	<b>4.1</b>	<b>68</b>	<b>0.0739</b>	<b>4.9</b>	<b>4.9</b>	<b>0.0800</b>	<b>4.9</b>	<b>4.9</b>
<b>AG31</b>	<b>6.7</b>	<b>1.1</b>	<b>3.8</b>	<b>176</b>	<b>0.1366</b>	<b>4.6</b>	<b>4.6</b>	<b>0.1400</b>	<b>4.6</b>	<b>4.6</b>
AG32	6.7	1.3	3.7	142	0.0020			0.002		
<b>AH32</b>	<b>6.4</b>	<b>1.1</b>	<b>3.7</b>	<b>428</b>	<b>0.2253</b>	<b>5.0</b>	<b>4.9</b>	<b>0.221</b>	<b>5.0</b>	<b>4.9</b>
<b>AH33</b>	<b>6.4</b>	<b>1.3</b>	<b>5</b>	<b>2645</b>	<b>1.0000</b>	<b>5.9</b>	<b>5.8</b>	<b>1.0000</b>	<b>6.0</b>	<b>5.9</b>
AH39	6.7	1.6	3.6	94	0.0385			0.0375		
<b>AI33</b>	<b>6.4</b>	<b>1.3</b>	<b>4.3</b>	<b>767</b>	<b>0.3373</b>	<b>5.4</b>	<b>5.4</b>	<b>0.3247</b>	<b>5.5</b>	<b>5.5</b>
AI35	6.8	1.4	3.7	120	0.0153			0.0188		
<b>AJ29</b>	<b>6.1</b>	<b>1.6</b>	<b>3.1</b>	<b>74</b>	<b>0.2705</b>	<b>4.7</b>	<b>4.7</b>	<b>0.2662</b>	<b>4.8</b>	<b>4.8</b>
AJ35	5.9	1.9	3.4	57	0.0017			0.0019		
<b>AJ37</b>	<b>6.8</b>	<b>1.9</b>	<b>3.4</b>	<b>81</b>	<b>0.0499</b>			<b>0.0542</b>	<b>5.1</b>	

TableS2.