



Supplement of

Distribution, microphysical properties, and tectonic controls of deformation bands in the Miocene subduction wedge (Whakataki Formation) of the Hikurangi subduction zone

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Figure S1. Schmidt nets of back-tilted orientations of structural features compared with present-day orientations. Structural data was back-tilted using the nearest S₀ measurement in Stereonet 10 (Allmendinger et al., 2011). a) Deformation bands associated with D1 faulting. b) Normal faults formed during D2 horizontal extension. c) Deformation bands with normal-sense shear formed during D2 horizontal extension. d) Reverse faults formed during D3 horizontal contraction. e) Deformation bands with reverse-sense shear formed during D3 horizontal contraction. f) Deformation bands with a regular spacing and minimal offset observed in areas of folded sandstone beds, formed during D3 horizontal contraction. Tight clustering of these bands when in their original orientation indicates that they have since been rotated with folding.

Table S1. Table of microfabric data for analysed thin sections.

		Sample	Band width (mm)	Host rock average Perimon	DB average Perimeter (um)	HR diamerer (um)	D B Diameter (um)	A spect ratio (HR)	A spect ratio (DB)	Grainsize Reduceio	Band off set (mm)	DBporosty	DBporosty fraction	HR Porosity	HR porosity fraction	Weights	DBrieg error	DBposerror	HR nag artor	HR poserior	Dc	DarDe	Dihedral angle	Porosity R eduction	Macro spacing (cm)	Vamage zone widh (cm)	Fault offset (cm)	Bed thickness (cm)	L ocation (lary	Location (forg)	Type of Band	Lthology (Faces)
		48.1	0.636	171.65	59.39	54.64	18.90	1.63	1.68	35%	4.40	7.30	0.07	13.50	0.13	0.19	1.33	1.36	2.10	2.13	0.05	96.59	N/A	6.20	NL	12.00	30.00	N/A	-40.938763	176.169680	Normal CSB	FA3
		97.4	1.505	257.44	147.21	81.95	46.86	1.50	1.63	57%	6.20	4.93	0.05	12.66	0.13	0.23	1.13	1.13	1.62	1.64	0.13	46.56	N/A	7.73	NL	> 55 cm IDZ	195.00	N/A	-40.925111	176.190607	Normal CSB	FA2
		97.1.2	1.300	195.57	157.03	62.25	49.98	1.58	1.61	80%	8.30	2.89	0.03	9.83	0.10	0.22	0.64	0.63	1.53	1.54	0.10	82.96	N/A	6.94	NL	> 55 cm IDZ	195.00	N/A	-40.925111	176.190607	Normal CSB	FA2
		131.5	0.877	283.55	161.85	90.26	51.52	1.55	1.58	57%	5.60	8.49	0.08	17.43	0.17	0.22	1.82	1.84	2.49	2.55	0.09	59.01	N/A	8.94	NL	> 30 cm IDZ	55.00	N/A	-40.929451	176.181770	Normal CSB	FA2
	D2	74.3	0.917	216.14	65.17	68.80	20.75	1.62	1.60	30%	6.10	7.96	0.08	18.71	0.19	0.15	1.15	1.16	1.61	1.64	0.12	50.31	N/A	10.74	NL	4.00	31.00	N/A	-40.936817	176.173234	Normal CSB	FA2
	DZ	53.3.2	0.939	213.39	56.61	67.92	18.02	1.76	1.14	27%	5.50	8.08	0.08	17.17	0.17	0.22	1.76	1.77	2.19	2.24	0.10	53.33	N/A	9.09	NL	> 200 cm IDZ	>10 m	N/A	-40.938075	176.170602	Normal CSB	FA3
		53.1.2	0.807	143.51	86.23	45.68	27.45	1.65	1.58	60%	4.80	7.04	0.07	13.19	0.13	0.17	1.18	1.18	2.06	2.08	0.06	83.95	N/A	6.15	NL	> 200 cm IDZ	>10 m	N/A	-40.938075	176.170602	Normal CSB	FA3
		53.1.1	0.952	258.45	61.45	82.27	19.56	1.58	1.63	24%	6.10	5.55	0.06	14.12	0.14	0.22	1.22	1.21	2.27	2.29	0.10	64.19	N/A	8.57	NL	> 200 cm IDZ	>10 m	N/A	-40.938075	176.170602	Normal CSB	FA3
		53.3.1	0.742	245.68	74.61	78.20	23.75	1.67	1.65	30%	6.20	8.93	0.09	16.71	0.17	0.12	0.99	1.03	1.96	1.89	0.07	89.48	N/A	7.78	NL	> 200 cm IDZ	>10 m	N/A	-40.938075	176.170602	Normal CSB	FA3
		101.1	0.827	254.32	115.02	80.95	36.61	1.62	1.69	45%	3.20	6.04	0.06	19.09	0.19	0.19	1.16	1.14	2.60	2.64	0.13	23.99	N/A	13.05	NL	0.10	4.00	N/A	-40.944526	176.160817	Normal CSB	FA3
		141.1.2	1.830	217.33	84.30	69.18	26.83	1.71	1.66	39%	11.20	12.03	0.12	26.09	0.26	0.25	2.99	3.01	2.62	2.72	0.35	32.16	N/A	14.06	NL	145.00	3.00	N/A	-40.941299	176.165649	Reverse CSB	FA3
	D2	74.5	0.639	178.99	44.62	56.97	14.20	1.53	1.68	25%	6.80	13.30	0.13	21.19	0.21	0.19	2.52	2.55	2.00	2.04	0.06	106.30	N/A	7.89	NL	6.00	12.00	N/A	-40.936817	176.173234	Reverse CSB	FA2
	DS DZ	96.1	0.791	246.35	147.98	78.41	47.10	1.61	1.57	60%	3.80	12.53	0.13	19.20	0.19	0.17	2.07	2.10	2.19	2.24	0.07	58.18	N/A	6.67	NL	272.00	10.00	N/A	-40.930442	176.180182	Reverse CSB	FA2
		141.1	1.979	209.30	93.24	66.62	29.68	1.67	1.64	45%	5.60	11.15	0.11	16.57	0.17	0.22	2.45	2.47	2.16	2.21	0.13	43.52	N/A	5.42	NL	145.00	3.00	N/A	-40.941299	176.165649	Reverse CSB	FA3
		141.1.1	1.513	202.43	76.17	64.44	24.24	1.57	1.53	38%	6.20	13.48	0.13	18.08	0.18	0.18	2.37	2.42	1.82	1.87	0.09	72.92	N/A	4.60	NL	145.00	3.00	N/A	-40.941299	176.165649	Reverse CSB	FA3
		1.1	1.002	157.36	92.49	50.09	29.44	1.71	1.69	59%	0.10	11.86	0.12	20.09	0.20	0.16	1.87	1.91	1.49	1.52	0.10	0.97	88.00	8.24	11.80	N/A	N/A	80.10	-40.939025	176.168786	SECB	FA3
	D2	3.1	0.581	173.15	104.68	55.12	33.32	1.68	1.64	60%	0.02	8.63	0.09	16.01	0.16	0.14	1.21	1.22	1.51	1.52	0.05	0.39	76.00	7.38	6.80	N/A	N/A	40.90	-40.938891	176.169167	SECB	FA3
nor	n-FDZ	4.1	0.526	166.19	104.54	52.90	33.28	1.68	1.66	63%	0.08	8.71	0.09	20.01	0.20	0.19	1.63	1.65	1.66	1.70	0.07	1.08	75.00	11.30	2.20	N/A	N/A	29.20	-40.938865	176.169072	SECB	FA3
		11.2	0.695	142.59	98.56	45.39	31.37	1.74	1.65	69%	0.15	6.03	0.06	17.88	0.18	0.16	0.97	0.98	1.31	1.33	0.10	1.50	68.00	11.85	30.00	N/A	N/A	93.80	-40.938841	176.169425	SECB	FA3
		11.3	0.635	76.34	46.40	24.30	14.77	1.76	1.60	61%	0.02	5.16	0.05	17.24	0.17	0.15	0.76	0.77	1.25	1.27	0.09	0.22	68.00	12.08	30.00	N/A	N/A	93.80	-40.938813	176.169415	SECB	FA3
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		FDZ	Fault	Damage	Zone																											
		IDZ	Intera	ction Da	image Zo	ne																										
		CSB	Compa	actional	Shear B	and																										
	SE		Shear-Enhanced Compaction Band																													

		IDZ	Interaction Damage Zone						
I		CSB	Compactional Shear Band						
		SECB	Shear-Enhanced Compaction Band						
	Key	FA2	50:50 mudstone to sandstone						
	-	FA3	Sandstone dominated						
		HR	Host Rock						
		DB	Deformation Band						
		NL	Non-Linear						

	Fault	Mean P	Median P	P Range	P IQR
	Day 23 D2	0.10	0.07	0.62	0.06
	Day 24 D2	0.47	0.60	1.62	0.04
	Fault 14	0.15	0.10	1.19	0.06
D2 FDZ	Fault 17.1	0.32	0.33	0.43	0.16
	Fault 17.2	0.62	0.61	0.25	0.04
	Fault 100	0.44	0.46	0.21	0.03
	Fault 161	0.42	0.42	0.62	0.07
	Day 23 D3	-0.02	0.25	1.36	0.53
	Fault 96	0.13	0.17	1.65	0.10
D3 FDZ	Fault 102	0.11	0.22	1.16	0.35
	Fault 117	0.67	0.59	0.43	0.22
	Fault 141	0.66	0.62	0.52	0.05
	Bed 1 Set 2	-0.17	-0.07	0.95	0.04
	Bed 1 Set 1	-0.69	-0.64	0.40	0.09
	Bed 2 Set 2	0.03	-0.10	1.23	0.30
	Bed 3 Set 1	-0.25	-0.27	0.94	0.20
	Bed 4 Set 2	0.09	0.25	1.48	0.59
	Bed 6 Set 1	0.02	0.04	1.11	0.04
	Bed 7 Set 1	-0.15	-0.07	1.17	0.13
	Bed 8 Set 1	0.31	0.32	0.90	0.20
	Bed 9.2 Set 1	0.34	0.34	0.71	0.31
	Bed 10 Set 1	0.42	0.39	0.27	0.17
	Bed 10 Set 1 Main	0.42	0.40	0.32	0.31
	Bed 10 Set 2	0.29	0.31	0.84	0.06
	Bed 11 Set 2	-0.31	-0.32	1.82	0.24
D3	S1 B1 set 2	-0.39	-0.29	0.81	0.34
non-FDZ	S1 B2 set 1	0.31	0.33	1.50	0.14
	S1 B3 set 1	0.04	0.04	1.49	0.19
	S2 B2 set 1	0.57	0.61	1.68	0.04
	S2 B3 set 1	0.09	0.10	1.21	0.23
	S3 B3 set 2	-0.40	-0.32	0.92	0.60
	Stop 2	-0.73	-0.65	0.63	0.42
	Stop 3	0.37	0.16	1.09	0.90
	Stop 4 bed 1	-0.12	-0.07	0.99	0.08
	Stop 4 bed 2	-0.15	-0.13	1.03	0.09
	Stop 4 bed 3	-0.17	-0.25	1.16	0.12
	Stop 5	0.09	0.13	0.99	0.08
	Stop 6	0.32	0.32	0.60	0.03
	Stop 7	0.21	0.10	0.96	0.13
	Stop 8	-0.27	-0.25	0.89	0.06

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Table SZ. I	able of	results from	Pearson	correlation	coentcient	anaivsis (or de	iormation	Dana S	DACIUS.

	FDZ	Fault Damage Zone					
Кеу	IQR	Inter-QuartileRange					
	Р	Pearson Correlation Coefficient					



Figure S2. Schmidt net showing the orientations of deformation bands in three beds across a fold hinge. Deformation band present day orientation, and back-rotated orientations are shown. Present data orientation aligns with the great circle that is perpendicular to the fold axis indicating that deformation bands have been passively rotated with the folding of the host beds.



Figure S3. A plot to show the relationship between the fault displacement and the associated damage zone width. Fault displacement was measured where true displacement could be calculated from slip vector orientations and the separation of sedimentary markers across the fault plane (Shipton et al., 2006). Data shows that there is no correlation between the width of a damage zone and the offset of the associated fault.

Table S3. Table to show estimated permeability values. Equation used to estimate permeability from porosity: $\ln k = 21.41 + 11.425 \ln \phi_e + 1.327 (\ln \phi_e)^2$ (Wu, 2004). Order of magnitude reduction (OoMR) was calculated using: $OoMR = \log_{10} \frac{Host Rock Permeability}{Deformation Band Permeability}$

			Order of magnitude
	Porosity (%)	Permeability (mD)	reduction
D2 Host Rock	13.00	38.00	1.00
D2 Deformation Band	5.00	0.40	1.98
D3 FDZ Host Rock	20.00	645.00	
D3 FDZ Deformation			1.45
Band	12.00	23.00	
D3 non-FDZ Host Rock	19.00	449.00	
D3 non-FDZ			1.95
Deformation Band	9.00	5.00	

Table S4. Table to show the correlation statistics from porosity analysis of different band kinematics shown in Figure 9.

Porosity Analysis	Band Kinematics	Pearson	R ²
	D2 CSB, D3 CSB, SECB	0.69	0.47
Host Rock and	D2 CSB	0.72	0.51
Deformation Band	D3 CSB	0.06	0.00
	SECB	0.56	0.32
	D2 CSB, D3 CSB, SECB	0.55	0.30
Host Rock and Absolute	D2 CSB	0.79	0.62
Porosity Reduction	D3 CSB	0.97	0.94
	SECB	0.14	0.02



Figure S4. Empirical cumulative distribution plots to show the variation in grain sizes measured in thin sections of D2 CSBs [a], D3 CSBs [b], and D3 SECBs [c]. Two-sample Kolmogorov-Smirnov tests indicate that for each type of DB, the difference between the grain size within the DB and within the adjacent host rock is statistically significant. Within each DB, the grain size reduces.

Supplement Section S.9



Figure S5. Histograms to show Pearson correlation coefficient values established from multiple scanlines along deformation band maps from fault damage zones (FDZs). D2 FDZ and D3 FDZ are differentiated by colour. Many analyses have a main peak ca. 0.5 indicating a positive relationship between the spacing of deformation bands and the distance of those bands from a fault plane. However, within the dataset, there are peaks at values that are closer to 0. E.g.: in b) where the peak value is ca. 0.1 or h) where there is a cluster of peaks around 0. Peaks that have Pearson values that are close to zero indicate that there is no relationship between spacing and distance from the fault plane and is indicative of regular spacing. The range in Pearson values for each outcrop indicates that the spacing between deformation bands and the distance from a fault plane are not described by a simple relationship and that this relationship can vary on the outcrop scale.



Figure S6. Histograms to show Pearson correlation coefficient values for D3 deformation bands that are characterised by minimal offset and a regular spacing (D3 non-FDZ). The spacing of bands has been compared to the distance perpendicular to strike. Most histograms show a peak ca. 0. This indicates no relationship between spacing and distance. There are, however, instances of a large spread of Pearson data e.g. in image (k). 12 out of 28 outcrops analysed have a spread of Pearson data that is greater than 1. This indicates that there can be scan-lines across a single outcrop that are identifying band populations with positive, negative, and zero correlation between the spacing and distance from the image origin.



Figure S7. Histograms to show the frequency distribution of absolute spacing measurements between bands in fault damage zones. The probability density function is on the y-axis. The histograms have a positive skew representing the decay of damage away from the fault plane.



Figure S8. Histograms to show the probability density function of spacing of D3 deformation bands observed in outcrops that are not directly adjacent to a fault. In these outcrops, deformation bands show a 'regular' spacing. The bands analysed in this plot are characterised by minimal offset / no observable offset. Histogram plots are not consistent. Some have a bimodal distribution (e.g. d and I). Some are characterised by a normal distribution (e.g., k and t). Many have a positive skew yet compared to 'fault-associated' band spacing, there is a broader spread, indicative of regularly spaced bands, with noise (Fig. S10b).



Figure S9. [a], [b] Spacing analysis of CSBs associated with the damage zone of faults. 100 scan-lines were taken for each image during analysis. [a] represents a D2 normal fault and [b] shows a small D3 reverse fault. Both faults show an increase in spacing between deformation bands with increasing distance from the fault plane. This is reflected in the Pearson correlation coefficient. Values are approaching 1, which shows a dependence of distance on spacing. [c], [d] Spacing analysis of dominantly SECBs with rare CSBs not associated with the damage zone of faults. 100 scan-lines were taken for each image during analysis. Each image shows a general lack of correlation of the distance with the spacing between deformation bands. Pearson correlation coefficient values close to 0 further suggest a lack of correlation. These bands show a near-constant spacing. Median spacing: [c] = 1.8 cm; and [d] = 2.3 cm.

In this research, we have created six synthetic images to show ideal spacing distributions and to highlight how natural variation in heterogeneous rocks and data collection errors can impact the measured spacing of natural sample. These images are created as an interpretive guide to analyse natural spacing distributions. The six synthetic images represent (Fig. S10):

[a] Deformation bands with constant spacing

[b] Deformation bands with constant spacing and added noise to replicate measuring bias and outcrop conditions. The noise in image [b] was generated by adding an array of random values, between 0 and 0.8 of the constant spacing value, to the space. The random values are collectively characterised by a normal distribution and a median value of 0

[c] Deformation bands spatially characterised by an exponential spatial decay away from a fault

[d] Deformation bands characterised by an exponential spatial decay away from a fault with integrated noise. Noise in the image [d] is generated by adding values up to 0.4 of the maxima spacing onto each spacing measurement, with added values collectively characterised by a normal distribution with a median value of 0

[e] Deformation band spacing that reflects the overprint of an equally spaced distribution [a] by an exponentially decaying damage zone [c]

[f] Deformation band spacing reflecting the overprint of an equal distribution with integrated noise [b] by an exponentially decaying damage zone also containing integrated noise [d].

Bands with a strictly constant spacing show a zero Pearson correlation coefficient (Fig. S10a). With the addition of normally distributed 'noise' to case [a], a distributed set of spacing with Gaussian noise is obtained (Fig. S10b). In this case [b], the Pearson correlation coefficient of spacing over distance is -0.08. The third synthetic image [c] represents a damage zone with an exponential decay of deformation band density away from the fault plane (Fig. S10c). For this example, the Pearson correlation coefficient between spacing and distance to the fault is exactly 1 (Fig. S10c). A histogram of this spacing distribution shows positive skew. The same results are expected for any other analytical expression in which spacing grows monotonously with distance from the fault (e.g., the power-law relationship established by Savage and Brodsky (2011)). With the addition of Gaussian noise to a damage zone [d], the Pearson correlation coefficient reduces to 0.56 (Fig. S10d). However, its exact value depends on the amount of noise and can be larger or smaller. Synthetic image [e] represents an overprint of two distributions, equal spacing and variable spacing, simulating two different deformation events affecting the same bed subsequently (Fig. S10e). If the deformation bands resulting from the two events are morphologically similar, they may be difficult to distinguish in the field and can be mapped together as one. In this case, the Pearson value is 0.71, although it could be any value between 0 and 1 dependent upon the value of spacing in the background density compared with the damage zone spacing. In image [f], noise is integrated into both distributions and they are combined (Fig. S10f). This is the most realistic outcome if there is an overprint of two events with different distributions. In the case shown, the Pearson value is 0.59. However, with different magnitudes of noise and varied initial spacings, any value from -1 to 1 could be obtained. For the interpretation of our field data, we assume a positive correlation between band spacing and spatial location if the Pearson value is > 0.5.



Figure S10. Synthetic images produced to replicate different distributions of the deformation bands. [a] deformation bands with a constant spacing, [b] deformation bands with a constant spacing with added Gaussian noise, [c] bands with an exponential decay away from a fault plane, and [d] deformation bands with an exponential decay away from a fault plane with added Gaussian noise. [e] and [f] represent images that combine constant spacing with a damage zone. These examples would be relevant if a damage zone overprinted a constant background spacing of the deformation band. [e] combines [a] with [c]. [f] combines [b] and [d] resulting in a spacing that contains two distributions that have noise. The relationship between spacing and distance is analysed using the Pearson correlation coefficient. Values close to 1 show a positive relationship between the distance

from a point and the spacing. This would be seen in a damage zone that shows an increase in spacing between deformation bands as the distance from the fault plane increases. Pearson correlation coefficient values close to 0 show no correlation between spacing and distance. A histogram of the spacing is also shown. Unimodal distributions with no skew reflect bands with near-constant spacing. A positive skew represents damage zones. Distance and spacing are also plotted for different scan-lines. Distance is normalised to the maximum distance and spacing is normalised to the maximum spacing. P = Pearson correlation coefficient value.

References

Allmendinger, R. W., Cardozo, N., and Fisher, D. M.: Structural geology algorithms: Vectors and tensors, Cambridge University Press, 2011.

Savage, H. M. and Brodsky, E. E.: Collateral damage: Evolution with displacement of fracture distribution and secondary fault strands in fault damage zones, Journal of Geophysical Research, 116, 2011.

Shipton, Z., Soden, A., Kirkpatrick, J., Bright, A., and Lunn, R.: How Thick is a Fault? Fault Displacement-Thickness Scaling Revisited, Earthquakes: Radiated Energy and the Physics of Faulting, 170, 2006.

Wu, T.: Permeability prediction and drainage capillary pressure simulation in sandstone reservoirs., 2004. Texas A&M University, 2004.