

Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

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Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

⏪

⏩

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



The relation between the long-term movement trend of horizontal velocity on a ground station and the Euler vector of plate movement can be expressed as follows (Jin et al., 2006; Yang and Zeng, 2009):

$$\begin{bmatrix} v_n \\ v_e \end{bmatrix} = \begin{bmatrix} R \sin \lambda & -R \cos \lambda & 0 \\ -R \sin \phi \cos \lambda & -R \sin \phi \sin \lambda & R \cos \phi \end{bmatrix} \times \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}, \quad (2)$$

5 where v_e denotes the easterly component of the ground station's horizontal velocity in a topocentric coordinate system, and v_n represents the northerly component. R represents the radius of earth, and λ , ϕ are the latitude and longitude of the ground point. Thus, the matrix \mathbf{A} in Eq. (1) is:

$$\mathbf{A} = \begin{bmatrix} R \sin \lambda & -R \cos \lambda & 0 \\ -R \sin \phi \cos \lambda & -R \sin \phi \sin \lambda & R \cos \phi \end{bmatrix}. \quad (3)$$

10 Generally, the measured point signal is the local motion variation without the plate rigid motion, which is the horizontal residual velocity in measured points. So $\mathbf{B} = \mathbf{I}$ (unit matrix) in Eq. (1).

If we take the local movement variation signal $\hat{\mathbf{S}}'$ of a non-observed point into account and assume that there exists a covariance matrix $\boldsymbol{\Sigma}_{SS'} = \boldsymbol{\Sigma}_{S'S'}^T \neq 0$ between the non-
15 observed point's signal $\hat{\mathbf{S}}'$ and the observed point's signal $\hat{\mathbf{S}}$ then, if the covariance matrix is known, the collocation solution considering the non-observed point's signal simultaneously (Yang and Zeng, 2009; Zeng et al., 2012) is:

$$\begin{cases} \hat{\boldsymbol{\omega}} = (\mathbf{A}^T \mathbf{P}_L \mathbf{A})^{-1} \mathbf{A}^T \mathbf{P}_L L \\ \hat{\mathbf{S}} = \boldsymbol{\Sigma}_S \mathbf{B}^T \mathbf{P}_L (L - \mathbf{A} \hat{\boldsymbol{\omega}}) \\ \hat{\mathbf{S}}' = \boldsymbol{\Sigma}_{S'S} \boldsymbol{\Sigma}_S^{-1} \hat{\mathbf{S}} \end{cases}, \quad (4)$$

where $\mathbf{P}_L = (\mathbf{B} \boldsymbol{\Sigma}_S \mathbf{B}^T + \boldsymbol{\Sigma}_e)^{-1}$.

Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



dom signals, like the collocation, but as non-random variables, taking into account their random nature (Tao and Yao, 2003), reflected by the distance function, to construct the covariance matrix of the local signals. The covariance matrix of the local deformation is

$$\mathbf{G}_S = \begin{bmatrix} g_{11} & g_{12} & \cdots & g_{1m} \\ g_{21} & g_{22} & \cdots & g_{2m} \\ \cdots & \cdots & \cdots & \cdots \\ g_{m1} & g_{m2} & \cdots & g_{mm} \end{bmatrix}, \quad (5)$$

where g is the value obtained by the distance function.

We still use the Eq. (1) as the error equation. Because of this, the distance function does not explicitly consider the physical nature of the local deformation. Using the compensation least squares method estimation criterion:

$$V^T \Sigma_e^{-1} V + \hat{\mathbf{S}}^T G_S^{-1} \hat{\mathbf{S}} = \min. \quad (6)$$

Then, according to Tao and Yao (2003) and Wang and Ou (2004),

$$\begin{cases} \hat{\omega} = \left(\mathbf{A}^T (\mathbf{B} \mathbf{G}_S \mathbf{B}^T + \Sigma_e) \mathbf{A} \right)^{-1} \mathbf{A}^T (\mathbf{B} \mathbf{G}_S \mathbf{B}^T + \Sigma_e)^{-1} \dot{X} \\ \hat{\mathbf{S}} = \mathbf{G}_S \mathbf{B}^T (\mathbf{B} \mathbf{G}_S \mathbf{B}^T + \Sigma_e)^{-1} (\dot{X} - \mathbf{A} \omega). \end{cases}$$

Considering the collocation problem of the non-observed point's signal parameter \mathbf{S}' , we use the distance function to contact the measured point's signal parameter \mathbf{S} and the unmeasured point's signal parameter \mathbf{S}' . So the $\Sigma_{\mathbf{S}\mathbf{S}'}$ in Eq. (4) is transformed to

$$\mathbf{G}_{\mathbf{S}'\mathbf{S}} = \begin{bmatrix} g_{s'_1 s_1} & \cdots & g_{s'_1 s_m} \\ \cdots & \cdots & \cdots \\ g_{s'_p s_1} & \cdots & g_{s'_p s_m} \end{bmatrix}. \quad (7)$$

Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Again, δ represents the smoothing factor, and if $\delta = 0$, the inverted double curved surface is a conical surface.

3. Positive three surface:

$$g(x, y, x_{0i}, y_{0i}) = \left[(x - x_{0i})^2 + (y - y_{0i})^2 + \delta^2 \right]^{\frac{3}{2}} \quad (11)$$

4. Inverted three surface:

$$g(x, y, x_{0i}, y_{0i}) = \left[(x - x_{0i})^2 + (y - y_{0i})^2 + \delta^2 \right]^{-\frac{3}{2}} \quad (12)$$

As can be seen, the actual covariance matrix Σ_S of the signal is replaced by the matrix G_S determined in the multi-quadric function, which is exactly the same as the standard configuration model in the form; namely, Eqs. (4) and (6) are exactly identical. Although the two methods are similar in form, their theoretical basis is different. According to the rule of maximum posterior estimation, the standard configuration model obtains the optimal estimate under the condition of the signal a priori variance being known. However, the latter considers the randomness of the parameters, gives a certain compensation and balance, and still considers it as a parameter estimation of non-random parameters, and the optimization is better than the previous method (Wang and Ou, 2004). In this way, we not only overcome the problem that the covariance function of the classical fit model is difficult to determine but also keep the formula invariance of the fitting model. Because of its simplicity and rationality, the application scope of the model can be greatly expanded (Tao et al., 2002; Tao and Yao, 2003).

4 Calculation and analysis

We used the same observation data as in (Yang and Zeng, 2009), that is, 1041 repeat observation stations of the Crustal Movement Observation Network Engineering,

Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page	
Abstract	Introduction
Conclusions	References
Tables	Figures
◀	▶
◀	▶
Back	Close
Full Screen / Esc	
Printer-friendly Version	
Interactive Discussion	



whose precision of horizontal velocity is superior to fitting point coordinates velocity by 3 mm yr^{-1} . This data includes 85 high precision points (29 consecutive observation stations and 56 irregular observation basis points) as the external inspection points to assess the accuracy of the constructed velocity field model, and a net of the remaining 985 regular observation points after subtracted 56 irregular observation basis points from the 1041 repeat observation stations to establish the velocity field model.

In order to evaluate the internal precision of the model, the calculation formula for the root-mean-square error (RMS) of the horizontal residual velocity of the 985 observation stations is calculated:

$$\text{RMS} = \sqrt{\frac{V^T \cdot V}{985}}, \quad (13)$$

where V is residuum calculated by different solutions, that is, station horizontal residual velocity.

The RMS of the external checkpoint horizontal velocity can be defined by:

$$\text{RMS} = \sqrt{\frac{(\dot{X}_m - \dot{X}_c)^T \cdot (\dot{X}_m - \dot{X}_c)}{85}}, \quad (14)$$

where \dot{X}_m is the measured horizontal velocity of the 85 checkpoints, and \dot{X}_c is the horizontal velocity of the 85 stations, calculated by different functions.

4.1 Calculation results for different kernel functions

Since the multi-quadric function is used to determine the signal priori random information in the multi-quadric collocation model, different kernel functions have different results. We use inverted and positive, double curved, two, and three surfaces to obtain results. Table 1 shows statistics for velocity residuals for the different kernel functions

Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page	
Abstract	Introduction
Conclusions	References
Tables	Figures
◀	▶
◀	▶
Back	Close
Full Screen / Esc	
Printer-friendly Version	
Interactive Discussion	



Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page	
Abstract	Introduction
Conclusions	References
Tables	Figures
◀	▶
◀	▶
Back	Close
Full Screen / Esc	
Printer-friendly Version	
Interactive Discussion	



Discussion Paper | Discussion Paper | Discussion Paper | Discussion Paper | Discussion Paper

for east and 1.43 mm yr^{-1} for north. The external check precision also improved, to 2.14 mm yr^{-1} for east and 1.47 mm yr^{-1} for north.

4. Using a multi-quadric function method can obviously improve the precision of the velocity model. The internal residual statistic is 2.79 mm yr^{-1} for east and 2.25 mm yr^{-1} for north; the external check precision is 1.85 mm yr^{-1} for east and 1.40 mm yr^{-1} for north. Theoretically, multi-quadric functions can approximate the measured surface with arbitrary accuracy, but in practice it is impossible to select all the observation points for the node in order to improving the fitting internal precision without considering the estimate precision of the non-observation points (i.e. the precision of the external check points). However, extrapolation precision is what we need to focus on.
5. Synthesizing collocation method and multi-quadric function method not only obviously improved internal precision, with east and north precision reaching 0.78 and 0.73 mm yr^{-1} , respectively, which is obviously superior to the collocation method and the multi-quadric function method; but external precision has also obviously improved, with east and north direction precision reaching 1.67 and 1.45 mm yr^{-1} , respectively, which is slightly superior to the collocation method and the multi-quadric function method. This approach integrates the characteristics of the two methods. It avoids the establishment of the covariance function, and achieves a combined effect.
6. The Euler vector, collocation and multi-quadric collocation models have physical meaning, and can work out the Euler vectors of Chinese mainland blocks. However, the Euler vector method has larger differences from the other two methods, which, in particular, have smaller differences in latitude and longitude components and rotating angle speed aspects. The Euler vectors determined by the collocation method and the multi-quadric function configuration model are very close.

5 Conclusion

Multi-quadric functions and the collocation method are the most commonly used methods of fitting the observed points and estimating the non-observed points. However, it is difficult to select the kernel function, smoothing factor, and node when we use the multi-quadric function method. The key to applying the collocation model is to establish reliable covariance function. Usually, it tends to adopt an empirical formula in a gravitational field, where the majority of applications are established, by using a measured data covariance model, which not only affects the optimality of the collocation method but also reduces its usable area.

Taking into account the establishment of the covariance function is a relatively high requirement for data, and generally, it is difficult to achieve. Bearing in mind that the covariance function is a function of the distance, the local deformations covariance matrix is often chosen as a simple function of distance in multi-quadric functions. The estimating effects of this integrated approach are similar to the collocation method. Because the solution is simple and reasonable, it can greatly expand the scope of application of the collocation model.

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Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

⏪

⏩

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Freymueller, J. T., Woodard, H., Cohen, S. C., Cross, R., Elliott, J., Larsen, C. F., Hreinsdóttir, S., and Zweck, C.: Active deformation processes in Alaska, based on 15 years of GPS measurements, in: Active Tectonics and Seismic Potential of Alaska, American Geophysical Union, Washington, D. C., 1–42, 2013.

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**Multi-quadric
collocation model of
horizontal crustal
movement**

G. Chen et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

⏪

⏩

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Table 1. Velocity residuals statistics for different kernel functions (mm yr^{-1}).

Plan	East				North			
	Max	Min	Average	RMS	Max	Min	Average	RMS
Inverted double curved surface	4.17	-7.65	0.01	0.56	3.03	-6.49	0.01	0.51
Inverted two surface	5.75	-11.27	0.02	0.78	3.76	-9.633	0.02	0.73
Inverted three surface	11.00	-22.61	0.02	1.46	9.05	-19.52	0.02	1.41
Positive double curved surface	-	-	-	-	-	-	-	-
Positive two surface	21.50	-30.13	0.00	3.79	27.68	-22.94	0.00	4.54
Positive three surface	13.25	-22.59	0.00	1.29	5.02	-19.30	0.00	1.14

[Title Page](#)
[Abstract](#)
[Introduction](#)
[Conclusions](#)
[References](#)
[Tables](#)
[Figures](#)
[Back](#)
[Close](#)
[Full Screen / Esc](#)
[Printer-friendly Version](#)
[Interactive Discussion](#)


Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

[Title Page](#)
[Abstract](#)
[Introduction](#)
[Conclusions](#)
[References](#)
[Tables](#)
[Figures](#)




[Back](#)
[Close](#)
[Full Screen / Esc](#)
[Printer-friendly Version](#)
[Interactive Discussion](#)


Table 2. External inspection accuracy of different kernel functions (mm yr^{-1}).

Plan	East				North			
	Max	Min	Average	RMS	Max	Min	Average	RMS
Inverted double curved surface	5.79	−4.59	0.08	1.38	6.20	−3.32	0.08	1.18
Inverted two surface	6.21	−4.75	0.00	1.67	7.69	−2.79	0.12	1.45
Inverted three surface	7.06	−5.79	0.15	1.93	8.49	−4.22	0.03	1.77
Positive double curved surface	4.76	−20.83	0.09	2.61	2.59	−3.68	0.49	1.27
Positive two surface	21.24	−14.73	0.78	5.02	21.71	−12.48	0.34	5.02
Positive three surface	3.73	−4.79	0.13	1.2	3.01	−2.61	20.24	0.89

Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Table 4. Internal precision of the Euler vectors (mm yr^{-1}).

Scheme	East				North			
	Max	Min	Average	RMS	Max	Min	Average	RMS
1	30.17	-23.30	0.16	4.63	23.48	-27.69	-0.20	6.19
2	30.29	-23.89	0.04	4.89	25.37	24.08	0.24	6.59
4	30.46	-23.53	0.04	4.89	24.69	24.59	-0.17	6.35

Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Table 5. Velocity residuals statistics (mm yr^{-1}).

Scheme	East				North			
	Max	Min	Average	RMS	Max	Min	Average	RMS
1	30.17	-23.30	0.16	4.63	23.48	-27.69	-0.20	6.19
2	23.12	-13.30	0.03	1.60	19.68	-7.49	-0.03	1.43
3	29.13	-15.20	0.00	2.79	24.54	-9.12	0.00	2.25
4	5.75	-11.27	0.00	0.78	3.76	-9.633	0.00	0.73

Multi-quadric collocation model of horizontal crustal movement

G. Chen et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Table 6. External examination precision (mm yr^{-1}).

Scheme	East				North			
	Max	Min	Average	RMS	Max	Min	Average	RMS
1	13.34	-20.29	-0.05	5.89	16.47	-23.29	1.315	7.06
2	9.10	-8.54	0.00	2.14	3.12	-5.34	0.00	1.47
3	12.48	-3.75	0.00	1.85	4.50	-6.94	0.00	1.40
4	6.21	-4.75	0.00	1.67	7.69	-2.79	0.12	1.45

**Multi-quadric
collocation model of
horizontal crustal
movement**

G. Chen et al.

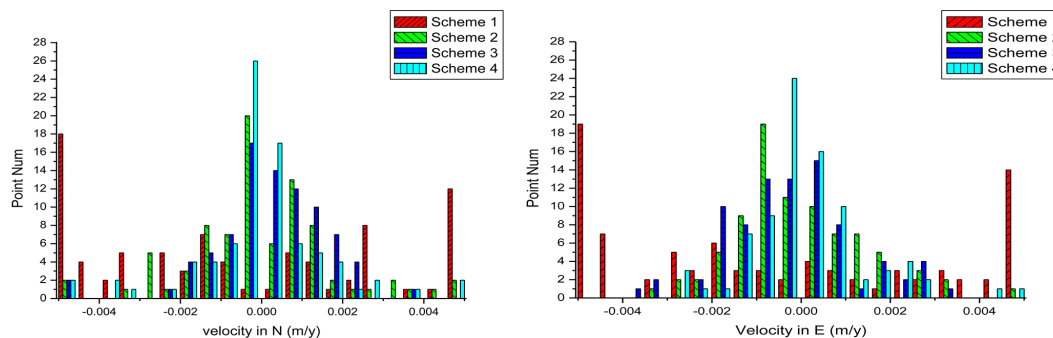


Figure 1. The velocity residuals statistics of 85 external check points.

[Title Page](#)[Abstract](#)[Introduction](#)[Conclusions](#)[References](#)[Tables](#)[Figures](#)[Back](#)[Close](#)[Full Screen / Esc](#)[Printer-friendly Version](#)[Interactive Discussion](#)