

Response to Interactive comment on “A simple 3-D numerical model of thermal convection in Earth’s growing inner core: on the possibility of the formation of the degree-one structure with lateral viscosity variations” by M. Yoshida

Anonymous Referee #2

This manuscript is aimed to reveal the style of thermal convection in Earth’s inner core with its thermal history that might have degree-one structure. There have been several studies on the style of inner core convection mainly done by R. Deguen and his colleagues that was called as ‘Translational Regime’. The author discussed formation of degree-one convection caused by the rheological heterogeneity because a series of studies by Deguen and his colleagues could not address the lateral viscosity variation due to their numerical limitation. The lateral viscosity variation could be caused by the generation of hemispherical feature observed by various seismological analyses but the time-scale is too much long compared to the current understanding on the age of the inner core, which would be over 3.0 Gyrs. This means that the ‘translational regime’ found by Deguen and colleague would be still a great candidate for understanding the large-scale seismic heterogeneity and anisotropy observed in the inner core but this study would be somewhat interesting and important step for the community. However, unfortunately, I CANNOT recommend publishing this manuscript without huge amount of revisions experienced because I found a bunch of technical errors in the model assumptions and treatment of boundary conditions as well as missed citations on various important literatures and important discussion on inner core dynamics and its implication for seismic observations. If the author fix all of his mistakes in his model assumption and numerical procedure, cite various important literatures and add some important discussion on the age of the inner core, I would re-consider my recommendation. Again, currently, this manuscript SHOULD NOT be published in anywhere. Before discussing contexts of science in the original manuscript, author should address significant issues listed-up (also required with re-run for all cases as well as several additional runs will be required. In addition to that, both thermal and mechanical boundary conditions used in this study MUST be changed.) below because entire discussions in this manuscript would NOT be quite understandable and convinced for readers.

[Reply] I sincerely thank the reviewer for critical comments. I have carefully incorporated all the comments and suggestions into the revised manuscript attached below. The revised parts are highlighted by red. Although I regret that there are some misleading descriptions for readers in the original manuscript, this paper did not violate any of previous studies published so far. I have total respect for all of the previous studies on the core modeling. However, I would acknowledge sincerely the lack of explanation of our model and discussion with the previous studies. Thanks to the reviewer’s thoughtful comments, I could find new literatures, expand discussion largely, and largely improve the manuscript, separating the previous Section 4 to new Sections 4 (Discussion) and 5 (Conclusions). However, the main conclusions was not changed from that in the

original manuscript. Of course, I knew that there are many theoretical and numerical studies on core dynamics, but am only trying to present a simple numerical model and open the discussion. This is because I submitted the manuscript to Solid Earth, not to other journals. However, again, I would acknowledge the lack of required discussion in the original manuscript and I deeply regret this point and deeply acknowledge all of reviewer's comments.

I provide below my response to reviewer's comments.

1. I demand author to check effects of radioactive heating because the possibility of radioactive elements in the outer and inner core would be still under the debate in mineral physics, geodynamics, geomagnetism and seismological communities.

[Reply] Thank you very much for your comment. Because the radioactive potassium may be major heat source in the inner and outer core, and there is a large possibility that the role of potassium is important in determining the history of growth of inner core and geodynamo power (e.g., Nimmo et al. 2004). However, I ignore explicitly radioactive heating in the present model because the amount of radioactive potassium in the inner and outer core would be still under the debate in mineral physics, geodynamics, geomagnetism and seismological communities, and instead consider primordial heating in the heat source term of the conservation equation of energy. I have explained explicitly this point in Section 2.

2. Regarding the treatment of convective vigor and secular cooling (eq. (5) and eq. (6)), I did NOT quite understand why the author used such formulations. For example, the heat capacity was appeared in the Rayleigh number, which was quite odd to me. Why was the heat capacity appeared in the Ra? Please justify how to formulate the Rayleigh number.

[Reply] I opened eq. 5 to enable readers to understand a relationship of (thermal diffusivity) = (thermal conductivity) / (density x heat capacity)

3. I did not get it on the non-dimensionalization done by author's formulation. I did not understand the temperature difference without bottom boundary as the convection was occurred in the inner core. Since the temperature at the center of inner core could not be determined uniquely due to its singularity, using a temperature difference across the convective region would not be correct. The only correct way for determining the temperature difference across the inner core should be scaled by the amount of heat source. The author MUST correct it.

[Reply] Thank you for your comment. Of course, there is another way for normalizing the temperature the inner core by the amount of heat production. However, as stated in reply to reviewers comment #1, I ignore explicitly radioactive heating in the present model. This is because the temperature the inner core is normalized by the characteristic temperature variation, although there is another way for normalizing the temperature the inner core by the amount

of heat production. I have explicitly mentioned this point in Section 2. I agree that the word “reference temperature difference” misleads the readers, so, it is replaced by “characteristic temperature variation”.

4. On addressing the secular cooling, the non-dimensional heating shown in Eq. (5) was somewhat odd to me as well. Yes, it should be zero without the inner core BUT the inner core got cooling down rapidly (11.3 TW!) once the inner core gets started growing. I am not quite sure if the inner core might have the primordial heating or not. I guess that it would be probably NOT. The correct way is for secular cooling to be addressed as the boundary condition NOT the internal heat source in the convection system. The initial temperature of inner core should be determined by the solidus temperature of iron-alloy and adiabatic heat flux across the ICB plus the latent heat release and gravitational energy caused by light element release. I would understand that the molten core might have initial accretion energy before inner core started growing but, again, NOT in the inner core. Therefore, this assumption is completely WRONG. The author MUST fix it then re-run all cases.

[Reply] Thank you very much for your thoughtful comment. I absolutely agree your comment. In section 4, I have explicitly mentioned the lack and limitation of the present simple numerical model. I absolutely agree your comment and expanded the discussion. As reviewer pointed out, the dimensionless internal heating production shown in Eq. (5) is incomplete because the inner core got cooling down rapidly once the inner core gets started growing in the present model. The exact way is for the secular cooling to be addressed as the boundary condition problem, not the internal heating production, because the initial temperature of inner core should be determined by the solidus temperature of iron-alloy, adiabatic heat flux across the ICB, the latent heat release and gravitational energy caused by light element release. Furthermore, the molten core might have initial accretion energy before the inner core started growing, but not in the inner core. Although the integration of these two serious problem into the present numerical model is numerically difficult and is beyond the present study on the possibility of the formation of the degree-one structure with lateral viscosity variations, they should be considered in the future model. In any case, I have explicitly discussed these point in Section 4.

5. Moreover, related with comment #3 listed here, I demand author to check if singularity of center of the inner core (Earth) could avoid correctly because the spectral method approach done by Deguen and his colleague and Takehiro [2011; 2015] could avoid the singularity at the center of inner core with special technique. In other words, I demand author to check the validity of model comparing with results of Deguen and his colleague if the author’s way to avoid the singularity at the center of inner core would be robust or not. I do not really think that the initial state of Earth’s core should not have such a small particle as the author stated before inner core got started growing. As far as I understood, a numerical method used by the author (finite volume/difference scheme) that could avoid the singularity at the center of sphere should be found in various

literatures [e.g. a series of papers on core formation by Taras Gerya's group]. Please check them out and ask author to avoid the singularity completely. Otherwise, numerical results shown in this manuscript would NOT be quite RELIABLE for the community.

[Reply] About the extremely small virtual-sphere, I regret that the model description in the original manuscript misleads the readers. This is for the purpose of the computational convenience characteristic of the Yin-Yang grid, and this setup does not mean the existence of the real singularity that violates the mass and heat transport near the center of the model. I have explicitly mentioned this point in Section 2. Yes, I know that there are other theoretical models that avoid the mathematical singularity in the Earth's center. Just in case, I read the papers below by Gerya's and Takehiro's groups that reviewer kindly listed. A largest difference in the methodologies used in our 3D spherical code and Geryas' 2-D spherical code is that they used finite difference method based on a fully staggered rectangular Eulerian grid with a Lagrangian marker-in-cell technique for solving the momentum, continuity and temperature equations, whereas we used finite volume method based on a fully staggered spherical Eulerian grid for solving these basic equations by a primary variable method (Yoshida and Kageyama, 2004 in GRL; 2006 in JGR, Yoshida, 2008 in G-cubed).

- Gerya, T.V. & Yuen, D.A., 2007. Robust characteristics method for modelling multiphase visco-elasto-plastic thermo-mechanical problems, *Phys. Earth Planet. Int.*, 163, 1-4, 83-105.
- Golabek, G.J., Gerya, T.V., Kaus, B.J.P., Ziethe, R. & Tackley, P.J., 2011. Rheological controls on the terrestrial core formation mechanism, *Geochem. Geophys. Geosyst.*, 10, 11, Q1107.
- Deguen, R., 2013. Thermal convection in a spherical shell with melting/freezing at either or both of its boundaries, *J. Earth Sci.*, 24, 5, 669-682.
- Deguen, R., Alboussière, T. & Cardin, P., 2013. Thermal convection in Earth's inner core with phase change at its boundary, *Geophys. J. Int.*, 194, 3, 1310-1334.
- Deguen, R. & Cardin, P., 2011. Thermochemical convection in Earth's inner core, *Geophys. J. Int.*, 187, 3, 1101-1118.
- Lin, J.-R., Gerya, T.V., Tackley, P.J., Yuen, D.A. & Golabek, G.J., 2009. Numerical modeling of protocore destabilization during planetary accretion: Methodology and results, *Icarus*, 204, 2, 732-748.
- Takehiro, S., 2011. Fluid motions induced by horizontally heterogeneous Joule heating in the Earth's inner core, *Phys. Earth Planet. Int.*, 184, 3-4, 131-142.
- Takehiro, S., 2015. Influence of surface displacement on solid state flow induced by horizontally heterogeneous Joule heating in the inner core of the Earth, *Phys. Earth Planet. Int.*, 241, 15-20.

6. Besides of comments on technical issues mentioned above, the first issue was how to address rheological properties of inner core material, i.e, iron-nickel alloy. Author used the simple temperature-dependent viscosity based on numerical mantle convection simulation but not quite sure if this type of rheological properties could be applicable for the inner core material or not. Please give

appropriate references in the manuscript with some justification why the inner core rheology could be similar to that of the mantle one.

[Reply] I could not find appropriate references for rheology of the inner core material, i.e, iron-nickel alloy, except Karato's textbooks [2003; 2008], but The essence of the viscosity equation in Eq. (15) is just a simple relationship between the temperature and viscosity under the assumption that non-Newtonian rheology does not work in the iron-nickel alloy unlike in the rocky mantle I have explicitly mentioned this point in Section 2.

7. The second issue in this manuscript was a treatment of inner core growth model – Author assumed that the energy releases caused by latent heat and gravitational energy were IGNORED because they were secondary effects (see eq. (8)). To understand inner core growth itself, the energy balance should be SATISFIED even if they were secondary effects. Why did author ignore those two important energy resources in the core evolution system? I could not find it in the manuscript. Thus, I demand author to give sufficient justifications (explanations) on reason that those could be ignored because I could not get explanations or justifications in the manuscript.

[Reply] Yes, this issue is raised by another reviewer, who gave me appropriate references (below) required for discussion. First, “the heat source associated with solidification of the inner core are ignored because these effects play a secondary role in the growth of the inner core” in the original manuscript have been removed because there is a possibility to mislead the readers. Next, I have modified the relevant sentences in Section 2 to clarify that most of other studies kept these effect. For example, the modeling studies of the core evolution by Gubbins et al. (2003) and Nimmo et al. (2004) revealed that the latent heat plus gravitational energy is larger than the specific heat for the present Earth, and once the inner core starts to freeze, the core temperature decreases significantly with time, which has probably influence on the growth speed of the inner core and the generation and maintenance of geodynamo. The added references for discussion are as follows:

-Gubbins, D., Alfè, D., Masters, G., Price, G.D. & Gillan, M.J., 2003. Can the Earth's dynamo run on heat alone?, *Geophys. J. Int.*, **155**, 2, 609-622, doi:10.1046/j.1365-246X.2003.02064.x.

- Nimmo, F., Price, G.D., Brodholt, J. & Gubbins, D., 2004. The influence of potassium on core and geodynamo evolution, *Geophys. J. Int.*, **156**, 2, 363-376, doi:10.1111/j.1365-246X.2003.02157.x.

8. Third issue is about the comparison between previous studies finding the ‘translational regime’ and author’s model result. L.5 to L.13 of page 3228 was absolutely unclear to me. As far as I understood, the degree one convection generated from lateral viscosity variation such like ‘Sluggish Lid Regime’ would be alternative idea compared to the ‘translational regime’ (=this second form). As discussed the following paragraph (pointed out the next comments), the

formation time-scale of degree one convection would be ~ 3.0 Gyr from author's model simulations, which would be much longer timescale than the age of the inner core, thus translational regime would be STILL one great candidate for understanding to find out the large-scale seismic heterogeneity (anisotropy) observed in the inner core. Such a logical flow seems to be an ethic of self-denial, which means that this type of simulation of convection in the inner core by the author would NOT be worth investigating. To get more worth doing, author should change his boundary conditions on both mechanical and thermal (similar boundary condition to other groups' studies instead of impermeable boundary condition) as well as laterally heterogeneous heat flux condition at ICB should be applied if mantle heat flux pattern could be transparent to the ICB suggested from 'top-down hemispherical dynamics'. If author could do these stuffs, author's results might be more comparable with other investigations to check if the 'translational regime' would be a strong candidate or not. Again, the author should avoid the singularity in his model at the center of the inner core.

[Reply] Again, thank you for your comment. On the lack and limitation of the present simple numerical model, in particular, boundary condition problem, I have further expanded the discussion in Section 4. Again, on the singularity problem, no worries as stated above. Next, about the sluggish lid regime and translational regime, the degree-one thermal structure of mantle convection that lies between the mobile-lid regime and the stagnant-lid regime. In 3-D spherical convection, the sluggish lid regime are replaced by degree-two or degree-one convection with increasing degree of the temperature-dependence of viscosity (e.g., Yoshida and Kageyama, 2004 in GRL, 2006 in JGR; McNamara and Zhong, 2005 in GRL). In this study, I show that the degree-one thermal/mechanical structure is only appeared for a limited range of parameter values for lateral viscosity variations. If the value of the total CMB heat flow is significantly larger than that used in this study, the possibility of the formation of degree-one structure by an endogenic factor due to rheological heterogeneity becomes less likely, because it takes c. 3.0 Gyr to form the degree-one structure. I have emphasized this point in new Section 5.

9. Forth issue is about the age of the inner core. Looking at Figure 3, the inner core has already grown 714.3 km at $t = 3.0$ Ga. It seems for author to integrate 0 to 4.6 Gyr in his model. This is very odd because, as quoted by the author, the age of inner core would be less than 1.3 Ga to 2.0 Ga with referring some literatures. Why did the author decide to integrate over 4.6 Gyrs? To be more comparable for other studies, again, author should improve his own boundary condition. In addition to that comment, author ignored a bunch of literatures by S. Labrosse and F. Nimmo as well as by C. Davis. I do think that their accomplishments would be quite important for both evolution and dynamics of the inner core. To behave a fairplay in the scientific research, the author should not ignore those important literatures to cite in his manuscript. They are really IMPORTANT for discussing the thermal history of Earth's core and its influence to the inner core dynamics. Please cite them and add appropriate discussion.

[Reply] I totally agree your comment and regret the missing references on the young inner core age estimated from paleomagnetic and geodynamics studies. In Section 4, I have expanded the discussion about this point and added new references below:

- Biggin, A.J., Piispa, E.J., Pesonen, L.J., Holme, R., Paterson, G.A., Veikkolainen, T. & Tauxe, L., 2015. Palaeomagnetic field intensity variations suggest Mesoproterozoic inner-core nucleation, *Nature*, 526, 245-248.
- Davies, C.J., 2015. Cooling history of Earth's core with high thermal conductivity, *Phys. Earth Planet. Int.*, 247, 65-79.
- Labrosse, S., Poirier, J.-P. & Mouël, J.-L.L., 2001. The age of the inner core, *Earth Planet. Sci. Lett.*, 190, 3-4, 111–123.
- Nimmo, F., Price, G.D., Brodholt, J. & Gubbins, D., 2004. The influence of potassium on core and geodynamo evolution, *Geophys. J. Int.*, 156, 2, 363-376.

10. Additional idea for understanding the seismic heterogeneity in the inner core would be caused by the magnetic field – Please check literatures by Takehiro [2011; 2015 both in PEPI] and Lasbleis et al. [2015 in GJI] and author should discuss effects of magnetic field with his simulation results without the magnetic field effects. Here I listed 10 significant and critical points that author should address getting the revised manuscript. Since I think that a bunch of additional works and model validations should be done by author to get the revised version of manuscript and it would take a long time, I would not give any detailed comments here (line-by-line comments). Nevertheless, those comments would be useful for getting revised manuscript done by the author.

[Reply] Thank you very much for your comment. As pointed out by the reviewer, some authors suggested that the hemispheric seismic heterogeneity in the inner core would be caused by the magnetic field (Takehiro 2011; Lasbleis et al. 2015; Takehiro 2015). The effects of magnetic field on the 3D numerical model of thermal convection in the growing inner core should be investigated in future. As a start, we are developing a new 3-D numerical simulation code for multiple-layered thermal convection with a large viscosity contrast among each layer, considering the methodology used in the present study and several issues discussed in this Section. The relationship between the degree-one thermal convection and characteristic of geomagnetic field may be an interesting topic not only in earth science but also in computational fluid dynamics. I have expanded the discussion in Section 4 and, following your suggestion, I have cited the following papers:

- Lasbleis, M., Deguen, R., Cardin, P. & Labrosse, S., 2015. Earth's inner core dynamics induced by the Lorentz force, *Geophys. J. Int.*, 202, 1, 548-563.
- Takehiro, S., 2011. Fluid motions induced by horizontally heterogeneous Joule heating in the Earth's inner core, *Phys. Earth Planet. Int.*, 184, 3-4, 131-142.
- Takehiro, S., 2015. Influence of surface displacement on solid state flow induced by horizontally heterogeneous Joule heating in the inner core of the Earth, *Phys. Earth Planet. Int.*, 241, 15-20.

[Reply] I again deeply appreciate you for the careful reading and significant improvement of this paper. I will accept all of the valuable reviewer's comments with sincerely and would like to use these comments to improve the numerical model in future.

Masaki Yoshida

1 **A simple 3D numerical model of thermal convection in Earth's growing inner core:**
2 **On the possibility of the formation of the degree-one structure with lateral**
3 **viscosity variations**

4
5 Masaki Yoshida

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7 *Department of Deep Earth Structure and Dynamics Research, Japan Agency for*
8 *Marine–Earth Science and Technology (JAMSTEC), 2-15 Natsushima-cho, Yokosuka,*
9 *Kanagawa 237-0061, Japan. E-mail: myoshida@jamstec.go.jp*

10
11 Corresponding author: M. Yoshida (myoshida@jamstec.go.jp)

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15
16 **Abstract**

17
18 An east–west hemispherically asymmetric structure for Earth's inner core has been
19 suggested by various seismological evidence, but its origin is not clearly understood. Here,
20 to investigate the possibility of an “endogenic origin” for the degree-one
21 thermal/mechanical structure of the inner core, I performed new numerical simulations
22 of thermal convection in the growing inner core. A setup value that controls the viscosity
23 contrast between the inner core boundary and the interior of the inner core, $\Delta\eta_T$, was taken
24 as a free parameter. Results show that the degree-one structure only appeared for a limited
25 range of $\Delta\eta_T$; such a scenario may be possible but is not considered probable for the real
26 Earth. The degree-one structure may have been realized by an “exogenous factor” due to
27 the planetary-scale thermal coupling among the lower mantle, the outer core, and the inner
28 core, not by an endogenic factor due to the internal rheological heterogeneity.

29
30 **Key words:** numerical simulation; inner core; thermal convection; degree-one structure;
31 east–west hemispherical structure; viscosity variation

32
33
34 **1 Introduction**

35
36 After the segregation of the rocky mantle and molten iron core in the early stage of

37 Earth's formation (e.g., Stevenson 1981), the inner core was formed by gradual
38 solidification of the molten iron core and the size increased with age (Jacobs 1953; Buffett
39 *et al.* 1992) (for example, see reviews by Buffett (2000) and Sumita and Yoshida (2003)).
40 The solidification of the solid core could affect the vigor of outer-core convection owing
41 to the release of latent heat and the passage of light elements toward the liquid outer core
42 (e.g., Sumita & Yoshida 2003). The resulting growth of the inner core may have changed
43 the convection style in the outer core and affected the intensity of Earth's magnetic field
44 throughout Earth's history.

45 Although the structure of the present inner core cannot be inferred from surface
46 geophysical observations, various seismological evidence suggests that the inner core has
47 an east–west, hemispherically asymmetric structure in terms of seismic velocity,
48 anisotropy, and attenuation (Tanaka & Hamaguchi 1997; Creager 1999; Niu & Wen 2001;
49 Cao & Romanowicz 2004; Deuss *et al.* 2010; Irving & Deuss 2011; Waszek *et al.* 2011;
50 Lythgoe *et al.* 2014) (see also a recent review by Tkalčić (2015)).

51 Previous numerical simulations of Earth's mantle convection clarified that for
52 convecting rocky materials confined in a spherical shell, the spherical harmonic degree-
53 one structure was observed for a relatively wide range of the parameter that controls the
54 lateral viscosity variations due to temperature variations (McNamara & Zhong 2005;
55 Yoshida & Kageyama 2006). This is because when the temperature-dependence of
56 viscosity is moderate, the highly viscous lid that develops at the surface of the convecting
57 mantle has the longest-wavelength scale, and the dynamic instability at the bottom of the
58 lid concentrates in one area. This scenario characterizes the degree-one thermal structure
59 of mantle convection that lies between the “mobile-lid regime” with weakly temperature-
60 dependent viscosity and the “stagnant-lid regime” with strongly temperature-dependent
61 viscosity (Yoshida & Kageyama 2006).

62 It is possible that the degree-one seismic structure in the present inner core originated
63 from lateral temperature variations, which in turn originated from lateral viscosity
64 variations. Even given the uncertainties in the rheological properties and composition of
65 the inner core materials, lateral viscosity variation offers considerable potential as an
66 “endogenic factor” that may explain the formation of the degree-one seismic structure. It
67 is therefore worth examining whether a degree-one thermal/mechanical structure
68 generated from the lateral viscosity variations can be realized for solid materials confined
69 in a sphere. This topic had not been investigated in previous numerical simulation models
70 of inner core convection (Deguen & Cardin 2011; Cottaar & Buffett 2012; Deguen 2013;
71 Deguen *et al.* 2013).

72 In this study, to explore the time-dependent behavior of the convection regime in

73 Earth's growing inner core and the possibility of generating the degree-one
 74 thermal/mechanical structure from the internal rheological heterogeneity, a new simple
 75 numerical model of the growing inner core is constructed and a series of numerical
 76 simulations of thermal convection are performed, assuming that the solidification of the
 77 liquid core started at 4.5 Ga and that the radius of the inner core gradually increased with
 78 the square root of age.

79

80 **2 Model**

81

82 Convection in the inner core is computed numerically using a staggered grid-based,
 83 finite-volume code, ConvGS (e.g., Yoshida 2008). The material of the inner core is
 84 modeled as a Boussinesq fluid with an infinite Prandtl number confined in a sphere and
 85 modeled in spherical coordinates (r, θ, ϕ) . Impermeable, shear-stress-free, isothermal
 86 conditions are imposed on the inner core boundary (ICB) with a fixed dimensionless
 87 radius of $r_c' = 1$ (Fig. 1a). The driving force of convection is primordial heat alone because
 88 the radiogenic heat production is negligibly small in the inner core (e.g., Karato 2003)
 89 (see also below). The number of computational grids is taken as $64 (r) \times 64 (\theta) \times 192 (\phi)$
 90 $\times 2$ (for Yin and Yang grids) (Yoshida & Kageyama 2004). To avoid the mathematical
 91 singularity at the Earth's center, an extremely small virtual-sphere with a dimensionless
 92 radius of $r_\delta' = 10^{-6}$ is imposed at the center of the model sphere. For the purpose of
 93 computational convenience, impermeable, shear-stress-free, adiabatic conditions are
 94 imposed on the top boundary of the small sphere. However, this setup does not mean the
 95 existence of the real singularity that violates the mass and heat transport near the center
 96 of the model sphere.

97 Following standard techniques for mantle convection simulations (e.g., Schubert *et al.*
 98 2001), the length L , time t , velocity vector \mathbf{v} , stress tensor (or pressure) $\boldsymbol{\sigma}$, viscosity η , and
 99 temperature T are non-dimensionalized as follows:

$$100 \quad L = r_c(t)L', \quad t = \frac{r_c(t)^2}{\kappa_0}t', \quad \mathbf{v} = \frac{\kappa_0}{r_c(t)}\mathbf{v}', \quad \boldsymbol{\sigma} = \frac{\kappa_0\eta_0}{r_c(t)^2}\boldsymbol{\sigma}', \quad \eta = \eta_0\eta', \quad T = \Delta T_0 \cdot T' \quad (1)$$

101 where $r_c(t)$ denotes the time-dependence of the radius of the inner core, which depends
 102 on time (age); κ_0 denotes the reference thermal diffusivity; η_0 , the reference viscosity; ΔT_0 ,
 103 the characteristic temperature variation; and the subscript "0" refers the reference values
 104 for the inner core (Table 1). In these equations, symbols with primes represent
 105 dimensionless quantities.

106 Using these dimensionless factors, the dimensionless conservation equations for mass,

107 momentum, and energy, which govern inner core convection, are expressed as

$$108 \quad \nabla \cdot \mathbf{v} = 0, \quad (2)$$

$$109 \quad -\nabla p + \nabla \cdot \boldsymbol{\tau} + Ra(t)\zeta(t)^{-3}Te_r = 0, \quad \boldsymbol{\tau} = \eta(\nabla \mathbf{v} + \nabla \mathbf{v}^tr) \quad (3)$$

$$110 \quad \frac{\partial T}{\partial t} + \mathbf{v} \cdot \nabla T = \nabla^2 T + H(t)\zeta(t)^{-2}, \quad (4)$$

111 respectively, where p represents the pressure; $\boldsymbol{\tau}$, the deviatoric stress tensor; and e_r , the
 112 unit vector in the radial direction. Primes representing dimensionless quantities are
 113 omitted in Eq. (2)–(4).

114 In the numerical simulation for this study, instead of fixing the dimensionless radius of
 115 the ICB, the radius of the inner core in the thermal Rayleigh number, Ra , the internal heat-
 116 source number, H , and the “spherical-shell ratio”, ζ , depend on age. They are given by

$$117 \quad Ra(t) \equiv \frac{\rho_0 \alpha_0 \Delta T_0 g_0 [r_c(t) - r_\delta]^3}{\kappa_0 \eta_0} = \frac{\rho_0^2 \alpha_0 \Delta T_0 g_0 c_{p0} [r_c(t) - r_\delta]^3}{k_0 \eta_0},$$

$$H(t) \equiv \frac{\Omega [r_c(t) - r_\delta]^2}{M_m \Delta T_0 \kappa_0 c_{p0}} = \frac{\Omega \rho_0 [r_c(t) - r_\delta]^2}{M_m \Delta T_0 k_0}, \quad (5)$$

$$\zeta(t) \equiv \frac{r_c(t) - r_\delta}{r_c(t)},$$

118 where ρ_0 is the reference density; α_0 , the reference thermal expansion coefficient; ΔT_0 ,
 119 the reference temperature difference across the inner core; g_0 , the reference gravitational
 120 acceleration; c_{p0} , the reference specific heat at constant pressure; k_0 , the reference thermal
 121 conductivity; and M_m , the mass of the mantle (Table 1). **Note that I ignore the secular
 122 cooling of the whole inner core, because the cooling rate and the resulting time change of
 123 the temperature difference across the inner core can not be estimated a priori. However,
 124 the absolute time change in the temperature difference across the inner core should be
 125 small throughout the inner core formation, and the effect of the time change on the
 126 magnitude of thermal Rayleigh number (Eq. 5) is negligibly small compared to other
 127 physical values. Therefore, I consider that this assumption would be justified at least in
 128 the framework of this numerical model (see also discussion in Section 5). Furthermore,
 129 although the gravity acceleration is almost linearly increasing from 0 at the Earth’s centre
 130 to $\sim 4.4 \text{ m s}^{-2}$ at the present ICB (Dziewonski & Anderson 1981), I treated it as a constant
 131 with radius for the simplicity.**

132 Thermal conductivity has received a lot of attention in recent mineral physics studies,
 133 and the main finding is that it may be much larger than the value of $36 \text{ W m}^{-1} \text{ K}^{-1}$ from
 134 Stacey and Davis (2008), i.e., $100\text{--}200 \text{ W m}^{-1} \text{ K}^{-1}$ (de Koker *et al.* 2012; Pozzo *et al.*

135 2012, 2014). Therefore, two end-member models with $k_0 = 36$ and $200 \text{ W m}^{-1} \text{ K}^{-1}$ are
 136 investigated in this study.

137 Because the radioactive potassium may be major heat source in the inner and outer
 138 core, and there is a large possibility that the role of potassium is important in determining
 139 the history of growth of inner core and geodynamo power (e.g., Nimmo *et al.* 2004).
 140 However, I ignore explicitly radioactive heating in the present model because the amount
 141 of radioactive potassium in the inner and outer core would be still under the debate in
 142 mineral physics, geodynamics, geomagnetism and seismological communities, and
 143 instead consider primordial heating in the heat source term of the conservation equation
 144 of energy. This is because the temperature the inner core is normalized by the
 145 characteristic temperature variation, although there is another way for normalizing the
 146 temperature the inner core by the amount of heat production.

147 The amount of approximated primordial heat that has existed since Earth's formation,
 148 Ω , is taken as a free parameter estimated from the heat released by mantle cooling in the
 149 present Earth (Turcotte & Schubert 2014):

$$150 \quad \Omega = -\frac{4}{3} \pi r_e^3 \rho_e c_{pe0} \left. \frac{dT}{dt} \right|_{t=t_0}, \quad (6)$$

151 where r_e is the radius of Earth; ρ_e , the average density of Earth; and c_{pe0} , the average
 152 specific heat at constant pressure for Earth. Here $dT/dt|_{t=t_0}$ is the present cooling rate
 153 of the mantle (Turcotte & Schubert 2014):

$$154 \quad \left. \frac{dT}{dt} \right|_{t=t_0} = -3\lambda \left(\frac{RT_m^2}{E_a} \right), \quad (7)$$

155 where λ is the average radiogenic decay constant in the mantle; R , the gas constant, T_m ,
 156 the mean mantle temperature; and E_a , the activation energy of dry olivine. Using the
 157 values in Table 1, Ω is 11.3 TW, which is a reasonable value compared with the total heat
 158 release by mantle cooling estimated from a global heat-flow balance (Lay *et al.* 2008).

159 Following the work of Buffett *et al.* (1992), who studied an analytical model for
 160 solidification of the inner core, the global heat balance of the outer core is

$$161 \quad \frac{4\pi}{3} (r_b^3 - r_c^3) \rho_c \frac{dT_s(r)}{dt} = 4\pi r_c^2 f_i(t) - 4\pi r_b^2 f_m(t), \quad (8)$$

162 where $T_s(r)$ is the ‘‘solidification temperature’’, and $f_i(t)$ ($\equiv F_i(t)/(4\pi r_c^2)$) and $f_m(t)$
 163 ($\equiv F_m(t)/(4\pi r_b^2)$) are the heat fluxes across the ICB and the core-mantle boundary (CMB),
 164 respectively (Fig. 1b). The potential temperature in the well-mixed liquid outer core is

165 assumed to be spatially uniform and slowly decreases with time, and the ICB is assumed
 166 to be in thermodynamic equilibrium with the surrounding liquid. Under these assumptions,
 167 the temperature through the outer core is uniquely defined by the solidification
 168 temperature, $T_s(r)$, as a function of pressure or depth (see the explanation in Buffett *et al.*
 169 (1992) for details). Here, the heat sources associated with solidification of the inner core
 170 (i.e., the release of latent heat and gravitational energy) are ignored. **Although Buffett *et***
 171 ***al.* (1992) implicitly evaluated that these effects play a secondary role in the growth of**
 172 **the inner core, most of other studies kept these effect. For example, the modeling studies**
 173 **of the core evolution by Gubbins *et al.* (2003) and Nimmo *et al.* (2004) revealed that the**
 174 **latent heat plus gravitational energy is larger than the specific heat for the present Earth,**
 175 **and once the inner core starts to freeze, the core temperature decreases significantly with**
 176 **time, which has probably influence on the growth speed of the inner core and the**
 177 **generation and maintenance of geodynamo.**

178 According to Eq. (4) in Buffett *et al.* (1992), the radial dependence of T_s is expressed
 179 as

$$180 \quad T_s(r) = T_s(0) - \frac{2\pi}{3} G \rho_0^2 r^2 \frac{\partial T_s}{\partial p}, \quad (9)$$

181 where G is the gravitational constant, and $\partial T_s / \partial p$ is the solidification profile (Table 1).

182 Substituting Eq. (9) into Eq. (8), an expression for the radius of the inner core is
 183 obtained:

$$184 \quad r_c(t) = r_b \left[\frac{1}{4\pi r_b^2 N} \int_0^t F_m(t) dt \right]^{\frac{1}{2}}, \quad (10)$$

185 where the model constant N is expressed as

$$186 \quad N = \frac{2\pi}{9} r_b^3 c_{p0} \rho_0^2 G \frac{\partial T_s}{\partial p}. \quad (11)$$

187 Assuming that the heat flux across the CMB is constant throughout Earth's history
 188 (Buffett *et al.* 1992), a model constant, F_m' , is obtained:

$$189 \quad F_m' = \frac{4\pi N}{t} (r_c - r_c^i)^2, \quad (12)$$

190 where r_c^i is an arbitrary value that represents the initial radius of the inner core at the
 191 beginning of the simulation. When the age of Earth's core is assumed to be 4.5 Ga (Lister
 192 & Buffett 1998), the solidification of the inner core is assumed to have begun at this age,
 193 and r_c^i is taken to be 21.5 km so that $r_c - r_c^i$ is exactly 1200 km, F_m' is 2.56×10^{12} W, which
 194 would be a lower limit value for the real Earth considering an even relationship between
 195 the total plume buoyancy flux observed at the Earth's surface and the inferred total CMB

196 heat flow (e.g., Davies 1988; Sleep 1990; Davies & Richards 1992). Eq. (12) indicates
 197 that the relationship between the total CMB heat flow and the radius of the growing inner
 198 core is $F_m' \propto r_c'^2$, which means that the radius of the inner core is proportional to the square
 199 root of F_m' . It should be noted that there is a trade-off between the choices of F_m' and $r_c'^i$,
 200 which are critical for identifying the age of the present-day inner core in the real Earth.
 201 In the present model, I set $r_c'^i$ to a significantly small value to see the behavior of inner
 202 core convection over the longest geological time, i.e., 4.5 Gyr (see Section 4 for
 203 discussion).

204 Finally, the time-dependent radius of the growing inner core used in the present
 205 simulation is expressed as

$$206 \quad r_c'(t) = \left(\frac{F_m' \bar{t}}{4\pi N} \right)^{\frac{1}{2}} + r_c'^i, \quad (13)$$

207 where the dimensional time is scaled as $\bar{t} = (\bar{r}_c'(t)^2 / \kappa_0) \cdot t'$ using the radius of the inner
 208 core at the previous time step of the simulation, $\bar{r}_c'(t)$. Eq. (13) means that r_c' increases
 209 with the square root of age, and eventually reaches $r_c' = 1221.5$ km after 4.5 Gyr, which
 210 matches the present radius of Earth's inner core.

211 At the beginning of the simulation, the initial condition for dimensionless temperature
 212 with significant small-scale lateral perturbations is given as

$$213 \quad T'(r, \theta, \phi) = 0.5 + \omega \cdot Y_{34}^{17}(\theta, \phi) \cdot \sin \left[\pi \frac{r_1' - r'}{r_1'} \right], \quad (14)$$

214 where $Y_{\ell}^m(\theta, \phi)$ is the fully normalized spherical harmonic function of degree ℓ and
 215 order m and $\omega (=0.1)$ is the amplitude of perturbation.

216 The viscosity of the inner core materials, η_T' , in this model depends on temperature
 217 according to a dimensionless formulation (Yoshida 2014):

$$218 \quad \eta_T' = \eta_0' \cdot \exp \left[2T_{ave}'(t) \left(\frac{E'}{T' + T_{ave}'(t)} - \frac{E'}{2T_{ave}'(t)} \right) \right], \quad (15)$$

219 where $T_{ave}'(t)$ is the dimensionless average temperature of the entire sphere at each time
 220 step. A model parameter, E' , controls the viscosity contrast between the ICB with $T' = 0$
 221 and the interior of the inner core. In the present model, $E' = \ln(\Delta\eta_T)$ varies from $\ln(10^0)$
 222 $= 1$ (i.e., no laterally variable viscosity) to $\ln(10^5) = 11.51$. **The essence of the viscosity**
 223 **equation in Eq. (15) is just a simple relationship between the temperature and viscosity**
 224 **under the assumption that non-Newtonian rheology does not work in the iron-nickel alloy**

225 unlike in the rocky mantle (e.g., Karato 2003, 2008).

226

227 **3 Results**

228

229 Fig. 2 shows the time evolution of the convection pattern in the inner core for models
230 with $\eta_0 = 10^{17}$ Pa s, $k_0 = 36$ W m⁻¹ K⁻¹, and with $\Delta\eta_T = 10^0$ (Fig. 2a–d), $\Delta\eta_T = 10^3$ (Fig.
231 2e–h), $\Delta\eta_T = 10^{3.5}$ (Fig. 2i–l), and $\Delta\eta_T = 10^4$ (Fig. 2m–p). When $\Delta\eta_T = 10^0$ (i.e., the
232 viscosity of the inner core is homogeneous) the convection pattern kept a short-
233 wavelength structure over almost all of the simulation time and the “present” inner core
234 at 0.0 Ga has numerous downwellings uniformly distributed in the sphere (Fig. 2d). On
235 the other hand, when $\Delta\eta_T$ is large enough to make the surface thermal boundary layer
236 stagnant ($\Delta\eta_T \geq 10^4$), the convection pattern tends towards a short-wavelength structure
237 with age, and secondary cold plumes from the bottom of the highly viscous lid are evenly
238 distributed in the sphere (Fig. 2p). A remarkable change in the convection pattern is found
239 for moderate values of $\Delta\eta_T$: when $\Delta\eta_T = 10^3$ and $10^{3.5}$, the convection patterns shift
240 towards a long-wavelength structure with increasing age, and eventually the longest-
241 wavelength thermal structures develop for the inner core at 0.0 Ga (Fig. 2h, 2l)

242 To quantitatively assess the variations in thermal and mechanical heterogeneities in the
243 inner core with time, Fig. 3 shows the power spectra of the temperature and root-mean-
244 square velocity fields throughout the modelled inner core at each time step. On the other
245 hand, when $\Delta\eta_T$ is $\leq 10^{2.5}$, it is found that the scales of the thermal and mechanical
246 heterogeneities generally tend to shorten with increasing age, although long-wavelength
247 structures develop just after the beginning of the simulation (“A” in Fig. 3a, c) in spite of
248 an initial temperature condition with a short-wavelength structure (Eq. (14)). When $\Delta\eta_T$
249 is moderate (i.e., $\Delta\eta_T = 10^3$ and $10^{3.5}$) it appears that the scales of the thermal and
250 mechanical heterogeneities generally tend to shorten with increasing age before c. 2.0 Ga,
251 but the degree-one structure begins to develop after 1.0 Ga (see “B” in Fig. 3e–h).

252 Even when $\eta_0 = 10^{16}$ Pa s and $k_0 = 36$ – 200 W m⁻¹ K⁻¹, these conclusions remain
253 essentially unchanged: the degree-one thermal/mechanical structure only appeared for a
254 limited range of parameter values for lateral viscosity variations, i.e., $\Delta\eta_T = 10^4$ and $10^{4.5}$
255 for the model with $k_0 = 36$ W m⁻¹ K⁻¹ (“A” in Fig. 4) and $\Delta\eta_T = 10^3$ and $10^{3.5}$ for the
256 model with $k_0 = 200$ W m⁻¹ K⁻¹ (“A” in Fig. 5). These results imply that the degree-one
257 structure is found in the models with a wide range for the Rayleigh number, as also shown
258 in mantle convection simulations (McNamara & Zhong 2005; Yoshida & Kageyama
259 2006).

260 This degree-one convection pattern is similar to the familiar “sluggish-lid regime” or

261 the “transitional regime” in thermal convection of the mantle that has already been found
262 in numerical simulations of mantle convection (e.g., Solomatov 1995) (Fig. 6b). In this
263 regime, the flow velocities of downwelling plumes from the sluggish-lid are large
264 compared with the interior of the inner core, and the global flow pattern in the sphere
265 corresponds to the temperature distribution. This is because temporal changes in thermal
266 heterogeneity roughly correlate with those in mechanical heterogeneity, as shown in Fig.
267 3, 4 and 5. Also, once the degree-one structure is formed, the sluggish-lid regime
268 generates the largest magnitude of flow velocity and the most laterally heterogeneous
269 velocity field in the inner convecting region (Fig. 6b and 7a) when compared with other
270 regimes such as the mobile-lid regime (Fig. 6a) and the stagnant-lid regime (Fig. 7b).

271 When $\Delta\eta_T$ is 10^4 or larger, the scales of the thermal and mechanical heterogeneities
272 under the stagnant-lid, whose thickness is approximately 100 km, are quite small (the
273 dominant degrees are below 16) even after 4.5 Gyr (Fig. 3i–l). Although the relatively
274 long-wavelength mode is intermittently dominant during the simulation even when $\Delta\eta_T$
275 is quite large (“C” in Fig. 3k–l), it is immediately damped over a short time-scale of $\leq c.$
276 0.5 Gyr. As a result, the stagnant-lid regime is maintained for almost the entire simulation
277 time.

278

279 **4 Discussion**

280

281 The degree-one structure of the inner core suggested by various seismological evidence
282 may have been realized by an “exogenous factor” from outside the ICB, rather than by an
283 “endogenic factor” due to the internal rheological heterogeneity. **The** exogenous origin
284 for the hemispherically asymmetric structure of the inner core and the related
285 hemispherical difference in the degree of crystallization, i.e., freezing and melting, of the
286 inner core materials is consistent with a previous suggestion that planetary-scale thermal
287 coupling among the lower mantle, the outer core, and the inner core plays a primary role
288 in the growth and evolution of the inner core (Aubert *et al.* 2008; Gubbins *et al.* 2011;
289 Tkalčić 2015). More recently, a new isotopic geochemical analysis study (Iwamori &
290 Nakamura 2015; Iwamori *et al.* 2015) revealed that such planetary-scale thermal coupling
291 operates in the whole-Earth system through so-called “top-down hemispheric dynamics”,
292 in which the hemispheric supercontinent-ocean distribution at Earth’s surface controls the
293 thermal convection system in the whole Earth via the mantle, outer core, and inner core
294 over the course of Earth’s history (see Fig. 13 of Iwamori and Nakamura (2015)).

295 It should be noted that the style of convection envisioned in this study is only one form
296 of degree-one convection. Another form involves melting and solidification processes at

297 the ICB, as suggested by Alboussière *et al.* (2010) and Monnereau *et al.* (2010), who
298 concluded that the inner core translates laterally as a rigid body and the return flow
299 effectively occurs in the fluid outer core. Because the present study adopts impermeable
300 boundary conditions at the ICB, this second form of degree-one convection is not
301 permitted. This scenario provides a strong alternate candidate for the form of degree-one
302 convection through top-down hemispheric dynamics, if degree-one convection due to
303 internal rheological heterogeneity is not possible. As another new idea, some authors
304 suggested that the hemispheric seismic heterogeneity in the inner core would be caused
305 by the magnetic field (Takehiro 2011; Lasbleis *et al.* 2015; Takehiro 2015). The effects
306 of magnetic field on the 3D numerical model of thermal convection in the growing inner
307 core should be investigated in future. As a start, we are developing a new 3-D numerical
308 simulation code for multiple-layered thermal convection with a large viscosity contrast
309 among each layer, considering the methodology used in the present study and several
310 issues discussed in this Section. The relationship between the degree-one thermal
311 convection and characteristic of geomagnetic field may be an interesting topic not only
312 in earth science but also in computational fluid dynamics.

313 The age of the inner core is one of the most controversial issues in Earth Science. As
314 mentioned in Section 2, the value of the total heat flow at the CMB is a key parameter
315 that controls the speed of growth of the inner core. A previous study (Cottaar & Buffett
316 2012) has shown that the minimum heat flow for inner core convection is 4.1 TW, giving
317 a maximum inner core age of 1.93 Ga. Heat flow greater than 6.3 TW leads to the present
318 convection regime, but the inner core age is then less than 1.26 Ga. Following their
319 analysis, if the total CMB heat flow is c. 5–15 TW (Lay *et al.*, 2008 and references therein),
320 the age of inner core should be younger (i.e., less than 1 Ga). If the value of the total CMB
321 heat flow is significantly larger than that used in this study, the possibility of the formation
322 of degree-one structure by an endogenic factor due to rheological heterogeneity becomes
323 less likely, because it takes c. 3.0 Gyr to form the degree-one structure when $\eta_0 = 10^{17}$ Pa
324 s, $k_0 = 36 \text{ W m}^{-1} \text{ K}^{-1}$, and $\Delta\eta_T$ is 3.5 (Fig. 3g). At the very least, the conclusion that the
325 convective motion in the inner core is maintained even for the present Earth can be drawn
326 from the models studied here.

327 Almost all of recent paleomagnetic and geodynamics studies have suggested that the
328 age of inner core would be less than 1.3 Ga to 2.0 Ga (Labrosse *et al.* 2001; Nimmo *et al.*
329 2004; Davies 2015; Nimmo 2015). According to a more recent paleogeomagnetic study,
330 the inner core formed at ~ 1.5 Ga (Biggin *et al.* 2015). This “young” inner core age is
331 consistent with the indirect evidences from seismology and mineral physics that the CMB
332 heat flow is larger than previously thought (Hernlund *et al.* 2005; Lay *et al.* 2006; van der

333 Hilst *et al.* 2007). In the present numerical model, the CMB heat flow is assumed to be
334 constant, $F_m' = 2.56 \times 10^{12}$ W, based on the model constants used in Buffett *et al.* (1992)
335 and the initial radius of the inner core arbitrarily set. As stated in Section 2, this value
336 would be a lower limit value for the present Earth considering an even relationship
337 between the total plume buoyancy flux observed at the Earth' surface and the inferred
338 total CMB heat flow (e.g., Davies 1988; Sleep 1990; Davies & Richards 1992) and a
339 minimal power requirement for maintenance of the geodynamo (Buffett 2002). However,
340 the CMB heat flow in the past Earth would be lower than that in the present Earth, because
341 the average mantle temperature may increase as the Earth older. More than that, there is
342 a possibility that the CMB heat flow may have a significant variation throughout the
343 Earth's history. Although the implementation of time-dependent CMB heat flow is
344 beyond the framework of the present simple numerical model, it might be a serious
345 problem for the growing speed of the inner core. However, if the inner core grows faster
346 than the present model, the degree-one structure would only appeared for a further limited
347 range of $\Delta\eta_T$ than the results presented in this paper. Therefore I believe that the
348 conclusion on the less possibility of an endogenic origin for the degree-one
349 thermal/mechanical structure of the inner core is justified.

350 Seismic observations provide evidence for a seismic velocity discontinuity about 200
351 km below the ICB separating an isotropic layer in the uppermost inner core from an
352 underlying anisotropic inner core (e.g., Song & Helmberger 1998). The results presented
353 here may imply that this "inner core transition zone" represents the boundary between a
354 sluggish, highly viscous, cold layer and an underlying hot convection region (Fig. 6b and
355 7a). Sumita and Yoshida (2003) predicted that there may be a characteristic structure in
356 the topmost section of the inner core that is similar to the plate tectonic mechanism at
357 Earth's surface, which is explained by the existence of a crust-like, thin, low-degree
358 partial-melting layer and an underlying asthenosphere-like, high-degree partial-melting
359 layer. The ICB is, by definition, at melting temperature, which means that it is possible
360 that the viscosity could be lowest at the top and gradually increase with depth into the
361 interior of the inner core. However, because the temperature across the inner core is never
362 very far from the melting temperature (Stacey & Davis 2008), depending in detail on the
363 contribution from light element impurities, viscosity variations in the underlying hot
364 convection region should be small.

365 Here I need to mention the lack and limitation of the present simple numerical model.
366 First, the framework of present model is based on mantle convection simulations to deal
367 with convection within the growing inner core. In contrast to mantle convection
368 simulations, I used a time-dependent inner core radius to get dimensionless equations Eq.

369 (2–4) to account for the growing inner core. However, Eq. (2-4) is build based on an
370 Eulerian specification that is fixed on space. With increasing inner core radius, the grid
371 is actually slowly expanding through time. Thus, strictly speaking, mass, momentum, and
372 energy may be no longer conserved with this expending grid, although the growth rate
373 could be small enough to make it negligible. However, considering the significant
374 accumulating growth of the inner core during the whole simulation, improvement of the
375 present numerical model should be required.

376 Next, on the issue of secular cooling raised in Section 2, the dimensionless internal
377 heating production shown in Eq. (5) is incomplete because the inner core got cooling
378 down rapidly once the inner core gets started growing in the present model. The exact
379 way is for the secular cooling to be addressed as the boundary condition problem, not the
380 internal heating production, because the initial temperature of inner core should be
381 determined by the solidus temperature of iron-alloy, adiabatic heat flux across the ICB,
382 the latent heat release and gravitational energy caused by light element release.
383 Furthermore, the molten core might have initial accretion energy before the inner core
384 started growing, but not in the inner core. Although the integration of these two serious
385 problem into the present numerical model is numerically difficult and is beyond the
386 present study on the possibility of the formation of the degree-one structure with lateral
387 viscosity variations, they should be considered in the future model.

388

389 **5 Conclusions**

390

391 The systematic numerical simulations conducted in this study investigated the
392 possibility of the formation of a degree-one structure with lateral viscosity variations in
393 thermal convection within the age of Earth for a simulated inner core confined in a sphere.
394 The degree-one thermal/mechanical structure, however, only appeared for a limited range
395 of parameter values for lateral viscosity variations. Considering the uncertainties in the
396 exact magnitude of lateral temperature variations, the rheology, and the composition of
397 Earth's inner core materials, the formation of a degree-one structure with lateral viscosity
398 heterogeneity under the limited geophysical conditions confirmed here would be
399 considered possible but not probable for the real Earth. If the value of the total CMB heat
400 flow is significantly larger than that used in this study, the possibility of the formation of
401 degree-one structure by an endogenic factor due to rheological heterogeneity becomes
402 less likely, because it takes c. 3.0 Gyr to form the degree-one structure. Namely, the
403 degree-one structure of the inner core may have been realized by an “exogenous factor”
404 from outside the ICB, rather than by an “endogenic factor” due to the internal rheological

405 heterogeneity.

406 In future, the evolution of the inner core should be resolved by numerical simulations
407 of the whole-Earth thermal convection system because it is highly possible that the growth
408 rate of the inner core is determined by heat flow at the CMB, which largely depends on
409 the behavior and style of mantle convection (Buffett *et al.* 1992; Sumita & Yoshida 2003).
410 The combined effects of the thermal and compositional buoyancies (Lythgoe *et al.* 2015)
411 and the effects of non-uniform heat flux boundary condition at the ICB, rather than a fixed
412 temperature condition on the style and regime of inner core convection, should also be
413 studied numerically in future.

414

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416

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425

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427

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590

Table 1. Physical parameters for the simulation used in this study.

Symbol	Definition	Value	Unit	Refs.
α_0	Thermal expansion coefficient*	9.74×10^{-6}	K^{-1}	a, b
c_{p0}	Specific heat at constant pressure*	7.03×10^2	$\text{J kg}^{-1} \text{K}^{-1}$	a
g_0	Gravitational acceleration*	4.4002	m s^{-2}	a
ρ_0	Density*	1.27636×10^4	kg m^{-3}	a
k_0	Thermal conductivity*	36 or 200	$\text{W m}^{-1} \text{K}^{-1}$	a/c, d, e
κ_0	Thermal diffusivity*	4.01×10^{-6}	$\text{m}^2 \text{s}^{-1}$	a
η_0	Viscosity*	10^{17} or 10^{16}	Pa s	f
-	Temperatures at the inner core boundary	5000	K	a
ΔT_0	Characteristic temperature variation*	30	K	a
M_m	Mass of the mantle	4.043×10^{24}	kg	g
τ_c	Formation age of the core	4.5	Ga	h
c_{pe0}	Average specific heat at constant pressure for Earth	9.2×10^2	$\text{J kg}^{-1} \text{K}^{-1}$	g
ρ_{e0}	Average density of Earth	5.520×10^3	kg m^{-3}	g
T_m	Mean mantle temperature	2250	K	g
E_a	Activation energy for dry olivine	540×10^3	J mol^{-1}	g, i
λ	Average decay constant for the mixture of radioactive isotopes in the mantle	2.77×10^{-10}	yr^{-1}	g
$dT/dt _{t=t_0}$	Present cooling rate of the mantle	64.7	K Gyr^{-1}	Eq. (7)
G	Gravitational constant	6.67384×10^{-11}	$\text{m}^3 \text{kg}^{-1} \text{s}^{-2}$	g
R	Gas constant	8.3144621	$\text{J mol}^{-1} \text{K}^{-1}$	g
$\partial T_s / \partial p$	Solidification profile	7×10^{-9}	K Pa^{-1}	j, k
r_e	Radius of Earth	6.371×10^6	m	g
r_b	Radius of the outer core	3.48×10^6	m	l
$r_c(t)$	Radius of the inner core	Time-dep.	m	-
r_c	Radius of the present inner	1.2215×10^6	m	l

core				
r_c^i	Initial radius of the inner core	2.15×10^4	m	x
Ω	Model constant (see text)	1.13×10^{13}	W	Eq. (6)
N	Model constant (see text)	2.01×10^{16}	J m^{-2}	Eq. (11)
F_m'	Model constant (see text)	2.56×10^{12}	W	Eq. (12)
<i>Dimensionless parameters</i>				
$Ra(t)$	Thermal Rayleigh number	Time-dep.	-	Eq. (5)
$H(t)$	Internal heat-source number	Time-dep.	-	Eq. (5)
$\zeta(t)$	Spherical-shell ratio number	Time-dep.	-	Eq. (5)

592 Definition: “*” indicates reference values for the inner core. References: a, Stacey and
593 Davis (2008); b, Vočadlo *et al.* (2003); c, de Koker *et al.* (2012); d, Pozzo *et al.* (2012);
594 e, Pozzo *et al.* (2014); f, Karato (2003); g, Turcotte and Schubert (2014); h, Lister and
595 Buffett (1998); i, Karato and Wu (1993); j, Verhoogen (1980); k, Buffett *et al.* (1992); l,
596 Dziewonski and Anderson (1981). “x” indicates arbitrary values (see text).

597

598

599

600 **Figure captions**

601

602 **Figure 1.** (a) Illustration for the numerical model of inner core convection. (b) Schematic
603 profile of the potential temperature in the cooling core of the Earth used in an analytical
604 model for solidification of the inner core (after Buffett et al., 1992). The solid line
605 represents the temperature in the upper part of the thick solid inner core, the liquid outer
606 core, and the lower mantle at some instant. The thick dashed line represents the
607 subsequent evolution of temperature as heat is continuously extracted from the core. Heat
608 fluxes f_m and f_i pertain to the core-mantle and inner-core boundaries (CMB and ICB),
609 respectively. The solidification temperature $T_s(r_c)$ is defined at the ICB, and $T_s(r, t)$ is the
610 temperature within the inner core.

611

612 **Figure 2.** Time evolution of the convection pattern in the inner core for models with η_0
613 $= 10^{17}$ Pa s, $k_0 = 36$ W m $^{-1}$ K $^{-1}$, and (a–d) $\Delta\eta_T = 10^0$, (e–h) $\Delta\eta_T = 10^3$, (i–l) $\Delta\eta_T = 10^{3.5}$,
614 and (m–p) $\Delta\eta_T = 10^4$. Blue and copper isosurfaces indicate regions with lower and higher
615 than average temperatures at each depth. (a–d and m–p) blue: -0.3 K; copper: $+0.3$ K. (e–
616 f and i–k) blue: -0.6 K; copper: $+0.6$ K. (g, h, and l) blue: -1.5 K; copper: $+1.5$ K.

617

618 **Figure 3.** Temporal changes in the heterogeneity of temperature and root-mean-square
619 velocity fields in the inner core for the models with $\eta_0 = 10^{17}$ Pa s, $k_0 = 36$ W m $^{-1}$ K $^{-1}$,
620 and (a–b) $\Delta\eta_T = 10^0$, (c–d) $\Delta\eta_T = 10^2$, (e–f) $\Delta\eta_T = 10^3$, (g–h) $\Delta\eta_T = 10^{3.5}$, (i–j), $\Delta\eta_T = 10^4$,
621 and (k–l) $\Delta\eta_T = 10^5$. The logarithmic power spectra are normalized by the maximum
622 values at each elapsed time. The four black wedges on the panels (a), (e), (g), and (i)
623 represent the ages that correspond to Fig. 2.

624

625 **Figure 4.** Temporal changes in the heterogeneity of temperature and root-mean-square
626 velocity fields in the inner core for the models with $\eta_0 = 10^{16}$ Pa s, $k_0 = 36$ W m $^{-1}$ K $^{-1}$,
627 and (a–b) $\Delta\eta_T = 10^0$, (c–d) $\Delta\eta_T = 10^2$, (e–f) $\Delta\eta_T = 10^3$, (g–h) $\Delta\eta_T = 10^{3.5}$, (i–j), $\Delta\eta_T = 10^4$,
628 and (k–l) $\Delta\eta_T = 10^5$. The logarithmic power spectra are normalized by the maximum
629 values at each elapsed time.

630

631 **Figure 5.** Temporal changes in the heterogeneity of temperature and root-mean-square
632 velocity fields in the inner core for the models with $\eta_0 = 10^{16}$ Pa s, $k_0 = 200$ W m $^{-1}$ K $^{-1}$,
633 and (a–b) $\Delta\eta_T = 10^0$, (c–d) $\Delta\eta_T = 10^2$, (e–f) $\Delta\eta_T = 10^3$, (g–h) $\Delta\eta_T = 10^{3.5}$, (i–j), $\Delta\eta_T = 10^4$,
634 and (k–l) $\Delta\eta_T = 10^5$. The logarithmic power spectra are normalized by the maximum
635 values at each elapsed time.

636

637 **Figure 6.** Cross sections of temperature and velocity fields for the models with $\eta_0 = 10^{17}$
638 Pa s, $k_0 = 36 \text{ W m}^{-1} \text{ K}^{-1}$, and (a) $\Delta\eta_T = 10^0$ and (b) $\Delta\eta_T = 10^3$ at 0.0 Ga. The top panels
639 show the cross sections at the central depth of the inner core (i.e., radius of 610.8 km) and
640 bottom panels show the cross sections cut along the great circles shown by dashed lines
641 in the top panels. The contour interval in the temperature plots is 3 K. These figures
642 correspond to (a) Fig. 2d and Fig. 3a, and (b) Fig. 2h and Fig. 3e.

643

644 **Figure 7.** Cross sections of temperature and velocity fields for the models with $\eta_0 = 10^{17}$
645 Pa s, $k_0 = 36 \text{ W m}^{-1} \text{ K}^{-1}$, and (a) $\Delta\eta_T = 10^{3.5}$ and (b) $\Delta\eta_T = 10^4$ at 0.0 Ga. The top panels
646 show the cross sections at the central depth of the inner core (i.e., radius of 610.8 km) and
647 bottom panels show the cross sections cut along the great circles shown by dashed lines
648 in the top panels. The contour interval in the temperature plots is 3 K. These figures
649 correspond to (a) Fig. 2l and Fig. 3g, and (b) Fig. 2p and Fig. 3k.

650

651