

1 **Structural Disorder of Graphite and Implications for Graphite** 2 **Thermometry**

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10 **Key Points:**

11 graphite, disorder, thermometry, Raman

12 **Abstract**

13 Graphitization, or the progressive maturation of carbonaceous material, is considered an irreversible process. Thus, the
14 degree of graphite crystallinity has been calibrated as an indicator of the peak metamorphic temperatures experienced by the
15 host rocks. However, discrepancies between temperatures indicated by graphite crystallinity versus other thermometers have
16 been documented in deformed rocks. To examine the possibility of mechanical modifications of graphite structure and the
17 potential impacts on graphite 'thermometry' we performed laboratory deformation experiments. We sheared highly
18 crystalline graphite powder at normal stresses of 5 and 25 MPa and aseismic velocities of 1 $\mu\text{m/s}$, 10 $\mu\text{m/s}$ and 100 $\mu\text{m/s}$.
19 The degree of graphite crystallinity both in the starting and resulting materials was analyzed by Raman microspectroscopy.
20 Our results demonstrate consistent decrease of graphite crystallinity with increasing shear strain. Microstructural
21 observations show that brittle processes caused the documented structural disorder of graphite. We conclude that the
22 calibrated graphite 'thermometer' is ambiguous in active tectonic settings and we suggest that a calibration that accounts for
23 shear strain is needed.

24 **1. Introduction**

25 Organic matter, preserved in sedimentary rocks, can be transformed into crystalline graphite due to structural and
26 compositional changes during diagenesis and metamorphism, a process known as graphitization (Bonijoly et al., 1982;
27 Wopenka and Pasteris, 1993; Beyssac et al., 2002a; Buseck and Beyssac, 2014; etc.). Graphitization is thought to be an
28 irreversible process and graphite is known to remain stable to the highest temperatures of granulite facies and the highest
29 pressures of coesite-eclogite facies (Buseck and Beyssac, 2014). It is generally accepted that the degree of graphite
30 crystallinity, or its structural order, is determined mainly by the maximum temperature conditions experienced by the host
31 rocks, whereas lithostatic pressure and shear strain are considered to have only minor influence on graphitization (Bonijoly
32 et al., 1982; Wopenka and Pasteris, 1993; Bustin et al, 1995). Therefore, graphite crystallinity has been calibrated as an
33 indicator of the peak temperatures reached during progressive metamorphism (Beyssac et al., 2002a; Reitmeijer and
34 McKinnon, 1985). However, in strained rocks discrepancies between temperatures indicated by the crystallinity of graphite
35 vs. other thermometers have been reported (Barzoi, 2015; Nakamura et al., 2015; Kirilova et al., in press). Thus, numerous
36 authors have speculated that tectonic deformation results in graphite structural modifications that challenge the validity of
37 the existing graphite thermometers (Large et al., 1994; Bustin et al, 1995; Crespo et al., 2006; Barzoi, 2015; Nakamura et al.,
38 2015).

39 Furthermore, graphite occurrence and enrichment have been documented in several fault zones in the world, e. g. the Alpine
40 Fault zone, New Zealand (Kirilova, et al., in press), the Hidaka metamorphic belt, Hokkaido, Japan (Nakamura et al., 2015),
41 the Atotsugawa fault system, Japan (Oohashi, et al., 2012), the Tanakura Tectonic Line, Japan (Oohashi et al., 2011), the Err
42 nappe detachment fault, Switzerland (Manatschal, 1999), and the KTB borehole, Germany (Zulauf et al., 1990). In these
43 intensely deformed rocks its presence is of particular interest because its low friction coefficient of $\mu \sim 0.1$ (Morrow et al.,
44 2000) allows graphite to act as a natural solid lubricant (Savage, 1948). The mechanical behavior of graphite has been
45 broadly investigated in both natural and experimental specimens, where it manifests with the lowest μ among sheet structure
46 minerals (Moore and Lockner, 2004; Oohashi et al., 2011, 2013; Rutter, et al., 2013; Kuo et al., 2014, etc.) confirming it
47 could have a significant impact on fault mechanics. It has been experimentally proven that even a small fraction of graphite
48 can have a disproportionally large effect on frictional strength where graphite is concentrated by smearing into interlinked
49 layers (Rutter, et al., 2013).

50 However, structural changes in crystalline graphite caused by tectonic deformation have not yet been systematically
51 explored. To examine this aspect and to investigate the potential impacts of structural disordering of graphite on the graphite
52 ‘thermometer’, we have carried out laboratory deformation experiments on highly crystalline graphite powder.

53 2. Experimental methods

54 2.1 Sample description

55 As a starting material in the current study we used synthetic (commercially synthesized) graphitic carbon to avoid
56 complexities arising from variable degree of crystallinity in natural carbon materials. Initially, the material was crushed to
57 maximum grain size of 160 μm in a RockLabs Swing (TEMA) mill. The resulting fine graphitic powder was annealed at
58 700°C for two hours in a Lindberg Blue M Muffle Furnace to achieve full graphitization, which is known to occur at this
59 temperature in the absence of other variations in physical conditions (Buseck and Beyssac, 2014). This was used as the
60 starting material for the deformation experiments.

61 2.2 Experimental procedure

62 In total, 10 deformation experiments were performed at room temperature and room humidity in the Brittle Rock
63 deformAtion Versatile Apparatus BRAVA (Collettini et al., 2014), at INGV, Rome. For each experiment two 3-mm thick
64 layers of synthetic graphite gouges were placed in between three grooved forcing blocks in a double-direct shear
65 configuration (e.g. Dieterich, 1972). The two side blocks are held stationary, and the central forcing block is driven
66 downward causing shear to occur within the graphite gouge layers. Normal stress is applied by the horizontal piston in load-
67 feedback control mode and shear displacement accomplished by the vertical piston in displacement-feedback control mode.
68 Forces are measured with stainless steel load cells (± 0.03 kN) and displacements are measured with LVDTs (± 0.1 μm)
69 attached to each piston. Experiments have been conducted at normal stresses of 5 MPa or 25 MPa and aseismic sliding
70 velocities of 1 $\mu\text{m/s}$, 10 $\mu\text{m/s}$ and 100 $\mu\text{m/s}$. The experiments were carried out to total displacements of 20 mm. In addition,
71 some experiments were stopped at 5 mm and 10 mm and the specimens were then recovered to reveal graphite structural
72 changes that took place during different amounts of total deformation. The coefficient of friction (μ) was calculated as the
73 ratio of measured shear load to measured normal load ($\mu = \tau / \sigma_n$, where τ is shear stress and σ_n is effective normal stress).
74 The average shear strain within the layer was calculated by dividing shear displacement increments by the measured layer
75 thickness and summing. The displacement values of the vertical and horizontal load points were corrected for the elastic
76 stretch of each load frame, taking into account that the machine stiffness is 1283 kN/mm on the horizontal axis and 928.5
77 kN/mm on the vertical axis. In addition, we calculated total frictional work for each experiment as a function of shear stress
78 integrated over the total displacement (Beeler, 2007).

79 2.3 Raman microspectroscopy

80 The degree of graphite crystallinity was measured by an Alpha 300R+ confocal Raman microscope (WITec, Ulm, Germany)
81 with a 532 nm laser (Coherent, Santa Clara, California), located at the Department of Chemistry, University of Otago, New

82 Zealand. The laser (3.0 mW) was focused on the samples with a 50× Zeiss objective. The scattered light was dispersed with
83 a 1200 g/mm grating. The combination of the 50× objective and 532 nm laser wavelength produced a laser spot size of
84 approximately 412 nm in diameter. The integration time of each spectrum was 2 seconds with 50 co-additions (100 seconds
85 in total). The spectra were calibrated using the Raman band from a silicon wafer prior to each set of measurements.

86 The collected spectra were pre-processed in GRAMS AI 9.1 (Thermo Fisher Scientific Inc.), where cosmic spikes were
87 removed and a multi-point linear baseline offset was performed. This was followed by peak fitting three Lorentzian-
88 Gaussian functions to each spectrum with a linear baseline over 1000 - 1700 cm^{-1} . For each spectrum, the area ratio was
89 calculated ($R2 = A_{D1} / (A_G + A_{D1} + A_{D2})$, where A_i is the area of the i th peak, G band is the main high frequency band of
90 graphite, D1 and D2 bands are defect bands observed in the first order Raman spectrum of graphite) (Wopenka and Pasteris,
91 1993; Beyssac et al., 2002a).

92 **2.4 Scanning electron microscopy**

93 Microstructural analyses of the graphite gouge recovered from the biaxial apparatus were carried out using a scanning
94 electron microscope (SEM). Some SEM images were acquired from the shiny surfaces of the graphite layers that had been
95 parallel to the center and or side forcing blocks (Y-Z sections), with a Zeiss Sigma field emission scanning electron
96 microscope (VP FEG SEM) at the Otago Centre for Electron Microscopy (OCEM), University of Otago, New Zealand. The
97 instrument was operated in variable pressure mode (VP) at 15 kV using a working distance (WD) of 7 – 8 mm and a VPSE
98 (VP-mode secondary electrons) detector. In addition, polished thin sections cut perpendicular to the surface of contact with
99 the center and side forcing blocks (X-Z sections) were imaged on a JEOL JSM-6510 SEM at the University of Potsdam,
100 Germany, where high-resolution secondary electron images were collected at 20 kV and a WD of 10 mm.

101 **2.5 Transmission electron microscopy**

102 Transmission electron microscopy (TEM) was used for detailed microstructural characterization of the shiny surfaces. High-
103 resolution TEM images were collected by using a JEM-2010 electron microscope, located at the University of Hokkaido,
104 Sapporo, Japan. The instrument was operated at 200 kV with LaB6 filament. TEM foils (with size of 12 x 5 μm and
105 thickness of 1 μm) milled by FIB perpendicular to the shiny surface (X-Z section) were placed on a carbon coated film, and
106 examined by using dual-axis tilting holder.

107 **3. Results**

108 **3.1 Mechanical data**

109 Our experiments allowed us to investigate graphite mechanical behavior and structural modifications under various sliding
110 velocities, normal stresses and shear strain. These conditions are summarized in Table 1.

111 **3.1.1 Friction variations**

112 Over several mm of displacement, the friction coefficient shows a similar evolution trend in all experiments. On a plot of
113 friction coefficient vs. displacement (Fig. 1a), the friction coefficient (μ) delineates a curve characterized by a rapid increase
114 to an initial peak friction coefficient (μ_{peak}), followed by a subsequent exponential decay towards a steady-state friction
115 coefficient (μ_{ss}) over a slip weakening distance. The shapes of the friction-displacement curves vary with the normal stress
116 applied and are steeper for the experiments conducted at 25 MPa than the ones at 5 MPa (Fig. 1a) i.e. the displacement
117 required to achieve steady-state decreases at higher normal stress. In addition, the values of both μ_{peak} and μ_{ss} (Fig. 1a; Table
118 1) are significantly lower in the experiments at 25 MPa ($\mu_{\text{peak}} = \sim 0.4$; $\mu_{\text{ss}} = \sim 0.1$) than in the experiments at 5 MPa ($\mu_{\text{peak}} =$
119 ~ 0.5 ; $\mu_{\text{ss}} = \sim 0.2$) (where μ_{ss} values were read at the end of each experiment). Plots of μ at all sliding velocities (Fig. 1a)
120 show subtle variations in μ_{peak} and μ_{ss} with change of the applied sliding velocities (Fig. 1a; Table 1).

121 **3.1.2 Shear strain variations**

122 Plots of friction coefficient vs. shear strain (Fig. 1b) show significant variations in shear strain attained over equivalent
123 sliding displacements. The estimated shear strain values are a geometric consequence of different thickness changes.
124 Consideration of the shear strain at equivalent sliding velocities but different normal stresses demonstrates that shear strains
125 achieved during the 5 MPa experiments are approximately half of those at 25 MPa (Fig. 1b; Table 1). In addition, the
126 experiments at 25 MPa demonstrate a dramatic increase in shear strain with increasing slip velocity (Fig. 1b; Table 1),
127 whereas at low normal stress we do not observe any systematic variations associated with changes in sliding velocities (Fig.
128 1b, c and d). Fig. 1c and d show the experiments at low shear strain used to characterize graphite structural changes in the
129 early stages of deformation (Table 1).

130 **3.2 Graphite crystallinity**

131 All the experiments resulted in the development of shiny smooth surfaces with gentle slickenlines (macroscopic fine
132 grooves, parallel to the slip direction as defined by Toy et al., in press). Raman spectra obtained on the top of these surfaces,
133 that had accommodated most of the induced deformation, are compared to Raman spectra from the starting material to
134 identify the effects of mechanical deformation on graphite crystallinity.

135 Raman data from 20 spectra per sample are presented in Supplementary material 1 (S1). Representative spectra for each
136 sample are illustrated in Fig. 2, which shows spectra displaying the least (left column) and the most (right column)
137 disordered graphite within a sample (i.e. lowest and highest R2 values respectively). Spectra that were typical of the average
138 for each sample are also presented (middle column). Experiments 3 and 7 were stopped at only 5 mm displacement and
139 resulted in extremely fragile deformed surfaces, which were unable to be extracted without them breaking into pieces too
140 small to obtain spectra from. Thus, graphite crystallinity was not measured in these experiments.

141 All the acquired spectra show typical G, D1 and D2 bands, respectively at $\sim 1580\text{ cm}^{-1}$, $\sim 1350\text{ cm}^{-1}$ and $\sim 1620\text{ cm}^{-1}$ (S1). The
142 degree of graphite crystallinity in each sample could thus be calculated by using the area ratio R2 (Fig. 2; S1). Raman
143 spectra collected from the starting material show R2 values ranging from 0 to 0.327 (Fig. 2), corresponding respectively to
144 fully crystalline and highly organized graphite. Spectra acquired from the deformed surfaces show higher R2 values (Fig. 2;
145 S1). The most crystalline graphite with R2=0.330 was collected in Exp. 2 (Fig. 2) while the most disordered graphite with
146 R2=0.661 resulted from Exp. 10 (Fig. 2).

147 As graphite crystallinity varies within a sample (Fig. 2; S1), we examine average R2 values for each one and compare them
148 with applied normal stress, sliding velocity, shear strain, and total frictional work (Table 2). The starting material has
149 average $R2_{\text{pre-shear graphite}} = 0.173$, whereas all deformed samples have higher average R2 values (Table 2). Analyzing the
150 average R2 values for deformed samples reveals that graphite is more disordered in the high normal stress experiments
151 (Table 2) than in the experiments at 5 MPa. Furthermore, in the experiments at 25 MPa the average graphite crystallinity
152 decreases with increasing sliding velocities (Table 2). In contrast, at low normal stress, we do not observe any dependence of
153 the degree of graphite crystallinity on the applied sliding velocities (Table 2). Overall graphite appears as most disordered in
154 the experiments where the highest shear strain was achieved (Table 2). The relationship between average R2 and shear strain
155 is illustrated in Fig. 3a by fitting a power function with a correlation coefficient $R^2 = 0.95$. Fitting a power function to
156 average R2 and total frictional force showed a consistent correlation (Fig. 3b). The experiments 2 and 6 at low normal stress,
157 which were stopped at 10 mm displacement and accommodated the least amount of shear strain, contain the least disordered
158 graphite (Fig. 3; Table 2).

159 **3.3 Microstructural characteristics**

160 **3.3.1 Scanning electron microscopy (SEM)**

161 Similar microstructural features were observed in all the deformed samples. SEM images obtained from the sample
162 deformed during experiment 8 are presented to demonstrate our observations (Fig. 4).

163 These high-resolution images in Y-Z sections reveal that the shiny surfaces are decorated by closely spaced (from < 5 to 10
164 micrometers) slickenlines (Fig. 4a), on top of a smooth continuous layer. In places, the continuity of this layer is interrupted
165 by fine (~1 to 2 micrometers in width) fractures (Fig. 4a), with random orientation compared to the slip direction.
166 Occasionally, the deformed surface appears as completely disrupted, and is decorated with smaller graphite grains from 10 to
167 50 micrometers in size, oriented nearly parallel to the shear direction (Fig. 4b). In X-Z sections this highly deformed surface
168 is observed as a thin slip-localized zone, composed of well-compacted layer of aligned graphite grains (Fig. 4c). This
169 localized shear surface is underlain by a zone of randomly oriented, inequigranular, irregular graphite grains (Fig. 4d). In
170 places, most of the graphite grains are aligned with their basal (001) planes parallel to the slip direction, and form compacted
171 layers, defining a weakly-developed fabric (Fig. 4e). There has been some dilation along these cleavage planes, and the
172 spaces thus created are filled with smaller graphite grains with their (001) planes sub-perpendicular to the shear direction
173 (Fig. 4e). Locally, intensely fractured grains are also observed (Fig. 4f).

174 **3.3.2 Transmission electron microscopy (TEM)**

175 TEM was used to examine the microstructure of the material that makes up the shiny surfaces (Fig. 4c). TEM analyses were
176 performed on foils cut perpendicular to this surface. Fig. 5 shows characteristic TEM images obtained from the sample
177 recovered from experiment 8.

178 Graphite grains in this well-compacted layer have basal planes predominantly aligned with the shear plane, as were observed
179 in SEM images. However, adjacent grains show slightly different orientations (Fig. 5a). In addition, kink folded graphite
180 grains are observed in multiple locations in the foils (Fig. 5b, c), which yields a ‘wavy layering’ at a small angle to the shear
181 direction (Fig. 5b). In isolated areas, there are also some smaller grain fragments with random orientation (Fig. 5d).

182 **4. Discussion**

183 **4.1 Mechanical behavior**

184 Graphite in our experiments shows mechanical behavior consistent with other mechanical studies of pure graphite gouges.
185 Our results display low μ_{ss} values (from ~0.1 to ~0.2; Table 1) as did the low-pressure deformation experiments of
186 carbonaceous material performed by Morrow et al. (2000), Moore and Lockner (2004), Oohashi et al. (2011, 2013), Kuo et
187 al. (2014), and Rutter et al. (2013). The low frictional strength of graphite is well known and has been attributed to its sheet
188 structure composed of covalently bonded carbon atoms held together only by van der Waals forces. These weak interlayer
189 bonds along (001) planes are easily broken during shear (Moore and Lockner, 2004; Rutter, et al., 2013). Initial μ_{peak}
190 followed by strain weakening during deformation experiments of graphite gouges has been previously explained with the

191 work involved in rotating the grains with their (001) planes sub-parallel to the shear surfaces, which puts them in the optimal
192 position for shearing along the weak interlayer bonds (Morrow et al., 2000; Moore and Lockner, 2004; Rutter, et al., 2013).

193 Controversially, Oohashi et al. (2011) reported an absence of μ_{peak} in pure graphite gouges sheared at ≤ 2 MPa with sliding
194 velocities of 1.3 m/s. Instead shearing started and continued at a similar μ throughout their experiments. We hypothesize that
195 higher velocities result in more efficient reorientation of graphite grains, and therefore, μ_{peak} is not present in experiments
196 carried out at seismic rates. We also acknowledge that the imposed velocities in the experiments by Oohashi et al. (2011)
197 were substantially different to ours, and shearing at those seismic rates may cause frictional heating. Therefore, graphite
198 frictional strength in their experiments may be related to thermally-activated weakening mechanisms (Di Toro et al., 2011)
199 that are only significant at these high velocities.

200 We also observed shear strain variations in the various samples (Fig. 1b, c and d) that are systematically related to the
201 conditions of the experiments. The calculated shear strain (or the ratio of shear displacement to measured layer thickness) is
202 directly dependent on the applied normal stress, and shear strains are significantly higher in the experiments performed at 25
203 MPa than the ones at 5 MPa due to better compaction and thinning of the sheared graphite gouges. Furthermore, sliding
204 velocities also play a role in the accommodated total shear strain, and shear strain increases with increase in the applied
205 sliding velocities but only in the high normal stress experiments (Fig. 1b). As we previously suggested, higher velocities may
206 result in more efficient reorganization of graphite grains, and thus further progressive thinning of the graphite gouges
207 occurred. However, we cannot explain the absence of similar trend at the 5 MPa experiments by our results. There are too
208 few of these relationships to fully characterize the effect of sliding velocity on shear strain accumulation in graphite gouges,
209 and more mechanical data of this sort need to be collected in future.

210 **4.2 Structural disorder of graphite**

211 Our experimental study clearly demonstrates transformation of fully/highly crystalline graphite (with R2 ratios ranging from
212 0 to 0.327; Fig. 2; S1) into comparatively poorly organized graphitic carbon (with R2 ratios up to 0.661; Fig. 2; S1), which
213 indicates significant graphite disorder with increasing strain and total frictional work at the tested aseismic sliding velocities
214 (Fig. 3). The estimated bulk shear strains (Table 1) are likely to be significantly lower than the shear strains accommodated
215 within the thin shear surfaces. However, we expect the strain variations within these surfaces to be directly related to the
216 measured bulk shear strains. Nevertheless, we refer to the above relationship as a rough approximation. We also
217 acknowledge that the slickenlined surfaces that were produced experimentally contain some graphite that yield spectra
218 comparable to those acquired from the starting material i.e. there is highly crystalline graphite that appears as unaffected by
219 the deformation. However, at least some of these spectra are derived from undeformed graphite powder that underlies the
220 shear surfaces and could not be entirely removed during sample preparation due to the fragile nature of the samples. It is also
221 possible that some non-deformed graphite powder was accidentally measured through the fractures that are cross-cutting the

222 accumulated shear surfaces (Fig. 4a). But even if some graphite did not undergo mechanical modification during the
223 experiments, the results overall validate that structural disorder of graphite can result from shear deformation subsequent to
224 the graphitization process.

225 We evaluate the documented disorder of the crystal structure of graphite by analyzing variations in R2 ratios, which depend
226 on the increase of defect bands (D1 and D2) in the Raman spectrum of graphite. This relationship is a well-known
227 crystallinity index of graphite that shows the degree of maturity of the carbonaceous material (Wopenka and Pasteris, 1993;
228 Beyssac et al., 2002a; etc.). Alternatively, it may reflect increase in the grain boundary density (Tunistra and Koenig, 1970;
229 Pimenta et al., 2007). However, we aimed to avoid grain boundaries during spectra acquisition, which was possible due to
230 the laser spot size of 412 nm, which is much smaller than the graphite grains in our samples (>10 microns, Fig. 4b). We
231 acknowledge that some of the spectra may have been accidentally obtained in close proximity to grain boundaries, however
232 occasional measurements of this sort are unlikely to affect the average R2 per sample. Thus, we attribute the detected
233 increase in D bands in our experimental data to disorder of the internal structure of graphite rather than grain size reduction.

234 Our findings contradict the paradigm that the degree of graphite crystallinity is determined by an irreversible maturation of
235 carbonaceous material (Bonijoly et al., 1982; Wopenka and Pasteris, 1993; Beyssac et al., 2002a; Buseck and Beyssac,
236 2014). Therefore, graphite should not be considered as a stable mineral (Buseck and Beyssac, 2014), especially in active
237 tectonic settings, where mechanical motions, such as fault creep, may cause disordering of the structure of carbonaceous
238 material that formed during typical graphitization processes. Similar assumptions have been made on graphite in intensely
239 deformed cataclasites (comprising crushed mylonitic chips floating in a fine-grained matrix) that is significantly disordered
240 in comparison with graphite in the spatially associated mylonitic rocks (Kirilova et al, in press; Nakamura et al., 2015).

241 We have experimentally proven that shear strain can not only affect the final structural order of graphite but also manifests
242 as a controlling parameter in the transformation process (Fig. 3a; Table 2). Previous authors have suspected that shear strain
243 may play an important role for graphite modifications, and evidence for this has been found in graphite crystallinity
244 variations in natural samples from active fault zones (Kirilova et al, in press; Nakamura et al., 2015), and strained rocks in
245 metamorphic terrains (Barzoi, 2015; Large et al., 1994). Thus, we conclude that the previously proposed model of
246 progressive graphitization due to increase of temperature (Bonijoly et al., 1982) does not completely reflect the graphite
247 formation mechanisms.

248 Furthermore, graphite can form or be transported at various depths by tectonic processes, and therefore, it can be exposed to
249 different lithostatic pressures, and hence different normal stresses. We demonstrated that during shearing higher normal
250 stress results in an increase of shear strain (Fig. 1b), and thus causes a higher degree of graphite disorder (Fig. 3a; Table 2).
251 This outlines the significant effect of lithostatic pressure on graphite crystallinity that has been undervalued until now
252 (Bonijoly et al., 1982; Wopenka and Pasteris, 1993; Bustin et al, 1995; Beyssac et al. 2002b). Previous experimental studies

253 have identified initiation and enhancement of graphitization under pressure (i. e. increase in graphite crystallinity) but only at
254 nanometer scale (Bonijoly et al., 1982; Beyssac et al., 2003). Nevertheless, we speculate pressure should be also considered
255 as a factor that can determine the degree of graphite crystallinity during both graphitization and graphite structural
256 modifications.

257 We have investigated the effects of shear strain and pressure on graphite crystallinity during shear deformation with aseismic
258 velocities, using a starting material with uniform properties (i.e. highly crystalline graphite powder). In contrast, Kuo et al.
259 (2014) and Oohashi et al. (2011) simulated fault motions in synthetic and natural carbonaceous material with variable degree
260 of maturity at the start of the experiments (ranging from amorphous carbonaceous material to crystalline graphite). Both
261 studies reported graphitization of carbonaceous material due to localized frictional heating rather than structural disordering.
262 These experiments reveal the impact of seismic velocities on graphite structural order and the fact their findings differ so
263 markedly from ours highlights the complexity of graphite transformations in fault zones.

264 Our microstructural observations provide some indications of the deformation processes that affected graphite structural
265 order. The shiny slickenlined surfaces are composed of very fine-grained material visible as slip-localized zone on SEM
266 images (Fig. 4d). Nanoscale observations reveal graphite grains within it occasionally form stacked kink-band structures,
267 (Fig. 5b, c). This zone, which we assume accommodated most of the induced deformation, is underlined by a less deformed
268 zone composed of larger graphite grains in a finer matrix that in places has developed as an anastomosing fabric, typical of
269 creeping gouges (Fig. 4d). In rare places at SEM scale brittely fractured grains also occur (Fig. 4f and 5d). The interpreted
270 structures suggest that brittle processes operated during shearing, and we conclude that these processes resulted in the
271 structural disorder of graphite, manifested as changes in the Raman spectra. This interpretation is in agreement with the
272 conditions of our experiments (i.e. shearing with aseismic velocities took place at room temperature conditions), that
273 typically would not induce temperatures high enough for crystal plastic processes. Furthermore, the microstructures and the
274 inferred processes are exactly the same as those observed by Nakamura et al. (2015) in the Hidaka metamorphic belt, Japan.

275 However, crustal fault zones do not only accommodate brittle deformation. At higher temperatures and confining pressures,
276 localised shearing can operate by plastic mechanisms (White et al., 1980). We hypothesize that graphite crystallinity could
277 also be influenced by plastic deformation, as was also suggested in previous studies by Large et al. (1994), Bustin et al.
278 (1995), Barzoi et al. (2015). Investigating this hypothesis and identifying the exact effects of strain on graphite crystallinity
279 during ductile deformation remain goals for future research.

280 **4.3 Implications for graphite thermometry**

281 The crystallographic structure of graphite measured by Raman spectroscopy has been applied as a thermometer that relies on
282 progressive maturation of originally-organic carbonaceous material during diagenesis and metamorphism. Previous studies

283 have focused on calibrating this thermometer. The current best calibration is described by the following equation $T (^{\circ}\text{C}) = -$
284 $445 * R2 + 641 \pm 50$ (Beyssac et al. 2002) by inferring a linear correlation between R2 ratio and peak metamorphic
285 temperatures. However, this thermometer disregards the effects of mechanical modifications of the graphite structure, which
286 this study has identified as having a substantial influence on graphite crystallinity in deformed rocks at sub-seismic
287 velocities.

288 Our experiments demonstrate a shear strain-dependent increase of the R2 ratio of initially highly crystalline graphite powder
289 due to brittle deformation (Fig. 3a; Table 2). In natural analogues, the pre-shear graphite would yield temperatures up to 641
290 ± 50 $^{\circ}\text{C}$ (S1), which is the upper limit of the calibrated thermometer (Beyssac et al. 2002). Whereas, the sheared samples
291 would indicate peak metamorphic temperatures as low as 347 ± 50 $^{\circ}\text{C}$ (estimated from the most strained samples; S1). Thus,
292 we experimentally prove that in active tectonic settings graphite thermometers may underestimate the peak metamorphic
293 temperatures by < 300 $^{\circ}\text{C}$. In cataclasites from the Alpine Fault zone, New Zealand (Kirilova et al., in press) and fault zones
294 of the Hidaka metamorphic belt, Japan (Nakamura, et al., 2015), the graphite thermometer yields temperature discrepancies
295 of more than 100 $^{\circ}\text{C}$ compared to temperature estimates derived both from the surrounding high-grade amphibolite facies
296 mylonites and the lower grade equilibrium cataclastic phases (marked by chlorite alteration). Barzoi (2015) also described
297 differences of ~ 150 $^{\circ}\text{C}$ in graphite temperatures between strained and less strained low grade metamorphic rocks from
298 Parang Mountains, South Carpathians.

299 We conclude that shear strain calibration of the current graphite thermometer is needed, and we propose an appropriate
300 adjustment based on our dataset. Fig. 3a illustrates good correlation between the average R2 and the bulk shear strain
301 measured within a sample, which can be described by the following equation (1):

$$302 \quad F(x) = 0.14017 * x^{0.30713} + 0.15629 \text{ with a correlation coefficient } R^2 = 0.95 \quad (1)$$

303 where x = bulk shear strain.

304 However, a calibration of the existing graphite thermometer could be still insufficient to permit reliable temperature
305 estimates in active tectonic settings because both aseismic and seismic sliding velocities are likely to be encountered in fault
306 zones, resulting in structural disorder of graphite or graphitization (Oohashi et al., 2013) respectively. Furthermore, it can be
307 challenging to estimate shear strain in natural samples, so a strain-calibrated graphite thermometer may be impossible to use
308 in deformed rocks.

309 **5. Conclusions**

310 We have experimentally demonstrated that graphite crystallinity can be reduced by deformation by performing shear
311 deformation experiments at aseismic sliding velocities insufficient to generate appreciable frictional heat on graphite gouges

312 composed of powdered highly-organized graphite. Our results clearly demonstrate significant decrease in graphite structural
313 order, which is a function of the total shear strain attained during the various experiments. Microstructural data presented
314 here reveal that this is a result of brittle processes. We also observed a trend of increasing shear strain within a sample with
315 increase in the applied normal stresses and sliding velocities. This reveals the complexity of graphite structural modifications
316 and highlights the significance of the various parameters that can affect the graphitization process. Our findings compromise
317 the validity of the calibrated graphite thermometer by showing they may underestimate the peak metamorphic temperatures
318 in active tectonic settings. We further suggest a simple shear strain calibration of this thermometer.

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398

399 **Table 1.** Summary of the conditions at which experiments were carried out and results.

400 **Table 2.** Summary of the relationship between shear strain and average R2 within a sample. The conditions of each
401 experiment are also given as follows: applied normal stress in MPa, sliding velocities in $\mu\text{m/s}$ and sliding displacement in
402 mm.

403 **Figure 1.** Plots of mechanical data (a) friction coefficient, μ vs. displacement (b), (c), (d) friction coefficient, μ vs. shear
404 strain.

405 **Figure 2.** Representative Raman spectra illustrating: (i) the most crystalline graphite (left column) within a sample; (ii)
406 graphite with average crystallinity per sample (middle column); and (iii) the most disordered graphite (right column)
407 encountered in each sample. The R2 ratio for each spectrum is also noted in italic font.

408 **Figure 3.** Plot of the average R2 ratio vs shear strain accumulated during each experiment.

409 **Figure 4.** SEM images, obtained from the deformed graphite gouge during experiment 8 (normal stress at 25 MPa with 1
410 $\mu\text{m/s}$ sliding velocity), show: (a) Slickenlines ornamenting the shear surface; (b), (c) A well-compacted layer of aligned
411 graphite grains, which make up the shear surface. Bright patches due to a differential charging effect; (d) A less deformed
412 zone with typical cataclastic fabric, underlying the shear surface; (e) Dilated cleavage planes in large graphite grains filled
413 with smaller platy graphite grains oriented sub-perpendicular to the shear direction; (f) Fractured graphite grains.

414 **Supplementary material 1 (S1).** Raman data from 20 spectra per sample together with calculated R2 ratio and average R2
415 value for each sample. The last column represents temperature estimated by the current best calibration of a Raman-based
416 thermometer: $T (^{\circ}\text{C}) = - 445 * R2 + 641 \pm 50$.

Experiment number	Normal stress (MPa)	Sliding velocity ($\mu\text{m/s}$)	Displacement (mm)	Peak friction coefficient (μ_{peak})	Steady state friction coefficient (μ_{ss})	Shear strain maximum
1	5	1	20	0.53	0.22	17.70
2	5	1	10	0.53	0.22	8.17
3	5	1	5	0.52	<i>not reached</i>	4.23
4	5	10	20	0.53	0.24	20.45
5	5	100	20	0.57	0.22	16.89
6	5	100	10	0.55	0.22	9.80
7	5	100	5	0.57	<i>not reached</i>	3.87
8	25	1	20	0.43	0.17	21.45
9	25	10	20	0.43	0.17	31.86
10	25	100	20	0.41	0.14	46.77

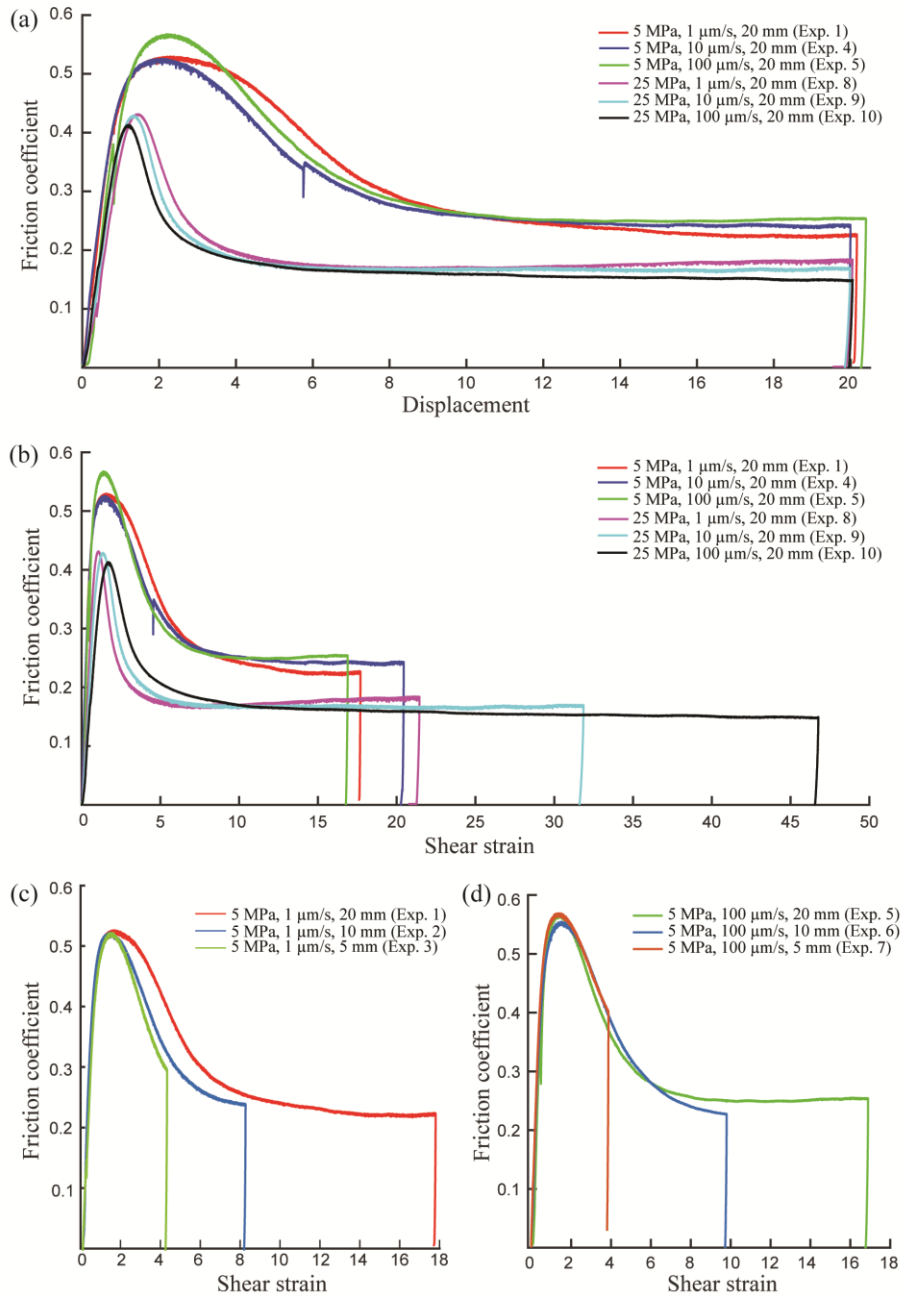
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Table 1. Summary of the conditions at which experiments were carried out and results.

Sample	Experimental conditions	Shear strain	Average R2 (error estimate ± 0.05)	Total frictional work
Pre-shear graphite	N/A	N/A	0.173	
Exp. 2	5 MPa, 1 $\mu\text{m/s}$, 10 mm	8.17	0.438	38.8689
Exp. 6	5 MPa, 100 $\mu\text{m/s}$, 10 mm	9.80	0.430	46.6369
Exp. 5	5 MPa, 100 $\mu\text{m/s}$, 20 mm	16.89	0.454	157.9314
Exp. 1	5 MPa, 1 $\mu\text{m/s}$, 20 mm	17.70	0.506	165.4748
Exp. 4	5 MPa, 10 $\mu\text{m/s}$, 20 mm	20.45	0.517	180.8346
Exp. 8	25 MPa, 1 $\mu\text{m/s}$, 20 mm	21.45	0.520	192.9007
Exp. 9	25 MPa, 10 $\mu\text{m/s}$, 20 mm	31.86	0.580	283.7721
Exp. 10	25 MPa, 100 $\mu\text{m/s}$, 20 mm	46.77	0.604	424.0356

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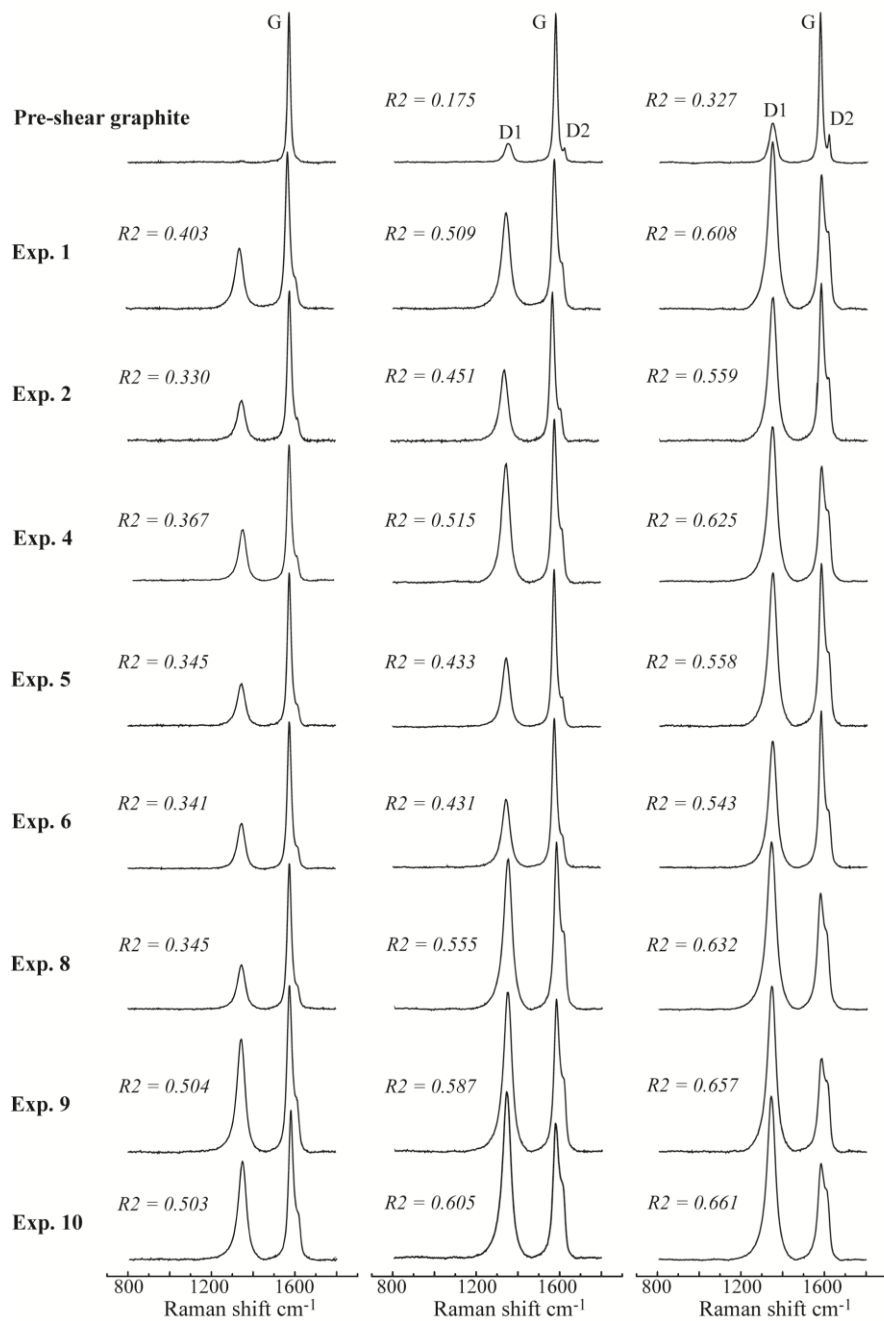
422 **Table 2.** Summary of the relationship between shear strain, average R2, and total frictional work within a sample. The
423 conditions of each experiment are also given as follows: applied normal stress in MPa, sliding velocities in $\mu\text{m/s}$ and sliding
424 displacement in mm.



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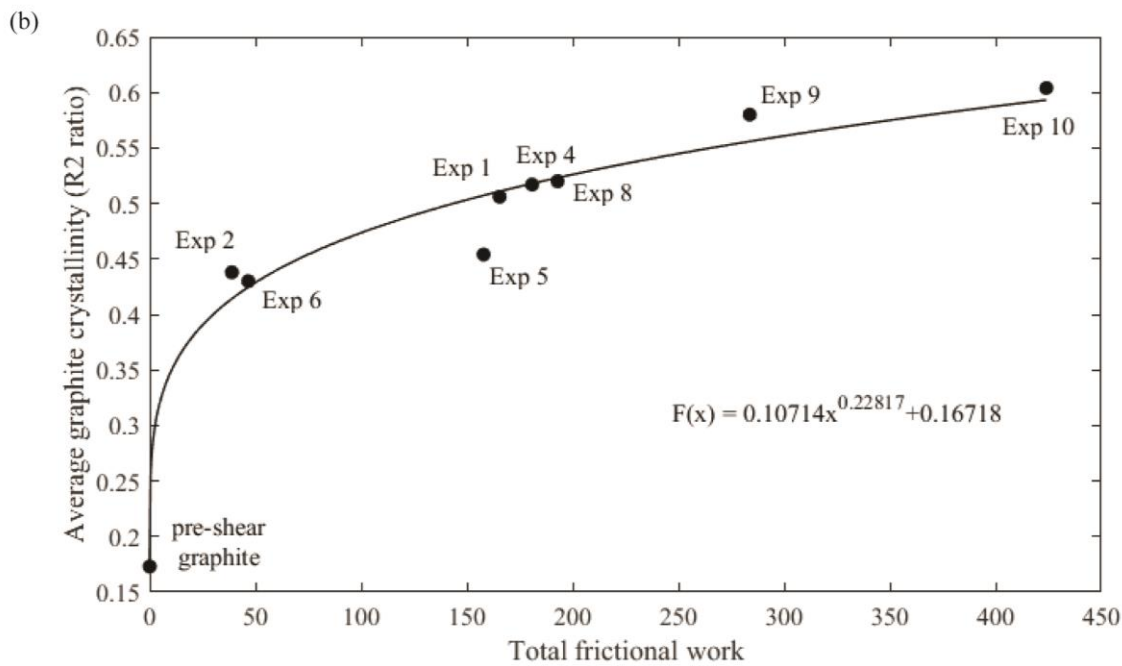
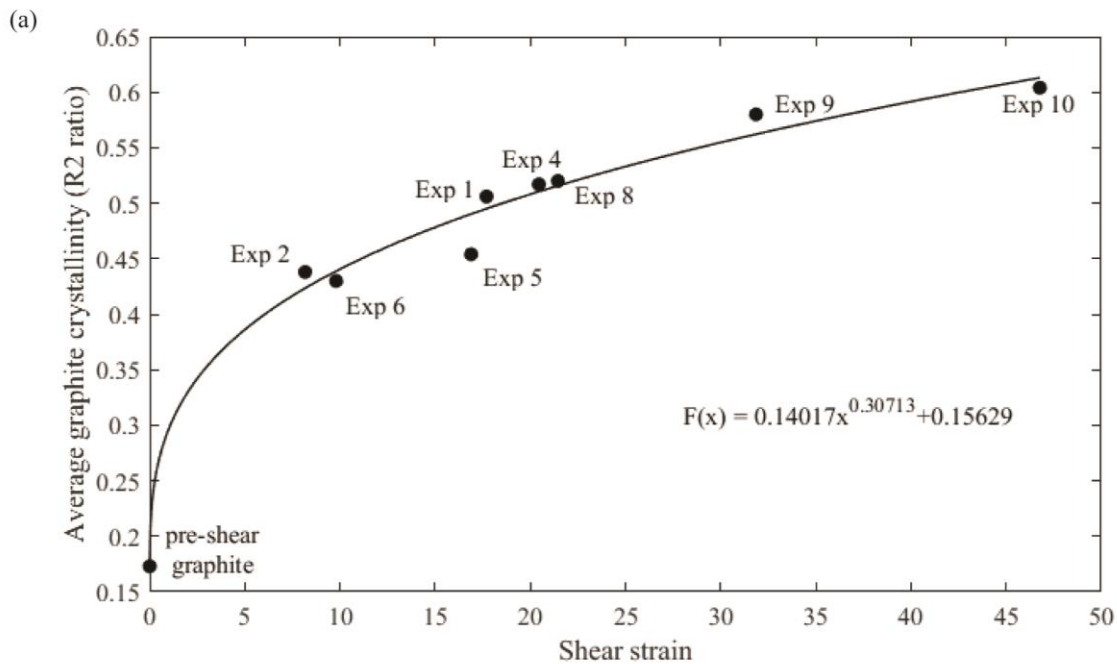
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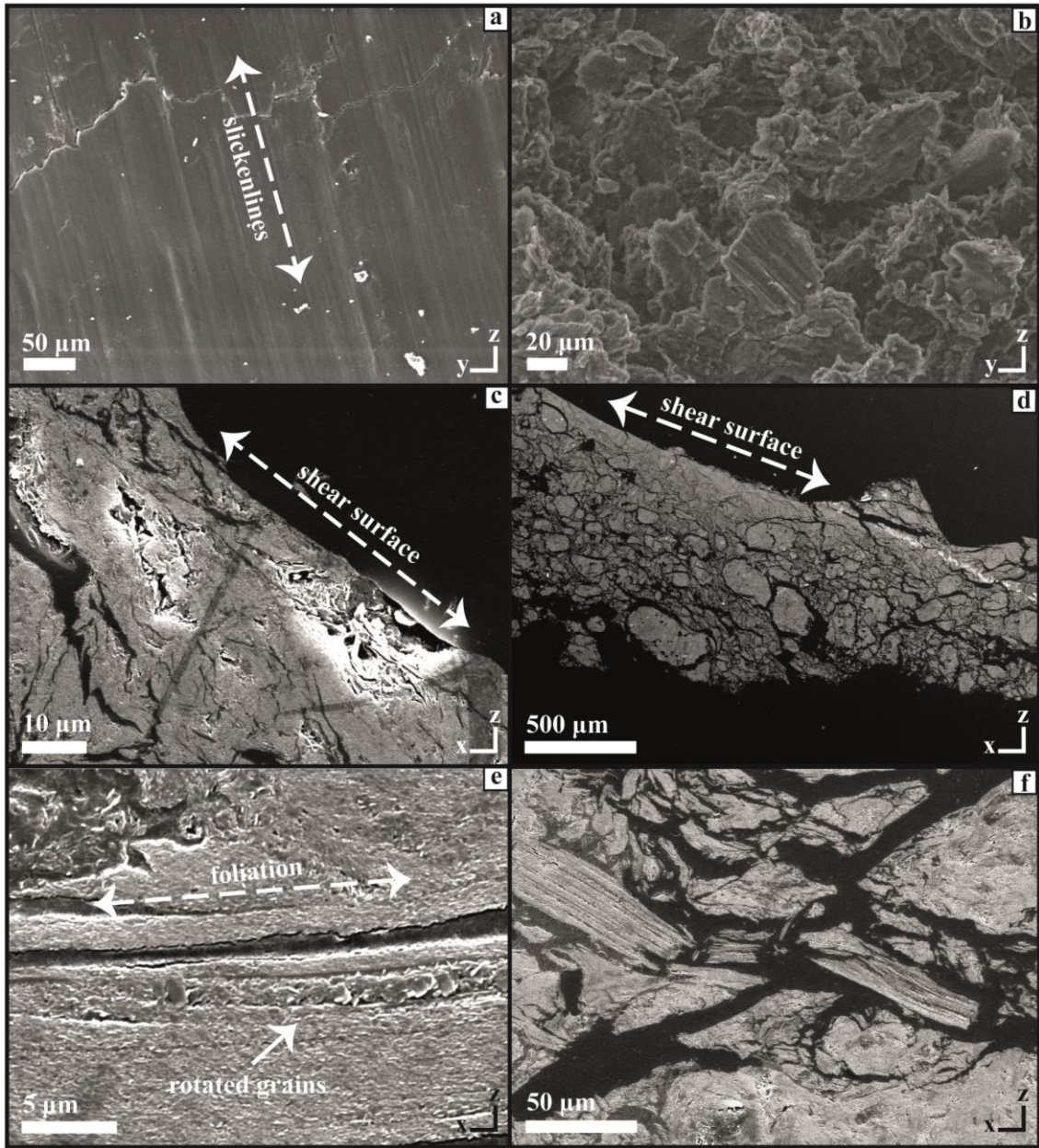
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 431 graphite with average crystallinity per sample (middle column); and (iii) the most disordered graphite (right column)
 432 encountered in each sample. The R_2 ratio (with an error estimate of 0.05) for each spectrum is also noted in italic font.



433

434 **Figure 3.** (a) Plot of the average R2 ratio vs shear strain accumulated during each experiment. (b) Plot of the average R2
 435 ratio vs total frictional work during each experiment.

436



437

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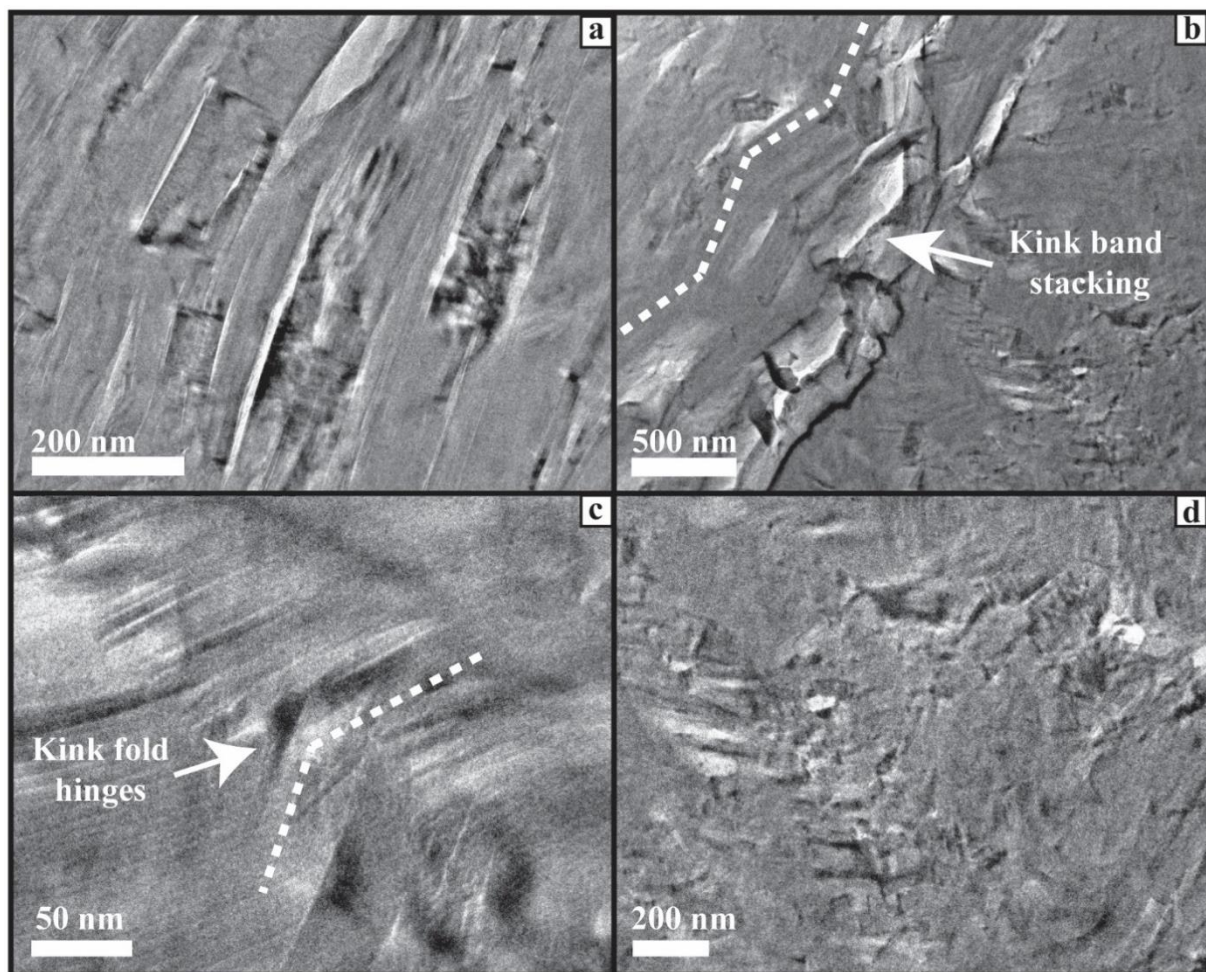


Figure 5 TEM images showing microstructural characteristics of the slip-localized shear surface: (a) aligned grains showing slightly different orientation; (b) kink band stacking; (c) dilated kink fold hinges; (d) fragmented grains.