



# 1 **Structural Disorder of Graphite and Implications for Graphite** 2 **Thermometry**

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## 9 **Key Points:**

- 10
  - graphite, disorder, thermometry, Raman

## 11 **Abstract**

12 Graphitization, or the progressive maturation of carbonaceous material, is considered an irreversible process. Thus, the  
13 degree of graphite crystallinity has been calibrated as an indicator of the peak metamorphic temperatures experienced by the  
14 host rocks. However, discrepancies between temperatures indicated by graphite crystallinity versus other thermometers have  
15 been documented in deformed rocks. To examine the possibility of mechanical modifications of graphite structure and the  
16 potential impacts on graphite 'thermometry' we performed laboratory deformation experiments. We sheared highly  
17 crystalline graphite powder at normal stresses of 5 and 25 MPa and aseismic slow sliding velocities of 1  $\mu\text{m/s}$ , 10  $\mu\text{m/s}$  and  
18 100  $\mu\text{m/s}$ . The degree of graphite crystallinity both in the starting and resulting materials was analyzed by Raman  
19 microspectroscopy. Our results demonstrate consistent decrease of graphite crystallinity with increasing shear strain. We  
20 conclude that the calibrated graphite 'thermometer' is ambiguous in active tectonic settings and we suggest that a calibration  
21 that accounts for shear strain is needed.



## 22 1 Introduction

23 Organic matter, preserved in sedimentary rocks, can be transformed into crystalline graphite due to structural and  
24 compositional changes during diagenesis and metamorphism, a process known as graphitization (Beysac et al., 2002a;  
25 Bonijoly et al., 1982; Buseck and Beysac, 2014; Wopenka and Pasteris, 1993; etc.). Graphitization is thought to be an  
26 irreversible process and graphite is known to remain stable to the highest temperatures of granulite facies and the highest  
27 pressures of coesite-eclogite facies (Buseck and Beysac, 2014). It is generally accepted that the degree of graphite  
28 crystallinity, or its structural order, is determined mainly by the maximum temperature conditions experienced by the host  
29 rocks, whereas lithostatic pressure and shear strain are considered to have only minor influence on graphitization (Bonijoly  
30 et al., 1982; Wopenka and Pasteris, 1993; Bustin et al, 1995). Therefore, graphite crystallinity has been calibrated as an  
31 indicator of the peak temperatures reached during progressive metamorphism (Beysac et al., 2002a; Reitmeijer and  
32 McKinnon, 1985). However, in strained rocks discrepancies between temperatures indicated by the crystallinity of graphite  
33 vs. other thermometers have been reported (Barzoi, 2015; Nakamura et al., 2015; Kirilova et al., in review). Thus, numerous  
34 authors have speculated that tectonic deformation results in graphite structural modifications that challenge the validity of  
35 the existing graphite thermometers (Large et al., 1994; Bustin et al, 1995; Crespo et al., 2006; Barzoi, 2015; Nakamura et al.,  
36 2015).

37 Furthermore, graphite occurrence and enrichment have been documented in several fault zones in the world, e. g. the Alpine  
38 Fault zone, New Zealand (Kirilova, et al., in review), the Hidaka metamorphic belt, Hokkaido, Japan (Nakamura et al.,  
39 2015), the Atotsugawa fault system, Japan (Oohashi, et al., 2012), the Tanakura Tectonic Line, Japan (Oohashi et al., 2011),  
40 the Err nappe detachment fault, Switzerland (Manatschal, 1999), and the KTB borehole, Germany (Zulauf et al., 1990). In  
41 these intensely deformed rocks its presence is of particular interest because its low friction at  $\mu \sim 0.1$  (Morrow et al., 2000)  
42 allows graphite to act as a natural solid lubricant (Savage, 1948). The mechanical behavior of graphite has been broadly  
43 investigated in both natural and experimental specimens, where it manifests with the lowest  $\mu$  among sheet structure  
44 minerals (Moore and Lockner, 2004; Oohashi et al., 2011, 2013; Rutter, et al., 2013; Kuo et al., 2014, etc.) confirming it  
45 could have a significant impact on fault mechanics. It has been experimentally proven that even a small fraction of graphite  
46 has disproportionately large effect on frictional strength due to concentration of smeared graphite layers (Rutter, et al., 2013).

47 However, structural changes in crystalline graphite caused by tectonic deformation have not been explained until now. To  
48 examine this aspect and to investigate the potential impacts of structural disordering of graphite on the graphite  
49 'thermometer', we have carried out laboratory deformation experiments on highly crystalline graphite powder.



## 50 2.2 Experimental methods

### 51 2.1 Sample description

52 As a starting material in the current study we used synthetic (or commercially synthesized) graphitic carbon to avoid  
53 complexities arising from variable degree of crystallinity in natural carbon materials. Initially, the material was crushed to  
54 160  $\mu\text{m}$  in a RockLabs Swing (TEMA) mill. The resulting fine graphitic powder was ‘cooked’ at 700°C for two hours in a  
55 Lindberg Blue M Muffle Furnace to achieve full graphitization, which is known to occur at this temperature in the absence  
56 of other variations in physical conditions (Buseck and Beyssac, 2014). This was used as the starting material for the  
57 deformation experiments.

### 58 2.2 Experimental procedure

59 In total, 10 deformation experiments were performed at room temperature and room humidity in the Brittle Rock  
60 Deformation Versatile Apparatus BRAVA (Colletini et al., 2014), at INGV, Rome. For each experiment two 3-mm thick  
61 layers of synthetic graphite gouges were placed in between three grooved forcing blocks in a double-direct shear  
62 configuration (e.g. Dieterich, 1972). The two side blocks are held stationary, and the central forcing block is driven  
63 downward causing shear to occur within the graphite gouge layers. Normal stress is applied by the horizontal piston in load-  
64 feedback control mode and shear displacement accomplished by the vertical piston in displacement-feedback control mode.  
65 Forces are measured with stainless steel load cells ( $\pm 0.03$  kN) and displacements are measured with LVDTs ( $\pm 0.1$   $\mu\text{m}$ )  
66 attached to each piston. Experiments have been conducted at normal stresses of 5 MPa or 25 MPa and aseismic sliding  
67 velocities of 1  $\mu\text{m/s}$ , 10  $\mu\text{m/s}$  and 100  $\mu\text{m/s}$ . The experiments were carried out to total displacements of 20 mm. In addition,  
68 some experiments were stopped at 5 mm and 10 mm and the specimens were then recovered to reveal graphite structural  
69 changes that took place during different amounts of total deformation. The coefficient of friction ( $\mu$ ) was calculated as the  
70 ratio of measured shear load to measured normal load ( $\mu = \tau / \sigma_n$ , where  $\tau$  is shear stress and  $\sigma_n$  is effective normal stress).  
71 The average shear strain ( $\gamma$ ) within the layer was calculated by dividing shear displacement increments by the measured layer  
72 thickness and summing. The displacement values of the vertical and horizontal load points were corrected for the elastic  
73 stretch of each load frame, taking into account that the machine stiffness is 1283 kN/mm on the horizontal axis and 928.5  
74 kN/mm on the vertical axis.

### 75 2.3 Raman microspectroscopy

76 The degree of graphite crystallinity was measured by an Alpha 300R+ confocal Raman microscope (WITec, Ulm, Germany)  
77 with a 532 nm laser (Coherent, Santa Clara, California), located at the Department of Chemistry, University of Otago, New  
78 Zealand. The laser (3.0 mW) was focused on the samples with a 50 $\times$  Zeiss objective. The scattered light was dispersed with



79 a 1200 g/mm grating. The combination of the 50× objective and 532 nm laser wavelength produced a laser spot size of  
80 approximately 412 nm in diameter. The integration time of each spectrum was 2 seconds with 50 co-additions (100 seconds  
81 in total). The spectra were calibrated using the Raman band from a silicon wafer prior to each set of measurements.

82 The collected spectra were pre-processed in GRAMS AI 9.1 (Thermo Fisher Scientific Inc.), where cosmic spikes were  
83 removed and a multi-point linear baseline offset was performed. This was followed by peak fitting three Lorentzian-  
84 Gaussian functions to each spectrum with a linear baseline over 1000 - 1700  $\text{cm}^{-1}$ . For each spectrum, the area ratio was  
85 calculated ( $R2 = AD1 / (AG + AD1 + AD2)$ , where  $A_i$  = area of the  $i$ th peak) (Beysac et al., 2002a; Wopenka and Pasteris,  
86 1993).

## 87 2.4 Scanning electron microscopy

88 Microstructural analyses of the graphite gouge recovered from the biaxial apparatus were carried out using a scanning  
89 electron microscope (SEM). Some SEM images were acquired from the shiny surfaces of the graphite layers that had been  
90 parallel to the center and or side forcing blocks (Y-Z sections), with a Zeiss Sigma field emission scanning electron  
91 microscope (VP FEG SEM) at the Otago Centre for Electron Microscopy (OCEM), University of Otago, New Zealand. The  
92 instrument was operated in variable pressure mode (VP) at 15 kV using a working distance (WD) of 7 – 8 mm and a VPSE  
93 (VP-mode secondary electrons) detector. In addition, polished thin sections cut perpendicular to the surface of contact with  
94 the center and side forcing blocks (X-Z sections) were imaged on a JEOL JSM-6510 SEM at the University of Potsdam,  
95 Germany, where high-resolution secondary electron images were collected at 20 kV and a WD of 10 mm.

## 96 3 Results

### 97 3.1 Mechanical data

98 Our experiments allowed us to investigate graphite mechanical behavior and structural modifications under various sliding  
99 velocities, normal stresses and shear strain. These conditions are summarized in Table 1.

#### 100 3.1.2 Friction variations

101 Over several mm of displacement, the friction coefficient shows a similar evolution trend in all experiments. On a plot of  
102 friction vs. displacement (Fig. 1a), the friction coefficient ( $\mu$ ) delineates a curve characterized by a rapid increase to an initial  
103 peak friction ( $\mu_{\text{peak}}$ ), followed by a subsequent exponential decay towards a steady-state friction ( $\mu_{\text{ss}}$ ) over a slip weakening  
104 distance. The shapes of the friction-displacement curves vary with the normal stress applied and are steeper for the  
105 experiments conducted at 25 MPa than the ones at 5 MPa (Fig. 1a) i.e. the displacement required to achieve steady-state  
106 decreases at higher normal stress. In addition, the values of both  $\mu_{\text{peak}}$  and  $\mu_{\text{ss}}$  (Fig. 1a; Table 1) are significantly lower in the  
107 experiments at 25 MPa ( $\mu_{\text{peak}} = \sim 0.4$ ;  $\mu_{\text{ss}} = \sim 0.1$ ) than in the experiments at 5 MPa ( $\mu_{\text{peak}} = \sim 0.5$ ;  $\mu_{\text{ss}} = \sim 0.2$ ). Plots of  $\mu$  at all



108 slip rates (Fig. 1a) indicate a gradual decrease of  $\mu_{\text{peak}}$  with increasing shear velocity at high normal stress (Table 1). In the  
109 experiments at 5 MPa subtle variations in  $\mu_{\text{peak}}$  also occur but a velocity-related trend is not observed.  $\mu_{\text{ss}}$  does not depend in  
110 any experiment on slip rates, and  $\mu_{\text{ss}}$  remains constant for experiments at both low and high normal stress (Fig. 1a; Table 1).

### 111 3.1.3 Shear strain variations

112 Plots of friction vs. shear strain (Fig. 1b) show significant variations in shear strain ( $\gamma$ ) attained over equivalent sliding  
113 displacements. The estimated shear strain values are a geometric consequence of different thickness changes. Consideration  
114 of the shear strain at equivalent sliding velocities but different normal stresses demonstrates that shear strains achieved  
115 during the 5 MPa experiments are approximately half of those at 25 MPa (Fig. 1b; Table 1). In addition, the experiments at  
116 25 MPa demonstrate a dramatic increase in shear strain with increasing slip velocity (Fig. 1b; Table 1), whereas at low  
117 normal stress we do not observe any systematic variations associated with changes in sliding velocities (Fig. 1b, c and d).  
118 Fig. 1c and d show the experiments at low shear strain used to characterize graphite structural changes in the early stages of  
119 deformation (Table 1).

### 120 3.2 Graphite crystallinity

121 All the experiments resulted in the development of shiny smooth surfaces with gentle slickenlines (macroscopic fine  
122 grooves, parallel to the slip direction as defined by Toy et al., in press). Raman spectra obtained on the top of these surfaces,  
123 that had accommodated most of the induced deformation, are compared to Raman spectra from the starting material to  
124 identify the effects of mechanical deformation on graphite crystallinity.

125 Raman data from 20 spectra per sample are presented in Supplementary material 1 (S1). Representative spectra for each  
126 sample are illustrated in Fig. 2, which shows spectra displaying the least (left column) and the most (right column)  
127 disordered graphite within a sample (i. e. lowest and highest R2 values respectively). Spectra that were typical of the average  
128 for each sample are also presented (middle column). Experiments 3 and 7 were stopped at only 5 mm displacement and  
129 resulted in extremely fragile deformed surfaces, which were unable to be extracted without them breaking into pieces too  
130 small to obtain spectra from. Thus, graphite crystallinity was not measured in these experiments.

131 All the acquired spectra show typical G, D1 and D2 bands, respectively at  $\sim 1580\text{ cm}^{-1}$ ,  $\sim 1350\text{ cm}^{-1}$  and  $\sim 1620\text{ cm}^{-1}$  (S1). The  
132 degree of graphite crystallinity in each sample could thus be calculated by using the area ratio R2 (Fig. 2; S1). Raman  
133 spectra collected from the starting material show R2 values ranging from 0 to 0.327 (Fig. 2), corresponding respectively to  
134 fully crystalline and highly organized graphite. Spectra acquired from the deformed surfaces show higher R2 values (Fig. 2;  
135 S1). The most crystalline graphite with R2=0.330 was produced in Exp. 2 (Fig. 2) while the most disordered graphite with  
136 R2=0.661 resulted from Exp. 10 (Fig. 2).



137 As graphite crystallinity vary within a sample (Fig. 2; S1), we examine average R2 values for each one and compare them  
138 with applied normal stress, sliding velocity and shear strain (Table 2). The starting material has average  $R2_{\text{pre-shear graphite}} =$   
139 0.173, whereas all deformed samples have higher average R2 values (Table 2). Analyzing the average R2 values for  
140 deformed samples reveals that graphite is more disordered in the high-pressure experiments (Table 2) than in the  
141 experiments at 5 MPa. Furthermore, in the experiments at 25 MPa the average graphite crystallinity decreases with  
142 increasing sliding velocities (Table 2). In contrast, at low normal stress, we do not observe any dependence of the degree of  
143 graphite crystallinity on the applied sliding velocities (Table 2). Overall graphite appears as most disordered in the  
144 experiments where the highest shear strain was achieved (Table 2). This relationship is illustrated in Fig. 3 by fitting a power  
145 function with a correlation coefficient  $R^2 = 0.96$ . The experiments 2 and 6 at low normal stress, which were stopped at 10  
146 mm displacement and accommodated the least amount of shear strain, contain the least disordered graphite (Fig. 3; Table 2).

### 147 3.3 Microstructural characteristics

148 Similar microstructural features were observed in all the deformed samples. SEM images obtained from the sample  
149 deformed during experiment 8 are presented to demonstrate our observations (Fig. 4).

150 These high-resolution images in Y-Z sections reveal that the shiny surfaces are decorated by closely spaced (from < 5 to 10  
151 micrometers) slickenlines (Fig. 4a), on top of a smooth continuous layer. In places, the continuity of this layer is interrupted  
152 by fine (~1 to 2 micrometers in width) fractures (Fig. 4a), with random orientation compared to the slip direction.  
153 Occasionally, the deformed surface appears as completely disrupted, comprising of platy graphite crystals 10 to 50  
154 micrometers in size, oriented nearly parallel to the shear direction (Fig. 4b). In X-Z sections this highly deformed surface is  
155 observed as a thin slip-localized zone, composed of well-compacted layer of aligned graphite grains (Fig. 4c). This localized  
156 shear surface is underlain by a zone of randomly oriented, inequigranular, irregular graphite grains (Fig. 4d). In places, most  
157 of the graphite grains are aligned with their basal (001) planes parallel to the slip direction, and form compacted layers,  
158 defining a weak fabric development (Fig. 4e). There has been some dilation along these cleavage planes, and the spaces thus  
159 created are filled with smaller graphite grains with their (001) planes sub-perpendicular to the shear direction (Fig. 4e).  
160 Locally, intensely fractured grains are also observed (Fig. 4f).

## 161 4 Discussion

### 162 4.1 Mechanical behavior

163 Graphite in our experiments shows mechanical behavior consistent with other mechanical studies of pure graphite gouges.  
164 Our results display low  $\mu_{\text{ss}}$  values (from ~0.1 to ~0.2; Table 1) as did the low-pressure deformation experiments of  
165 carbonaceous material performed by Morrow et al. (2000), Moore & Lockner (2004), Oohashi et al. (2011, 2013), Kuo et al.



166 (2014), and Rutter et al. (2016). The low frictional strength of graphite is well known and has been attributed to its sheet  
167 structure composed of covalently bonded carbon atoms held together only by van der Waals forces. These weak interlayer  
168 bonds along (001) planes are easily broken during shear (Moore & Lockner, 2004; Rutter, et al., 2016). Initial  $\mu_{\text{peak}}$  followed  
169 by strain weakening during deformation experiments of graphite gouges has been previously explained with the work  
170 involved in rotating the grains with their (001) planes sub-parallel to the shear surfaces, which puts them in the optimal  
171 position for shearing along the weak interlayer bonds (Morrow et al., 2000; Moore & Lockner, 2004; Rutter, et al., 2016).

172 Controversially, Oohashi et al. (2011) reported an absence of  $\mu_{\text{peak}}$  in pure graphite gouges sheared at  $\leq 2$  MPa with sliding  
173 velocities of 1.3 m/s. Instead shearing started and continued at a similar  $\mu$  throughout their experiments. Our data indicate  
174 that  $\mu_{\text{peak}}$  tends to increase with decreasing normal stresses (see experiments at 25 MPa vs. 5 MPa: Fig. 1a; Table 1),  
175 therefore, we attribute the discrepancies in graphite frictional strength to the effect of sliding velocity on graphite friction.  
176 We hypothesize that higher velocities result in more efficient reorientation of graphite grains, and therefore,  $\mu_{\text{peak}}$  is not  
177 present in experiments carried out at seismic rates. This hypothesis is also consistent with the observations from our  
178 experiments at 25 MPa that clearly indicate a trend of decreasing  $\mu_{\text{peak}}$  with increasing sliding velocity (Fig. 1a, b; Table 1).  
179 We also acknowledge that the imposed velocities in the experiments by Oohashi et al. (2011) were substantially different to  
180 ours, and shearing at those seismic rates may cause partial frictional heating. Therefore, graphite frictional strength in their  
181 experiments may be related to thermally-activated weakening mechanisms (Nakatani, 2001) that are only significant at these  
182 high velocities.

183 We also observed shear strain variations in the various samples (Fig. 1b, c and d) that are systematically related to the  
184 conditions of the experiments. The calculated shear strain (or the ratio of shear displacement to measured layer thickness) is  
185 linearly dependent on the applied normal stress, and shear strains are significantly higher in the experiments performed at 25  
186 MPa than the ones at 5 MPa due to better compaction and thinning of the sheared graphite gouges. Furthermore, slip rates  
187 also play a role in the accommodated total shear strain, and shear strain increases with increase in the applied sliding  
188 velocities but only in the high-pressure experiments (Fig. 1b). As we previously suggested, higher velocities may result in  
189 more efficient reorganization of graphite grains, and thus further progressive thinning of the graphite gouges occurred.  
190 However, we cannot explain the absence of similar trend at the 5 MPa experiments by our results. There are too few of these  
191 relationships to fully characterize the effect of sliding velocity on shear strain accumulation in graphite gouges, and more  
192 mechanical data of this sort need to be collected in future.

#### 193 **4.2 Structural disorder of graphite**

194 Our experimental study clearly demonstrates transformation of fully/highly crystalline graphite (with R2 ratios ranging from  
195 0 to 0.327; Fig. 2; S1) into comparatively poorly organized graphitic carbon (with R2 ratios up to 0.661; Fig. 2; S1), which  
196 indicates significant graphite disorder with increasing strain at the tested aseismic sliding velocities (Fig. 3). We also





197 acknowledge that the slickenlined surfaces that were produced experimentally contain some graphite that yield spectra  
198 comparable to those acquired from the starting material i.e. there is highly crystalline graphite that appears as unaffected by  
199 the deformation. However, at least some of these spectra are derived from undeformed graphite powder that underlies the  
200 shear surfaces and could not be entirely removed during sample preparation due to the fragile nature of the samples. It is also  
201 possible that some non-deformed graphite powder was accidentally measured through the fractures that are cross-cutting the  
202 accumulated shear surfaces (Fig. 4a). But even if some graphite did not undergo mechanical modification during the  
203 experiments, the results overall validate that structural disorder of graphite can result from shear deformation subsequent to  
204 the graphitization process.

205 Our findings contradict the paradigm that the degree of graphite crystallinity is determined by an irreversible maturation of  
206 carbonaceous material (Beysac et al., 2002a; Bonijoly et al., 1982; Buseck and Beysac, 2014; Wopenka and Pasteris,  
207 1993). Therefore, graphite should not be considered as a stable mineral, especially in active tectonic settings, where  
208 mechanical motions, such as fault creep, may cause disordering of the structure of carbonaceous material that formed during  
209 typical graphitization processes. Similar assumptions have been made on graphite in intensely deformed cataclasites  
210 (comprising crushed mylonitic chips floating in a fine-grained matrix) that is significantly disordered in comparison with  
211 graphite in the spatially associated mylonitic rocks (Kirilova et al, in review; Nakamura et al., 2015).

212 We have experimentally proven that shear strain can not only affect the final structural order of graphite but also manifests  
213 as a controlling parameter in the transformation process (Fig. 3; Table 2). Previous authors have suspected that shear strain  
214 may play an important role for graphite modifications, and evidence for this has been found in graphite crystallinity  
215 variations in natural samples from active fault zones (Kirilova et al, in review; Nakamura et al., 2015), and strained rocks in  
216 metamorphic terrains (Barzoi, 2015; Large et al., 1994). Thus, we conclude that the previously proposed model of  
217 progressive graphitization due to increase of temperature (Bonijoly et al., 1982) does not completely reflect the graphite  
218 formation mechanisms.

219 Furthermore, graphite can form or be transported at various depths by tectonic processes, and therefore, it can be exposed to  
220 different lithostatic pressures. We demonstrated that during shearing higher normal stress results in an increase of shear  
221 strain (Fig. 1b), and thus causes a higher degree of graphite disorder (Fig. 3; Table 2). This outlines the significant effect of  
222 lithostatic pressure on graphite crystallinity that has been undervalued until now (Bonijoly et al., 1982; Wopenka and  
223 Pasteris, 1993; Bustin et al, 1995; Beysac et al. 2002b). Previous experimental studies have identified initiation and  
224 enhancement of graphitization under pressure (i. e. increase in graphite crystallinity) but only at nanometer scale (Bonijoly et  
225 al., 1982; Beysac et al., 2003). Nevertheless, we speculate pressure should be also considered as a factor that can determine  
226 the degree of graphite crystallinity during both graphitization and graphite structural modifications.





227 We have investigated the effects of shear strain and pressure on graphite crystallinity during shear deformation with aseismic  
228 velocities, using a starting material with uniform properties (i.e. highly crystalline graphite powder). In contrast, Kuo et al.  
229 (2014) and Oohashi et al. (2011) simulated fault motions in synthetic and natural carbonaceous material with variable degree  
230 of maturity at the start of the experiments (ranging from amorphous carbonaceous material to crystalline graphite). Both  
231 studies reported graphitization of carbonaceous material due to localized frictional heating rather than structural disordering.  
232 These experiments reveal the impact of seismic velocities on graphite structural order and the fact their findings differ so  
233 markedly from ours highlights the complexity of graphite transformations in fault zones.

234 Our microstructural observations provide some indications of the deformation processes that affected graphite structural  
235 order. They reveal a thin slip-localized zone (Fig. 4d), underlined by a less deformed zone with typical cataclastic fabric  
236 (random fabric (Fig. 4d), affected by occasional fractures (Fig. 4f)). These observations demonstrate that brittle processes  
237 operated during shearing and we infer these processes resulted in the structural disorder of graphite, manifested as changes in  
238 the Raman spectra. However, crustal fault zones do not only accommodate brittle deformation; at higher temperatures,  
239 confining pressures, and lower strain rates, localised shearing may be accommodated by plastic mechanisms (White et al.,  
240 1980). We hypothesize that graphite crystallinity can also be influenced by plastic deformation as also suggested in previous  
241 studies by Large et al. (1994), Bustin et al. (1995), Barzoi et al. (2015). Investigating this hypothesis and identifying the  
242 exact effects of strain on graphite crystallinity during ductile deformation remain goals for future research.

### 243 **4.3 Implications for graphite thermometry**

244 The crystallographic structure of graphite measured by Raman spectroscopy has been applied as a thermometer that relies on  
245 progressive maturation of originally-organic carbonaceous material during diagenesis and metamorphism. Previous studies  
246 have focused on calibrating this thermometer. The current best calibration is described by the following equation  $T (^{\circ}\text{C}) = -$   
247  $445 * R2 + 641 \pm 50$  (Beysac et al. 2002) by inferring a linear correlation between R2 ratio and peak metamorphic  
248 temperatures. However, this thermometer disregards the effects of mechanical modifications of the graphite structure, which  
249 this study has identified as having a substantial influence on graphite crystallinity in deformed rocks at sub-seismic  
250 velocities.

251 Our experiments demonstrate a shear strain-dependent increase of the R2 ratio of initially highly crystalline graphite powder  
252 due to shear deformation (Fig. 3; Table 2). In natural analogues, the pre-shear graphite would yield temperatures up to  $641 \pm$   
253  $50 ^{\circ}\text{C}$  (S1), which is the upper limit of the calibrated thermometer (Beysac et al. 2002). Whereas, the sheared samples  
254 would indicate peak metamorphic temperatures as low as  $347 \pm 50 ^{\circ}\text{C}$  (estimated from the most strained samples; S1). Thus,  
255 we experimentally prove that in active tectonic settings graphite thermometers may underestimate the peak metamorphic  
256 temperatures by  $< 300 ^{\circ}\text{C}$ . In cataclasites from the Alpine Fault zone, New Zealand (Kirilova et al., in review) and fault  
257 zones of the Hidaka metamorphic belt, Japan (Nakamura, et al., 2015), the graphite thermometer yields temperature



258 discrepancies of more than 100 °C compared to temperature estimates derived both from the surrounding high-grade  
259 amphibolite facies mylonites and the lower grade equilibrium cataclastic phases (marked by chlorite alteration). Barzoi  
260 (2015) also described differences of ~ 150 °C in graphite temperatures between strained and less strained low grade  
261 metamorphic rocks from Parang Mountains, South Carpathians.

262 We conclude that shear strain calibration of the current graphite thermometer is needed and we propose an appropriate  
263 adjustment based on our dataset. Fig. 3 illustrates good correlation between the average R2 and the shear strain measured  
264 within a sample, which can be described by the following equation (1):

$$265 \quad y = 495.9 * \gamma^{4.875} + 1.117 \text{ with a correlation coefficient } R^2 = 0.96 \quad (1)$$

266 where  $\gamma$  = shear strain.

267 However, a calibration of the existing graphite thermometer could be still insufficient to permit reliable temperature  
268 estimates in active tectonic settings because of the variable slip rates likely to be encountered in fault zones.

## 269 **5 Conclusions**

270 We have experimentally demonstrated that graphite crystallinity is not irreversible by performing shear deformation  
271 experiments at aseismic sliding velocities on graphite gouges composed of powdered highly-organized graphite. Our results  
272 clearly demonstrate significant decrease in graphite structural order, which is a function of the total shear strain attained  
273 during the various experiments. We also observed a trend of increasing shear strain within a sample with increase in the  
274 applied normal stresses and sliding velocities. This reveals the complexity of graphite structural modifications and highlights  
275 the significance of the various parameters that can affect the graphitization process. Furthermore, our findings compromise  
276 the validity of the calibrated graphite thermometers as they may underestimate the peak metamorphic temperatures in active  
277 tectonic settings. Thus, we tentatively suggest a shear strain calibration of these thermometers.

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343

344 **Table 1.** Summary of the conditions at which experiments were carried out and results.

345 **Table 2.** Summary of the relationship between shear strain and average R2 within a sample. The conditions of each  
346 experiment are also given as follows: applied normal stress in MPa, slip rates in  $\mu\text{m/s}$  and sliding displacement in mm.

347 **Figure 1.** Plots of mechanical data (a) friction coefficient,  $\mu$  vs. displacement (b), (c), (d) friction coefficient,  $\mu$  vs. shear  
348 strain.

349 **Figure 2.** Representative Raman spectra illustrating: (i) the most crystalline graphite (left column) within a sample; (ii)  
350 graphite with approximate average crystallinity per sample (middle column); and (iii) the most disordered graphite (right  
351 column) encountered in each sample. The R2 ratio for each spectrum is also noted in italic font.

352 **Figure 3.** Plot of the average R2 ratio vs shear strain accumulated during each experiment.

353 **Figure 4.** SEM images, obtained from the deformed graphite gouge during experiment 8 (normal stress at 25 MPa with 1  
354  $\mu\text{m/s}$  sliding velocity), show: (a) Slickenlines ornamenting the shear surface; (b), (c) A well-compacted layer of aligned  
355 graphite grains, which make up the shear surface. Bright patches due to a differential charging effect; (d) A less deformed  
356 zone with typical cataclastic fabric, underlying the shear surface; (e) Dilated cleavage planes in large graphite grains filled  
357 with smaller platy graphite grains oriented sub-perpendicular to the shear direction; (f) Fractured graphite grains.

358 **Supplementary material 1 (S1).** Raman data from 20 spectra per sample together with calculated R2 ratio and average R2  
359 value for each sample. The last column represents temperature estimated by the current best calibration of a Raman-based  
360 thermometer:  $T (^{\circ}\text{C}) = - 445 * R2 + 641 \pm 50$ .

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Experiment number	Normal stress (MPa)	Sliding velocity ( $\mu\text{m/s}$ )	Displacement (mm)	Peak friction ( $\mu_{\text{peak}}$ )	Steady state friction ( $\mu_{\text{ss}}$ )	Shear strain maximum ( $\gamma$ )
1	5	1	20	0.53	0.22	17.70
2	5	1	10	0.53	0.22	8.17
3	5	1	5	0.52	<i>not reached</i>	4.23
4	5	10	20	0.53	0.24	20.45
5	5	100	20	0.57	0.22	16.89
6	5	100	10	0.55	0.22	9.80
7	5	100	5	0.57	<i>not reached</i>	3.87
8	25	1	20	0.43	0.17	21.45
9	25	10	20	0.43	0.17	31.86
10	25	100	20	0.41	0.14	46.77

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363 **Table 1.** Summary of the conditions at which experiments were carried out and results.

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Sample	Experimental conditions	Shear strain ( $\gamma$ )	Average R2
<b>Pre-shear graphite</b>	N/A	N/A	0.173
<b>Exp. 2</b>	5 MPa, 1 $\mu\text{m/s}$ , 10 mm	8.17	0.438
<b>Exp. 6</b>	5 MPa, 100 $\mu\text{m/s}$ , 10 mm	9.80	0.430
<b>Exp. 5</b>	5 MPa, 100 $\mu\text{m/s}$ , 20 mm	16.89	0.454
<b>Exp. 1</b>	5 MPa, 1 $\mu\text{m/s}$ , 20 mm	17.70	0.506
<b>Exp. 4</b>	5 MPa, 10 $\mu\text{m/s}$ , 20 mm	20.45	0.517
<b>Exp. 8</b>	25 MPa, 1 $\mu\text{m/s}$ , 20 mm	21.45	0.520
<b>Exp. 9</b>	25 MPa, 10 $\mu\text{m/s}$ , 20 mm	31.86	0.580
<b>Exp. 10</b>	25 MPa, 100 $\mu\text{m/s}$ , 20 mm	46.77	0.604

377 **Table 2.** Summary of the relationship between shear strain and average R2 within a sample. The conditions of each  
378 experiment are also given as follows: applied normal stress in MPa, slip rates in  $\mu\text{m/s}$  and sliding displacement in mm.

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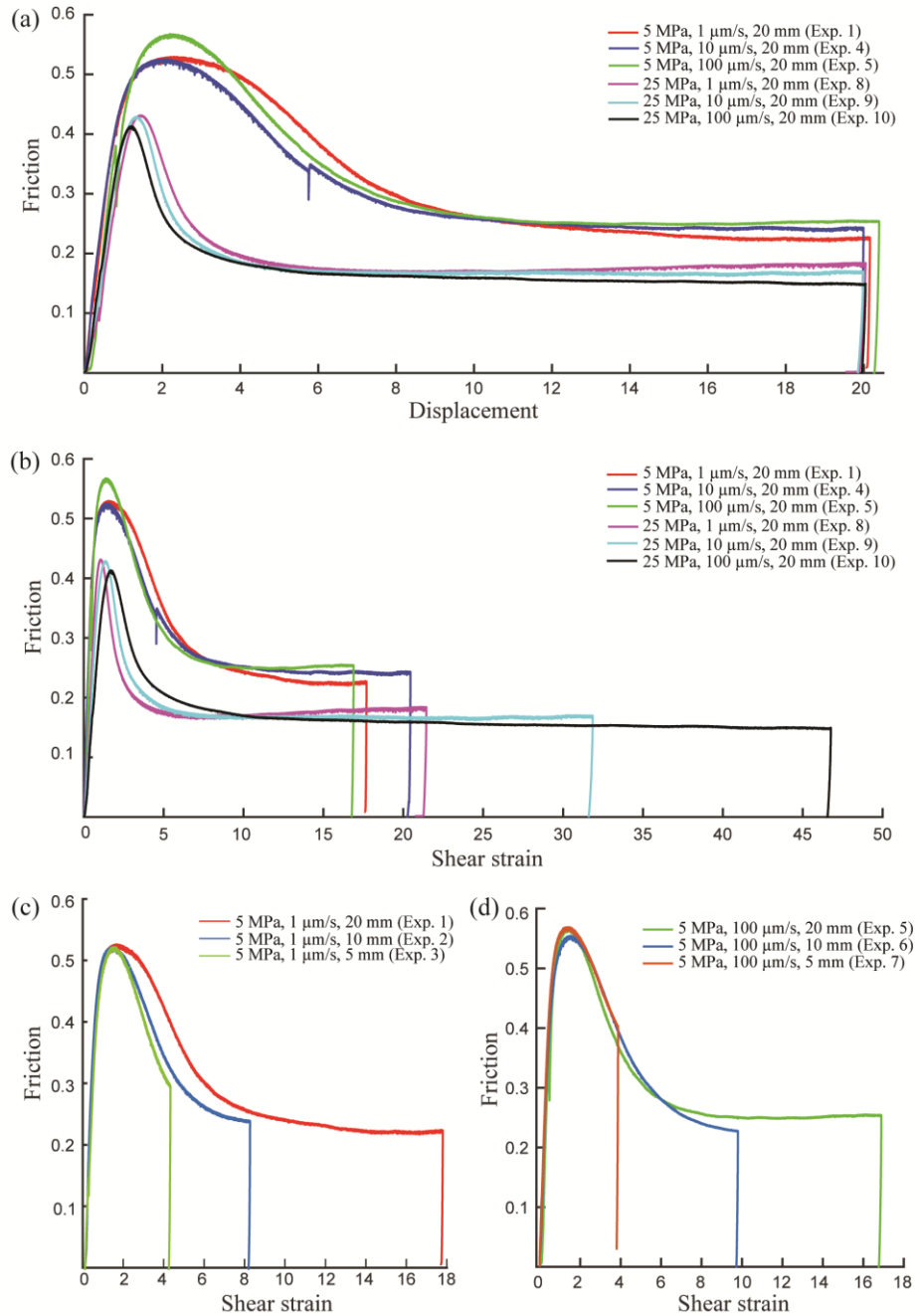
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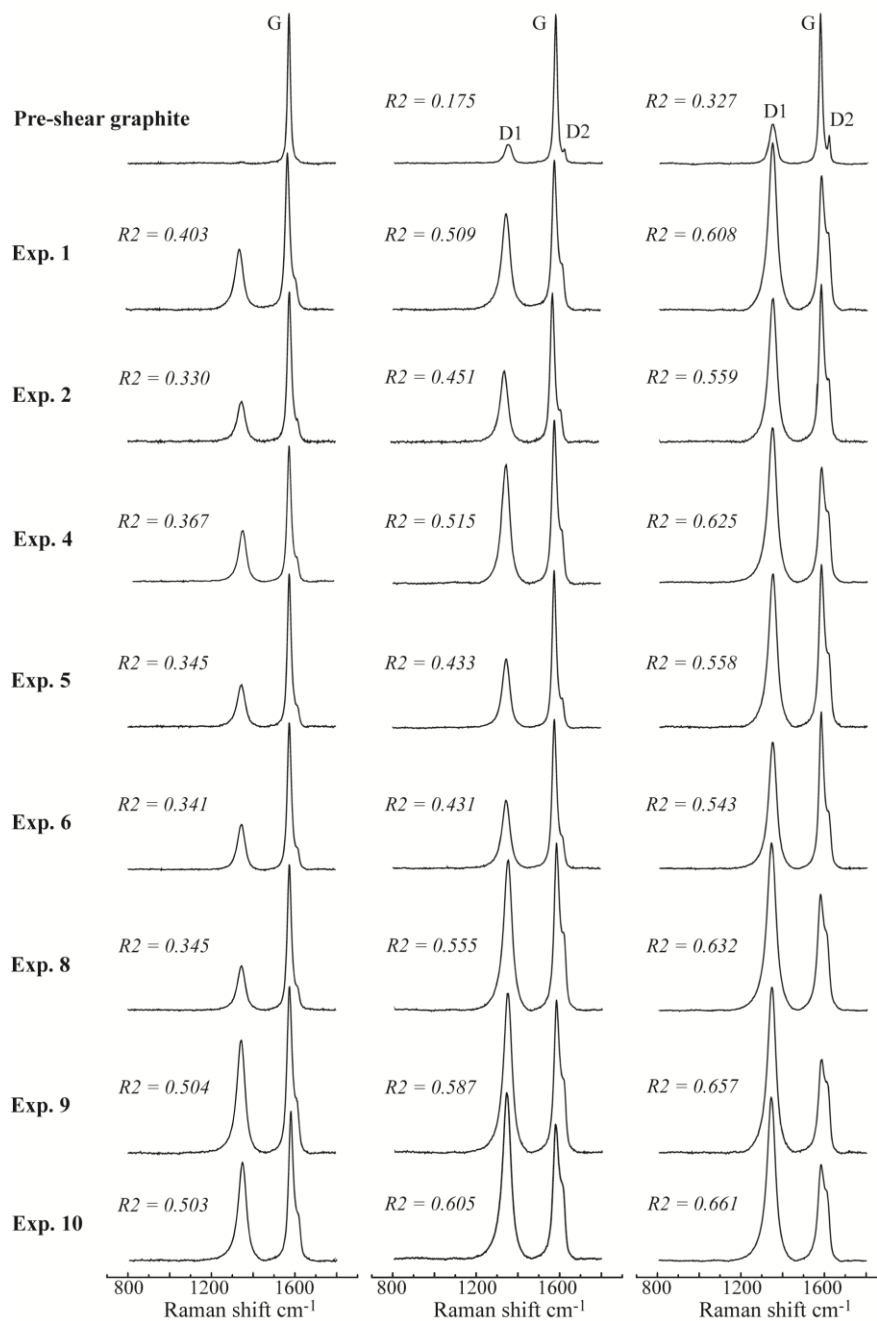




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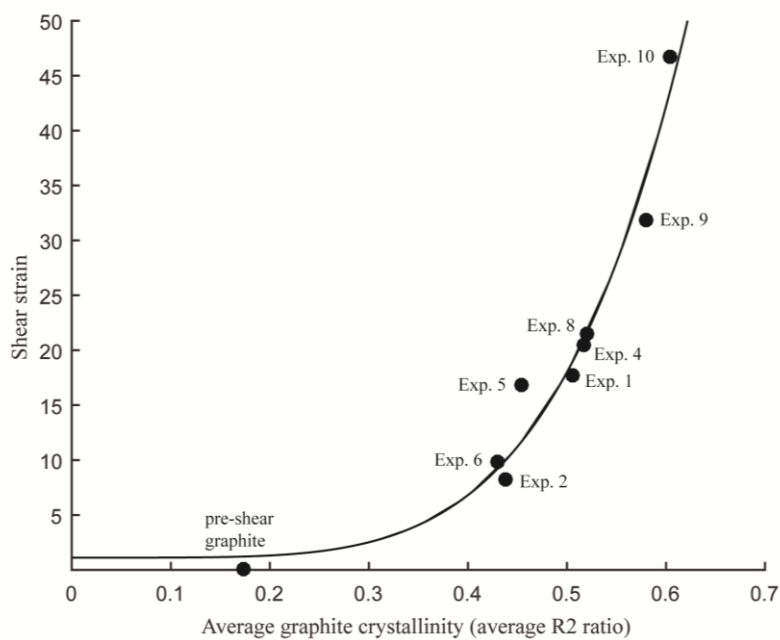


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400 **Figure 3.** Plot of the average R2 ratio vs shear strain accumulated during each experiment.

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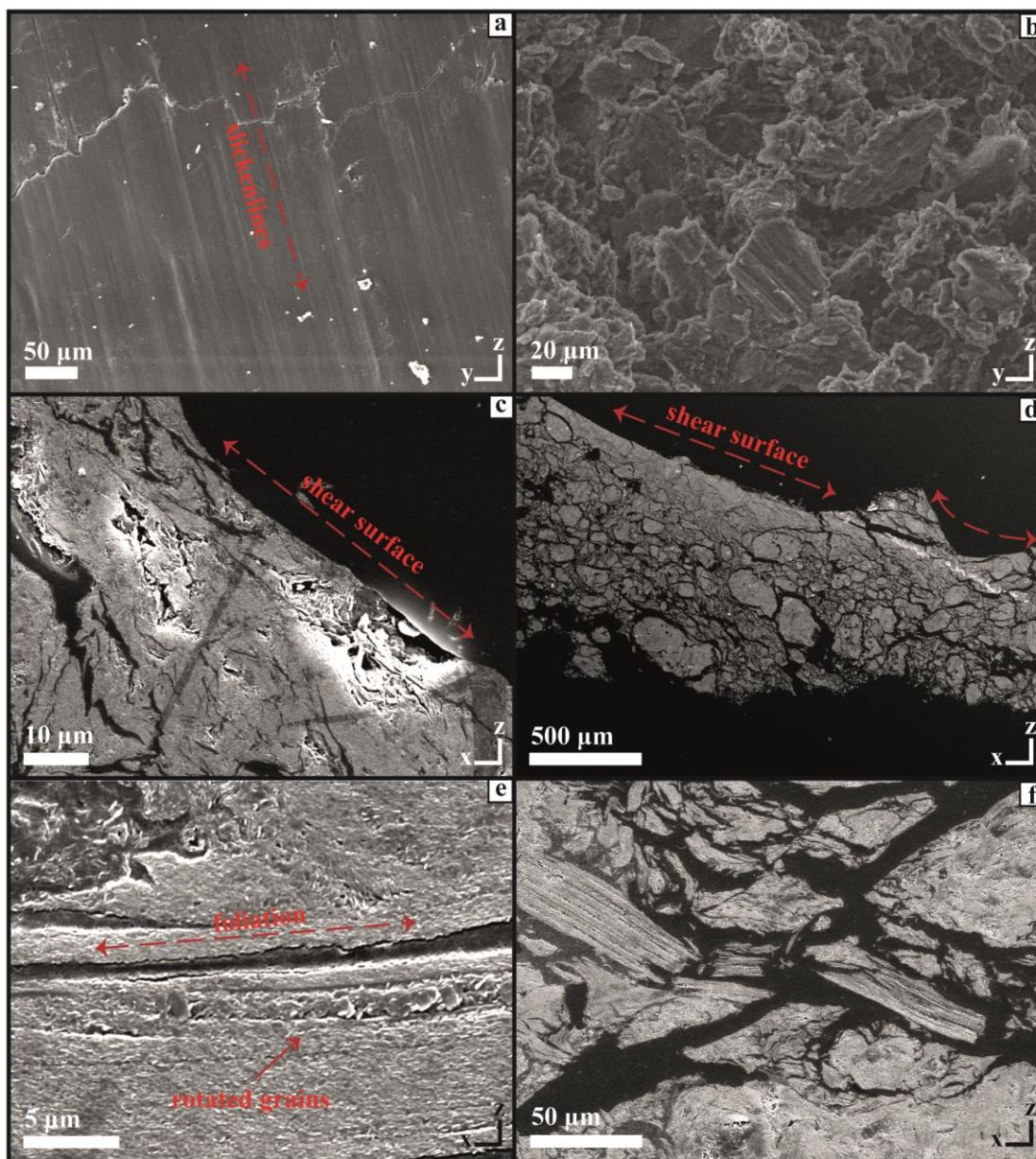
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