

# **Control of pre-existing fabric in fracture formation, reactivation and vein emplacement under variable fluid pressure conditions: An example from Archean Greenstone belt, India.**

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## **Abstract**

10 Most of the upper crustal fluid flows are strongly influenced by the pre-existing fractures/foliations in the rocks under a certain state of tectonic stress and fluid pressure condition. In the present study, we analyze a wide range of crosscutting fractures that are filled with quartz veins of variable orientations and thicknesses, from the gold bearing massive metabasalts (supracrustal) of the Chitradurga Schist Belt adjacent to the Chitradurga Shear Zone (CSZ), western Dharwar craton, south India. The study involves  
15 the following steps: 1) analyzing the internal magnetic fabric using anisotropy of magnetic susceptibility (AMS) studies, and strength of the host metabasalts, 2) quantifying the fluid pressure condition through lower hemisphere equal area projection of pole to veins by determining the driving pressure ratio ( $R'$ ), stress ratio ( $\phi$ ), and susceptibility to fracturing, and 3) deciphering the paleostress condition using fault  
20 slip analysis. We interpret that the NNW-SSE to NW-SE (mean  $337^\circ/69^\circ$  NE) oriented magnetic fabric in the rocks of the region developed during regional D1/D2 deformation on account of NE-SW shortening. However, D3 deformation manifested by NW-SE to E-W shortening led to the sinistral movement along

CSZ. As a consequence of this sinistral shearing, fractures with prominent orientations formed riedel shear components, with CSZ as the shear boundary. Subsequently, all the pre-existing fabrics along with the riedel shear components were reactivated and vein emplacement took place through episodic fluid pressure fluctuation from high to low  $P_f$  at shallow depth (~2.4 Km). However, NNW-SSE orientations were susceptible for reactivation under both high and low  $P_f$  conditions leading to a much greater thickness along the same. The deduced paleostress from fault-slip analysis, along with the kinematics of the fractures and veins are in good agreement with the previously revealed regional tectonics. Thus, integrating multiple domains of studies, help in the logical interpretation of fluid flow condition and vein emplacement mechanism in the study area that has not been ventured before.

## 1. Introduction

The upper crust is replete with fractures/faults, which act as pathways for fluid flow and vein emplacement. Fracture formation and vein emplacement mechanisms are closely interrelated, and require a detailed study for finding out potential hydrothermal deposits. Fracture formation and reactivation involves a combination of regional stress field (far field stress), stress ratio ( $\Phi$ ) and driving pressure ratio ( $R'$ ) that helps to determine the prevailing fluid pressure condition (Delaney et al., 1986; Jolly and Sanderson, 1997; McKeagney et al., 2004; Mazzarini, 2007; Martinez-Poza et al., 2016; Cucci et al., 2017). However, previous studies suggest that pre-existing anisotropy in host rocks play a significant role in formation and propagation of fractures provided the anisotropy is favorably oriented to the far field stresses (Ikari et al., 2015; Donath, 1961; Hoek, 1964; Attwell and Sandford, 1974). Presence of such

favorably oriented anisotropy lowers the shear strength of the host rocks, enabling failure/slip along them at minimum compressive stress, prior to/during vein emplacement. Such conduits are reactivated at both high and low fluid pressures forming pathways for fluid flow (Mondal and Mamtani 2013, Lahiri and Mamtani, 2016). Thus, vein emplacement mechanism requires fracture orientations that can be reactivated, when fluid pressure gradually builds and exceeds the normal stresses acting on the fracture wall (Gudmundsson, 2011). This enables dilation of the fracture planes, a mechanism known as *fault-valve action* (Sibson et al., 1988; Sibson, 1992, 1996, 2000; Boullier and Robert, 1992; Sibson and Scott, 1998; Petit et al., 1999; Cox et al., 2001 among others). Subsequently, fluid flows into the fractures, a phenomenon analogous to *burping*, triggering an immediate drop in fluid pressure. This sudden drop in fluid pressure is responsible for mineral deposition and vein formation (Cox et al., 1991, Cox, 1995; 2001). Vein materials thus deposited seals the fracture/fault planes, preparing the system for the next cycle of fluid pressure build up, rupture, fluid flow and vein formation (Mondal and Mamtani, 2013; Lahiri and Mamtani, 2016; Marchesini et al., 2019). Thus, repeated cycles of elevated and depleted fluid pressure generate criss-cross pattern in veins. Such intricate studies regarding the mechanism of fabric development and fracture formation vis-à-vis vein emplacement helps to provide a detailed insight about the development of brittle structures and their role in understanding the tectonic evolution of Archean cratons.



The Chitradurga Schist belt (western Dharwar craton, south India), is a NW-SE trending Archean greenstone belt, known to harbor a widespread network of veins with potential epigenetic gold bearing lodes (Gupta et al., 2014; Gopalakrishna et al., 2018). We have conducted this study in the meta-volcanic (metabasalt), hosting quartz veins of variable orientations and thicknesses, in and around Chitradurga

region. We emphasize on understanding the mechanism of vein emplacement under a tectonic environment where propensity of fracture reactivation for vein emplacement is mutually dependent on both fluid pressure condition and the regional far field stresses. The present paper is a comprehensive work which quantifies the fabric in the visually isotropic metabasalts of the Chitradurga Greenstone belt and its role in fracture instigation and in channelizing upper crustal fluids. We also found the reactivation potential of the fractures/faults at variable fluid pressure conditions to investigate the role of fractures/faults which are not favorably oriented to the pre-existing anisotropy and regional stress field, and their contribution towards vein emplacement in the study area.

## **2. Geology of the study area**

The study has been conducted in the Chitradurga Greenstone Belt of Dharwar craton (southern India; Fig. 1a), which represents a complex geological history. Dharwar craton exposes >3.0 Ga, Archean continental crusts, represented by the TTG (trondjemite-tonalite-granodiorite gneiss) also known as the peninsular gneiss (Jayananda et al., 2006). The craton stabilized during the accretion of Eastern Dharwar Craton (EDC) and Western Dharwar Craton (WDC) at 2.75-2.51 Ga. The zone of accretion of the two tectonic blocks is marked by a shear zone, referred to as Chitradurga Shear Zone (e.g., Naqvi and Rogers, 1987; Chadwick et al., 2003; Jayananda et al. 2006). The eastern part of WDC marked by Chitradurga Schist Belt (CSB) (Fig. 1b), comprises of peninsular gneiss (3.4-3.0 Ga), and younger supracrustal rocks (Beckinsale et al., 1980; Sarma et al., 2011; Taylor et al., 1984). The latter comprises metavolcanics/metabasalts (greenstone belt; greenschist/lower amphibolite facies metamorphism), metamorphosed greywacke-argillite (interbanded with ferruginous chert and banded iron formation),

polymict conglomerate, and ferruginous chert. It is believed that the basaltic rocks of the schist belt have  
85 an island arc affinity (Chakrabarti et al., 2006). Regionally, the belt is surrounded by older peninsular  
gneisses and younger granitoids (Ramakrishna and Vaidyanadhan, 2010). Previous geological  
investigations, revealed the presence of various younger granites ~2.6 Ga; (Jayananda et al., 2006;  
Chardon et al., 2002) which are associated with the schist belt, such as Chitradurga granite, J. N. Kote  
granite. The structural investigations of the adjacent meta-sedimentary rocks of the region show that the  
90 area has undergone three phases of deformation: D1, D2 and D3 respectively (Chadwick et al., 1989;  
Jayananda et al., 2006; Mondal and Mamtani, 2014). The D1/D2 deformations are coaxial with NW-SE  
striking axial plane. D1 folds are tight to isoclinal and asymmetric while the D2 folds are open to tight  
and upright. Earlier studies revealed that the folds (regional open; NE-SW striking vertical axial plane),  
related to early D3 deformation superposed the D1/D2 structures thus resulting in dome-basin geometry  
95 in the meta-sedimentary rocks of that region (Chakrabarti et al., 2006; Mondal and Mamtani, 2014).  
However, later phase of D3 deformation led to the formation of brittle structures in the younger granites  
of CSB (Mondal and Mamtani, 2016). The NE-SW shortening during D1/D2 deformation was responsible  
for NW-SE oriented structural elements in the CSB (Chadwick et al., 2003), while NW-SE to E-W  
shortening direction prevailed during D3 deformation (Jayananda et al., 2006; Mondal, 2018; Mondal and  
100 Acharyya, 2018). A number of petrological and geochemical investigations have been carried out on the  
area in the past. These studies suggest the presence of actinolite, albite, chlorite, epidote, quartz and calcite  
in the basaltic rocks (Chakrabarti et al., 2006). The CSB holds evidence of progressive metamorphism  
with a gradual increase in P-T conditions (approximately 3-4 Kb of pressure), from greenschist facies in  
north to amphibolite facies in south suggesting the depth of deformation to be 10-12 Km (during D1/D2).

105 However, recent studies by Acharyya and Mondal, (2019) shows that the brittle deformation during late D3 took place at a shallow depth of ~2-4 km. The dashed rectangular area in figure 1b demarcates the study area. The present study focuses on the dark greyish to blackish, massive to fine grained, altered metabasalt hosting quartz veins, of the region surrounded by meta-sedimentary sequences (Fig. 2). The metabasalts of the study area are devoid of any well-defined field foliation. The foliation planes in the adjacent meta-sedimentary rocks of the region are found to be NW-SE oriented (mean strike/dip is 323°/71° NE). Since, the metabasalts are devoid of mesoscopic field fabric, the anisotropy of magnetic susceptibility (AMS) study has been conducted in order to quantify the internal magnetic fabric in them.

### 3. Overview of brittle structures

115 Metabasalts of the study area are replete with fractures and faults of multiple orientations. Some of these fractures and faults are found to host quartz veins forming criss-cross pattern (Fig. 3a and c) and some of them are devoid of any vein material. Growth of vein materials (quartz crystals) are often found to be perpendicular to the vein wall suggesting that dilation was significant in these veins (Fig.3b). The maximum width and length of the quartz veins are recorded to be ~1 meter and ~130 meters respectively.

120 Some of the quartz veins are found to be displaced by other ones forming crisscross network of veins in the study area (Fig. 3c). Wing cracks filled up with quartz veins are commonly observed (Fig. 3d). At few places, the thicker quartz veins are replete with series of successive fault planes with slickenside lineations on them (Fig. 3e and *in-set*). Those veins are often found to enclose angular metabasalt enclaves (host material, Fig. 3f), suggesting that fault valve action was predominant in the region. Some of the fault planes recorded in the study area have shallow plunging slickenside lineations while others have moderate

to high. Both Left Lateral Faults (LLF's) and Right Lateral Faults (RLF's) are recorded based on the movement of the hanging wall with respect to the footwall. Presence of congruous steps helps in the discrete identification of the fault planes (Fig. 3g). Although, quartz veins of variable orientations and thicknesses are found, however, most of the veins are predominantly NNW-SSE trending (Fig. 4a). Most  
130 of the fractures and faults show NNW-SSE trend (maxima) whereas some others form a WNW-ESE to NE-SW sub maxima respectively (Fig. 4b & 4c). Some WNW-ESE trending Mode-I (tensional) cracks with prominent tips are also recorded from the study area which are often filled up with quartz veins. It may be noted that the veins with maximum thicknesses are oriented along NNW-SSE direction (Fig. 4d). In this study, 992 fracture data (strike/dip), 378 vein data (strike, dip and thickness) and 73 fault data  
135 (strike, dip and slip) have been measured from the metabasalt exposures of about 13 locations in the entire study area. All 73 shallow to moderately plunging fault planes are used to decipher the paleostress condition. Thus, integrating field observations and data obtained from brittle structures enables to reconstruct the tectonic stress conditions of the craton and helps to quantify the fluid pressure conditions that prevailed during fracture reactivation and vein emplacement.

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#### **4. Methods of analysis and results**

The quartz veins have been emplaced in the massive metabasalts of the region that are devoid of any prominent mesoscopic foliation as mentioned above. At places, veins of one orientation are dissected and sometimes displaced by others that led to the formation of mesh like structures (Fig. 3a, c). Sibson  
145 (1992) has mentioned that such a mesh is formed when a rock contains fractures of varying orientations that may get reactivated due to rise in fluid pressure. It is mentioned that in the Chitradurga region, veins

of various orientations show mutually cross-cutting relationships, which implies repeated cycles of vein emplacement (see sect.-3 and Sibson, 1992). Although veins have various orientations, NNW-SSE striking veins are the most common (Fig. 4a). It may be noted that NW-SE to NNW-SSE direction, which  
150 defines the maximum strike orientation of quartz veins, fractures and faults, is also the orientation of the adjacent Chitradurga shear zone, the overall trend of the schist belt. This implies that there is a strong structural control on the formation of these quartz veins. It has been shown earlier that the pre-existing anisotropy plays a critical role in propagating fractures and channelizing fluid in rocks (Sanderson and Zhang, 1999, Cox et al., 2001 and Ikari et al., 2015). It is also known from rock mechanics investigations  
155 that the rock strength variation controls the strain partitioning and influences fluid flow (e.g., Tsidzi, 1990; Vishnu et al 2018). Therefore, it is crucial to determine the rock fabric and state of stresses in order to understand the upper crustal fluid flow vis-à-vis vein formation.

In the past, 3-D Mohr circle analysis has been performed by Jolly and Sanderson (1997) using dyke orientation data to examine the magma pressure condition that was responsible for the opening of pre-  
160 existing fractures during dyke emplacement. Further the work has been extended to understand the fluid pressure condition and vein emplacement mechanism by McKeagney et al., 2004 (also see Yamaji et al., 2010). We present vein orientation data from the Chitradurga region (southern India), which is a province of epigenetic gold deposit (Gupta et al., 2014; Gopalakrishna et al., 2018).

We conduct anisotropy of magnetic susceptibility (AMS) study, followed by Brazilian Tensile  
165 strength (BTS) determination in order to quantify the internal magnetic fabric and tensile strength of the rocks within the study area. The 3-D Mohr circle construction using quartz vein orientation data helps to recognise the fluid pressure conditions under which they were emplaced. Further, these fluid pressure



conditions were integrated with dilation tendency, slip tendency and fracture susceptibility in order to understand the mechanism of vein emplacement in the Chitradurga region. A combination of data  
170 obtained from these methods along with paleostress analysis using fault-slip data recorded from the study area provides a comprehensive evaluation of vein forming conditions in Chitradurga greenstone belt.

#### ***4.1 Anisotropy of Magnetic Susceptibility (AMS)***

The quartz veins occur in massive metabasalt, which does not show any visible field foliation.  
175 However, such visibly massive rocks may preserve an internal fabric, which can be recognized on the basis of anisotropy of magnetic susceptibility (AMS) studies (e.g., Tarling and Hrouda, 1993; Maffione et al., 2015; Mamtani and Greiling, 2005; Raposo et al., 2007; Looock et al., 2008; Mondal and Mamtani, 2014; Mondal, 2018). The study involves preparation of cylindrical core samples (25.4 mm diameter  $\times$  22 mm height) from oriented metabasalt blocks. These metabasalt block samples have been collected from  
180 13 different locations (Fig. 5) in the study area. The prepared core samples are subjected to an external magnetic field and the induced magnetization for each core sample is measured in different directions. AMS is considered to be a symmetric second-rank tensor, represented by an ellipsoid with three mutually perpendicular stress axes,  $K_1$ ,  $K_2$  and  $K_3$  respectively where ( $K_1 \geq K_2 \geq K_3$ ). The orientation and magnitude of each of these principle axes are determined in this analysis, where  $K_1$  represents the magnetic lineation,  
185  $K_3$  is the pole to the magnetic foliation ( $K_1 K_2$ ). Using the magnitudes of  $K_1$ ,  $K_2$  and  $K_3$ , several AMS parameters are calculated such as magnetic susceptibility ( $K_m$ ), magnitude of the magnetic foliation (F) and magnetic lineation (L), degree of magnetic anisotropy ( $P_j$  or  $P'$ ) and shape parameter (T). The formulae for the parameters are given below (after Tarling and Hrouda, 1993; Jelínek, 1981):

$$K_m = (K_1 + K_2 + K_3) / 3 . \quad (1)$$

$$190 \quad F = (K_2 - K_3) / K_m . \quad (2)$$

$$L = (K_1 - K_2) / K_m . \quad (3)$$

$$P_j = \exp \sqrt{2 [(\eta_1 - \eta_m)^2 + (\eta_2 - \eta_m)^2 + (\eta_3 - \eta_m)^2]} . \quad (4)$$

$$T = (2\eta_2 - \eta_1 - \eta_3) / (\eta_1 - \eta_3) . \quad (5)$$

Here,  $\eta_1 = \ln K_1$ ,  $\eta_2 = \ln K_2$ ,  $\eta_3 = \ln K_3$  and  $\eta_m = (\eta_1 \cdot \eta_2 \cdot \eta_3)^{1/3}$ . In the above equations,  $P_j$  and  $T$  give the  
 195 measure of the eccentricity and shape of the AMS ellipsoid respectively. The value of  $T$  ranges between  
 -1 to +1. Positive and negative values represent oblate and prolate shapes of the AMS ellipsoid (Tarling  
 and Hrouda, 1993).

AMS measurements have been conducted in the spinner mode (field intensity of  $300 \text{ Am}^{-1}$ ) using  
 the KLY-4S Kappabridge (AGICO, Czech Republic); see Hrouda et al. (2006) for instrument details. The  
 200 SUFAR program has been used to calculate the required AMS parameters described above for each  
 sample. A total of 65 cores are prepared and analysed. The mean value of the AMS parameters at each  
 location site is calculated using the program Anisoft (version 4.2, AGICO; Jelinek statistics, Jelinek,  
 1981). It is noted that the  $K_m$  varies between 37 and  $1280 \times 10^{-6}$  SI units, with most of the samples having  
 $K_m$  below  $1000 \times 10^{-6}$  SI units (see supplementary sheet-1). This indicates that paramagnetic and  
 205 ferromagnetic minerals contribute significantly to the AMS. Petrographic studies reveal the presence of  
 actinolite, hornblende, chlorite, albite, epidote, pyrite which are inferred to contribute to the  
 susceptibilities recorded in the samples. The  $P_j$  lies between 1.003 and 1.539, and the shape of the AMS  
 ellipsoid is dominantly oblate (positive  $T$  values; see supplementary sheet-1). It is noted that the magnetic

foliation ( $K_1K_2$  plane) is consistently NW-SE striking (mean orientation:  $337^\circ/69^\circ$  towards NE; Fig. 5a).

210 The magnetic lineations plunge variably from NNW, through sub-vertical to SSE (Fig. 5b).

#### ***4.2 Tensile strength determination***

It is known that the dilation occurs in a direction parallel to the minimum compressive principal stress ( $\sigma_3$ ), when the fluid pressure ( $P_f$ ) exceeds the normal stress acting on the fracture wall.

215 Therefore the fractures may occur at any depth when the effective stress ( $\sigma_3 - P_f$ ) is sufficient to counteract the tensile strength ( $T$ ) of the rocks (see Fig.10c; Gudmundsson, 2011). We measure the tensile strength of the host metabasalts to quantify the  $P_f$  that prevailed during vein emplacement in the region. The measurement of direct tensile strength requires machined specimens and also involves difficulty in applying tensile load on the cylindrical specimen during analysis. Therefore,  
220 tensile strength measurement of rocks using Brazilian test has become imperative in rock mechanics. Compression-induced extensional fractures are generated in the test which essentially involves line-loading on a circular disk placed between two platens (Aydin and Basu, 2006; Basu et al., 2013; see Fig.6). This tensile strength ( $T$ ) is estimated from the elastic theory (ISRM, 1978; ASTM D3967, 2001):

$$225 \quad T = \frac{2P}{\pi LD} . \quad (6)$$

Here,  $P$  is peak/failure load, and  $L$  and  $D$ , are the length and diameter of the disk respectively. For this analysis, 18 core samples were drilled from metabasalt blocks which were later resized to obtain the desirable cores for the analysis (length: diameter = 1: 2). The maximum tensile strength of each specimen at the instance of failure is recorded. The maximum tensile strength for 18 samples are averaged out to

230 obtain the approximate tensile strength of metabasalts, which is ~12 MPa. This tensile strength value is further used for quantifying the  $P_f$  in 3D Mohr circle using vein orientation data.

#### ***4.4 Fluid pressure determination***

Here, we have used the method proposed by Jolly and Sanderson (1997) to quantify the  $P_f$  conditions that  
235 led to the vein emplacement in metabasalts of Chitradurga region (southern India). We have used the lower hemisphere equal area projection of the poles to quartz vein data. According to Jolly and Sanderson (1997), girdle distribution of vein pole data implies  $P_f > \sigma_2$ , described as a condition where large number of fracture orientations are susceptible to reactivate, while  $P_f < \sigma_2$  represents clustered distribution of vein pole data, where only limited range of fracture orientations reactivate. Depending on the type of  
240 distribution (girdle/cluster), parameters such as stress ratio ( $\phi$ ) and driving pressure ratio ( $R'$ ) are

calculated using ranges of fracture orientations ( $\theta_1$ ,  $\theta_2$  and  $\theta_3$ ) from the following equations provided by Jolly and Sanderson, 1997 and Baer et al., 1994.

$$R' = \frac{P_f - \sigma_3}{\sigma_1 - \sigma_3} = \frac{1 + \cos 2\theta_2}{2}. \quad (7)$$


For  $P_f > \sigma_2$ ,

$$\Phi = \frac{\sigma_2 - \sigma_3}{\sigma_1 - \sigma_3} = 1 - \frac{1 - \cos 2\theta_2}{1 - \cos 2\theta_3}. \quad (8)$$

For  $P_f < \sigma_2$ ,

$$\Phi = \frac{\sigma_2 - \sigma_3}{\sigma_1 - \sigma_3} = \frac{1 + \cos 2\theta_2}{1 + \cos 2\theta_1}. \quad (9)$$

In figure 7a, the lower hemisphere equal area projection of pole to vein data shows girdle distribution, implying high fluid pressure condition ( $P_f > \sigma_2$ ). From this distribution the orientations of the principle stress axes ( $\sigma_1$ ,  $\sigma_2$  and  $\sigma_3$ ) are determined using the Bingham statistics of the Stereonet 9 software (<http://www.geo.cornell.edu/geology/faculty/RWA/programs/stereonet.html>).  $\sigma_1$  is sub-vertical lying in the empty space devoid of any vein pole data. Subsequently, following Jolly and Sanderson (1997), the planes  $\sigma_1\sigma_2$ ,  $\sigma_1\sigma_3$  and  $\sigma_2\sigma_3$  are constructed and the range of fracture orientations,  $\theta_2$  and  $\theta_3$  are determined along the  $\sigma_1\sigma_3$  and  $\sigma_1\sigma_2$  planes respectively. For this high  $P_f$  condition,  $\theta_2 = 17^\circ$ ,  $\theta_3 = 59^\circ$  from which  $\phi = 0.72$  and  $R' = 0.8$  are calculated. Thus, such a  $P_f$  condition enhances the chances of vein emplacement along various orientations. Although pole to vein data represents a girdle distribution pattern, however the highest density cluster is found around  $\sigma_3$  indicating a number of veins with similar orientations. This suggests that the vein forming fluid along these orientations must have been channelized through a pre-existing anisotropy (along a preferred orientation). These data are segregated and plotted separately

260 in the lower hemisphere equal area projection and thus the obtained contour defines the SW cluster (see.  
 Fig. 7c). The orientations of the principle stress axes ( $\sigma_1$ ,  $\sigma_2$  and  $\sigma_3$ ) are determined using the Bingham  
 statistics of the Stereonet 9 software. Similarly the  $\sigma_1\sigma_2$ ,  $\sigma_1\sigma_3$  and  $\sigma_2\sigma_3$  planes are constructed and the  
 range of fracture orientations  $\theta_1$  and  $\theta_2$ , are calculated along the  $\sigma_2\sigma_3$  and  $\sigma_1\sigma_3$  planes. Again, for low  $P_f$   
 condition,  $\theta_1 = 38^\circ$ ,  $\theta_2 = 43.2^\circ$ ,  $\phi = 0.85$  and  $R' = 0.53$ . This implies that under low fluid pressure condition  
 265 ( $P_f < \sigma_2$ ) only limited range of fracture orientations are susceptible to reactivate. In each case, for  
 determining the absolute  $P_f$  magnitude, pole to vein data are plotted in 3D Mohr circles. Recent studies  
 by Mondal and Acharyya (2018), documented the depth of faulting and fracturing in close vicinity of the  
 study area (Chitradurga granite) to be  $\sim 2.4$  km. Similar depth of fracturing has also been reported by  
 Acharyya and Mondal (2019), from the elliptical clasts of conglomerate bed within the Chitradurga schist  
 270 belt. We have considered this depth for determining the magnitude of the maximum compressive stress  
 ( $\sigma_1$ ) during fracture formation, using  $\sigma_1 = h\rho g$ , where  $h$  = depth of fracturing in metabasalts ( $\sim 2.4$  km),  $\rho$  =  
 approximate bulk density of crust (2700 kg/m<sup>3</sup>),  $g = 9.8$  m/sec<sup>2</sup>. Therefore,  $\sigma_1 \geq 63.5$  MPa, when depth  
 of fracturing in metabasalt  $\sim 2.4$  km. Tensile strength of metabasalt ( $\sim 12$  MPa; obtained from  studies)  
 indicates that the minimum compressive stress ( $\sigma_3$ ) has to be  $\sigma_3 \geq 12$  MPa. In each case we consider the  
 275 limiting values for both maximum and minimum compressive stresses. Magnitude for the intermediate  
 compressive stress ( $\sigma_2$ ) is determined using the respective stress ratios ( $\phi$ ) for both high and low  $P_f$   
 respectively. Following Jolly and Sanderson (1997), the 3D Mohr circles are constructed using the above  
 magnitudes of principle stresses and the angles determining the range of fracture orientations. Thus, well-

defined  $P_f$  lines for both high  $P_f$  ( $P_f=53.2$  MPa; Fig. 7b) and low  $P_f$  ( $P_f=39.3$  MPa; Fig. 7d) conditions are  
280 obtained using the Fractend code (Github, 2017).

#### 4.5. Dilation tendency, slip tendency and fracture susceptibility

Dilation tendency ( $T_d$ ) and slip tendency ( $T_s$ ) determine the propensity of any fracture orientation to  
reactivate through dilation or shearing, under a certain state of stress condition  
285 (Mazzarini, 2019). While, high dilation tendency ensures reactivation through dilation, high slip tendency  
elevates chances of opening through shearing (Ferrill et al., 1999). According to, Stephens et al., 2017,  
fracture planes suffer dilation when the difference between  $\sigma_1$  and the normal stress acting on the plane  
is close enough to the magnitude of differential stress ( $\sigma_D = \sigma_1 - \sigma_3$ ) and  $T_d = (\sigma_1 - \sigma_n) / \sigma_D$ . Slip tendency is  
denoted by the ratio of shear stress ( $\sigma_s$ ) to normal stress ( $\sigma_n$ ); ( $T_s = \sigma_s / \sigma_n$ ) and also depends on the frictional  
290 characteristics of the rock (Morris et al., 1996), along with the fracture plane orientation. Under a  
particular state of stress condition if the ratio of shear stress to normal stress is significantly large, then  
that particular fracture orientation is susceptible to reactivate. Fracture susceptibility ( $S_f$ ), is defined as  
the variation of fluid pressure ( $\Delta P_f$ ) within a fracture plane that can lead to fluid induced shear reactivation  
(Mildren et al., 2002; Stephen et al., 2017). Such reactivations depend on the shear and normal stresses  
295 acting on the fracture plane, along with the cohesion ( $= 0$  in this case) and the static coefficient of friction  
( $\mu_s$ );  $S_f = \sigma_n - (\sigma_s / \mu_s)$ .

Lower hemisphere equal area projections (see Fig. 8) of the poles to fracture (vein-filled) data help us to  
understand the variation in dilation tendency, slip tendency and susceptibility of fractures with respect to  
their orientations, under both high and low  $P_f$  conditions. The diagrams are prepared using Fractend code

300 (Github, 2017). It is evident from figure 8a, that the dilation tendency is high for the fracture orientations which are at a high angle to the  $\sigma_3$  axis, i.e., pole to these fractures form a well-defined cluster around  $\sigma_3$ . These fractures show greater tendency towards dilational opening for both high and low  $P_f$  (Fig. 8a and b). For fracture orientations having higher slip tendency, i.e., susceptible to shear opening, pole to the fractures are at a low angle to the  $\sigma_3$  axis. The fracture planes are therefore oriented at an angle to the  
305 maximum compressive stress axis  $\sigma_1$ , condition favorable for shear reactivation for both, high and low  $P_f$  (Fig. 8c and d). Fracture susceptibility, which involves variation in fluid pressure ( $\Delta P_f$ ) is low for the fracture orientations having high dilation and slip tendencies, which indicates fluid-induced fracture reactivation in metabasalts (Fig. 8e and f) in the study area.

#### 310 **4.6Paleostress analysis**

The shallow to moderately plunging normal faults of the study area with prominent slip directions are used to determine the stress regime under which these fractures and faults were formed and reactivated. Fault-slip data (orientations of fault planes and slip directions) recorded from the field were used for paleostress determination. Several methods are proposed for paleostress analyses using fault-slip data (e.g. Angelier,  
315 1994; Dupin et al., 1993; Etchecopar et al., 1981; Gapais et al., 2000; Marrett and Allmendinger, 1990; Ramsay and Lisle, 2000; Twiss and Unruh, 1998; Yamaji, 2000; Žalohar and Vrabec, 2007 and the references therein). Since, the fault-slip analysis methods are well established, here we prefer to represent only the salient aspects. The fault-slip analysis can be divided into two categories based on whether the fault-slip data are viewed as representing kinematic or dynamic information (Blenkinsop 2006; Gapais et  
320 al. 2000; Twiss & Unruh, 1998) based on the following assumptions: (1) bulk state of stress is uniform





and movement on the fault planes are independent of each other; (2) slip on the fault plane occurs along the direction of the maximum resolved shear stress under a given stress state (Wallace–Bott Hypothesis); (3) faults are homogeneous and a part of the same tectonic event (Angelier, 1994; Gapais et al., 2000; Gephart & Forsyth, 1984; Twiss & Unruh, 1998). In this study, we have determined the paleostress  
325 direction, using fault-slip data measured from 73 shallow to moderately plunging normal faults (spatially distributed) in the metabasalt by Right Dihedron method. Since, some of the fault planes show variation in their strike orientations, the small amount of inhomogeneity in the data set is reduced in this process. Thus, the data sets are segregated methodically into homogeneous data subsets using the ‘Win\_Tensor’ software program (version 5.8.6; Delvaux and Sperner, 2003; Delvaux, 2011). In the present analysis all  
330 the collected data are represented in a single set and separation is done by using the Right Dihedron method without any sort of manual intervention. Following Delvaux and Sperner, 2003, the data is filtered on the basis of stress ratio ( $R$ ), orientation of the stress axes and symmetry of the measured sets. Out of 73 data, 30 data are accepted with a low value of counting deviation and nominal counting values of 0 and 100 for  $\sigma_1$  and  $\sigma_3$  respectively. Thus, the best fitted reduced stress tensor is obtained for the accepted  
335 data subset (30 out of 73 fault data; see Fig. 9) at a “C” quality ranking. It also provides the relative orientations of the principal stress axes, stress ratio ( $R = 0.72$ ) and stress regime index ( $R' = 1.25$ ). The NNE-SSW directed extension direction obtained from this paleostress analysis (see Fig. 9) coincides well with the regional D3 extension direction. Data rejected in this process to obtain the best fit stress tensor when treated separately yields a NNE-SSW oriented extension direction with small variations in the  $R$

340 and  $R'$  values. According to Delvaux and Sperner (2003), the obtained stress regime index indicates a pure-strike slip domain which is in a good agreement with sinistral shearing along CSZ.

## 5 Discussions

### 5.1 Fabric development vis-à-vis regional tectonics

345 It has been mentioned earlier that the metabasalts of the study area lack any distinct visible foliation. However, the AMS analysis suggests, a prominent NNW-SSE to NW-SE oriented magnetic fabric in metabasalts. This magnetic fabric also matches well with the field foliation of the meta-sedimentary sequences, surrounding the metabasalts and is also parallel to the regional trend of CSZ (see Fig. 2). This implies that the fabric in metabasalts of the study area must have been controlled by the regional  
350 deformation. Structural investigations suggest that the Chitradurga region was subjected to three deformational events-D1, D2 and D3 respectively. D1 and D2 were found to be coaxial and controlled by NE-SW shortening that led to the development of folds (NW-SE striking vertical axial plane), while D3 was controlled by NW-SE to E-W shortening, resulting in the development of NE-SW striking planar structures (Chakrabarti et al., 2006; Ramadass et al., 2003). The superposition of D3 over D1/D2 formed  
355 culmination and depression in the region (dome-basin structures; Type-I interference pattern) (Chakrabarti et al., 2006). Therefore, it is logical to infer that the magnetic fabric in metabasalts are also  
 related to the regional D1/D2 deformation under NE-SW directed shortening that generated the field  
foliation in the meta-sedimentary sequences. The magnetic lineations in the metabasalts are plunging due  
NNW through sub-vertical to SSE (Fig. 5b).  
 Earlier, these variations in the plunge of the magnetic  
360 lineations had been interpreted as a consequence of superposed deformation (e.g., Mantani and Sengupta,

2010; Mondal and Mamtani, 2013). Therefore, in the light of regional structural information and above discussions, it is inferred that these variations in magnetic lineations of the metabasalts are the manifestation of dome-basin geometry that were produced due to the superposition of D3 over D1/D2 regional deformation. Recently, Mondal (2018) documented similar results from the magnetic fabric  
365 analysis in adjacent Chitradurga granite. The studies by Bhatt et al., (2017); Mondal and Acharyya (2018), suggest that the D1/D2 deformation lasted between 2614 and 2555 Ma while the D3 deformation is approximated around ~2537 Ma.

### ***5.2 Control of regional far-field stress on developing the brittle structures in Chitradurga region.***

370 The above discussions suggest that (a) NNW-SSE oriented magnetic foliation developed during D1/D2 deformation under NE-SW directed shortening, (b) variation in plunge of magnetic lineation is a manifestation of dome-basin geometry on account of D3 deformation. It is argued that during D3 deformation under NW-SE to E-W directed shortening the CSZ evolved as a sinistral shear zone (Mondal and Acharyya, 2018). It may be noted that the angle between the mean orientation of the schist belt and  
375 the compression direction for D3 deformation are found to be ~45° which also supports the sinistral movement along Chitradurga shear boundary.

It is mentioned in sect. 2 and 3 that, the study area is replete with a number of brittle structures such as fractures, faults. At places, these fractures are filled-up with quartz veins and the present paper is aimed to understand the mechanism behind the formation of these veins. Therefore, it is now essential to  
380 evaluate whether and how this brittle structures and their kinematics can be fitted to the regional far-field stresses responsible for deformation in the Chitradurga region. The quartz vein orientation data from

northern part of the Chitradurga schist belt reveals that the vein emplacement took place during regional D3 deformation (Mondal and Mamtani, 2014). Recently, Mondal and Acharyya (2018), and Acharyya and Mondal (2019) suggested that the brittle structures (fractures/faults) in the Chitradurga granite (in close vicinity to the study area) are related to the D3 deformation. Moreover, paleostress investigation using fault-slip data also reveals NNE-SSW directed extension was dominant during D3 deformation. Apart from this, evidences of any later deformation, i.e., post D3 deformation, have not been recorded from the study area (from previous studies and as per our field observations). Thus, based on the present studies and above discussions, it is logically inferred that the formation of brittle structures (fractures/faults) as well as vein emplacement must be explained as a consequence of regional D3 deformation at a shallow depth. Mondal and Mamtani (2014) suggested that the Mulgund granite ( $2555 \pm 6$  Ma; Sarma et al., 2011), which lies in close vicinity to the metabasalts of the Chitradurga region, was emplaced syn-tectonically with CSZ. It is shown that the Mulgund granite underwent ductile deformation as it cooled and crystallized syntectonically with D3 deformation. The ductile deformation features in the granite were then superimposed by brittle structures during late D3, when the granite was fully solidified and had achieved a shallow depth (Mondal and Mamtani, 2016). Since both the lithologies (metabasalts and granite) have undergone same deformation and the fractures in them developed syntectonically with adjacent CSZ, it is favourable to interpret that the brittle structures, such as fractures and faults in metabasalts developed on account of late D3 deformation under NW-SE to E-W directed compression at a shallow depth of about  $\sim 2.4$  Km. For evaluating the nature (mode) of fracturing in the metabasalts of the study area, we used tensile strength (T) to be 12 MPa (from BTS studies). We estimated  $\Delta\sigma = 51.5$  MPa, which is greater than  $4T$ , suggesting that the fractures in the metabasalts are not purely tensile except

for the cracks parallel to D3 shortening direction. However, the calculated value of  $\Delta\sigma$  is less than  $5.7T$ , indicating that the normal stress on the fractures are not purely compressive also. Therefore the value of  $\Delta\sigma$  satisfies  $4T < \sigma_1 - \sigma_3 < 5.7 T$  (Sibson, 2000), indicating that these fractures in the study area are extensional shear mode fractures.

### ***5.3 Regional tectonics and the mechanism of fracturing, faulting***

We discussed earlier in sect. -3, that the fractures and faults recorded in the metabasalts show a wide range of orientations with a NNW-SSE maxima and a WNW-ESE to NE-SW sub-maxima respectively (Fig. 4b). Among which, fractures trending along WNW-ESE to E-W are sub-parallel to the D3 (late phase) shortening direction. As previously mentioned in sect. -3, these WNW-ESE trending fractures have been regarded as tensional fractures. Similar orientations have also been recorded and interpreted as tensile fractures from the micro-granitoid enclaves in Chitradurga granite as evident from the studies of Mondal and Acharyya (2018). However, it is essential to explain the predominance of fractures and faults along the NNW-SSE orientation (forming the maxima). In order to explain this, we refer to the pre-existing fabric in the metabasalts of the study area, i.e., the NNW-SSE to NW-SE oriented magnetic fabric developed during D1/D2 regional deformation (Fig. 5a). Earlier studies suggest, that fractures are more likely to propagate along a pre-existing anisotropy, if and when the anisotropy is favorably oriented with respect to the regional stress field (Ikari et al., 2015). The CSZ being a sinistral shear zone exhibits a pure strike slip stress regime, coeval with D3 deformation (NW-SE to E-W directed shortening).

In the later phase of D3 deformation, the favorably oriented NNW-SSE fabrics were reactivated under a congenial stress field, thereby, causing reactivation of the pre-existing fabrics in the metabasalts. This

however, fails to justify the occurrence of the ~NW-SE and ~NE-SW oriented fractures within the  
425 metabasalts. From field investigations, the NE-SW oriented fractures show dextral movements, while the  
NNW-SSE and NW-SE oriented fractures are recorded with sinistral movements respectively (see Fig.  
3c and d). However, the fracture disposition and consistency in their respective orientations indicate that  
all of these fractures are related to the same deformational event and have been reactivated under similar  
stress conditions. Moreover, any other brittle deformational event post D3, have not been recorded from  
430 the study area as mentioned earlier. Therefore, we need to explain the occurrence of such variably oriented  
fractures/faults within a single kinematic framework. The NNW-SSE and NW-SE orientations are most  
likely to be sinistral, whereas NE-SW orientations form the dextral shear components respectively,  
considering CSZ to be the sinistral shear boundary. (See Fig. 10b and 4b, c). Thus, the NNW-SSE to NW-  
SE (P, Y and R) and the NE-SW to ENE-WSW (X and R') fractures coincide with the shear components  
435 of a riedel shear system considering the angle of internal friction ( $\Phi$ ) in metabasalts of the study area to be  
~30°. It may be noted that the value of  $\Phi$  is approximated from the Uniaxial Compressive Strength (UCS)  
studies of the metabasalts core samples following Sivakugan et al., 2014. These fracture planes acted as  
pathways for fluid flow and vein emplacement during the late D3 deformation.

#### 440 ***5.4 Understanding the mechanism of fluid flow and vein emplacement in Chitradurga region***

In order to explain the vein emplacement mechanism along these weak zones we need to consider the  
fluid pressure conditions that prevailed in the study area. In sect. 4.4, we mentioned earlier that the lower  
hemisphere equal area projection of pole to vein data shows girdle distribution, indicating high  $P_f$   
condition (~53.2 MPa;  $>\sigma_2$ ) in the study area. Under such high  $P_f$  conditions, veins were emplaced along

all possible orientations, including NNW-SSE, NW-SE, WNW-ESE, NE-SW and ENE-WSW trending fractures. The building fluid pressure surpassed the normal stresses acting on the fracture wall, and hence, fluid burped into the weak planes leading to fluid-induced reactivation of the fractures, promoting vein emplacement along them (Fig. 10c). However, the NNW-SSE trending veins show greater thickness and abundance with respect to other orientations (see Fig. 4d and 3e). We found that pole to these veins (NNW-SSE trending orientations) lie within the warm zones of the stereoplots obtained from the Fractend code (Github, 2017), indicating higher dilation tendencies (see Fig. 8a and 8b). In Fig. 8a and 8b, it is perceived that pole to these orientations form a cluster around the  $\sigma_3$  stress axis. Similarly, pole to the orientations trending NW-SE and NE-SW respectively, have higher slip tendencies, indicating shear reactivation along them (Fig. 8c and d). Most of the poles to the NNW-SSE trending orientations lie within the overlapping warm zones, indicating high potential to reactivate in both shear and dilation mode (high slip and dilation tendencies). These orientations are susceptible for dilation as well as shear reactivation, depending on the predominance of fluid pressure and availability of fluid for inducing dilation or shear reactivation. Availability of fluid significantly reduces the effective normal stress ( $\sigma_n' = \sigma_n - P_f$ ); where  $\sigma_n'$  and  $\sigma_n$  are the effective normal stress and normal stress respectively) acting on the fracture planes (see Fig. 10c and d). Under this condition, fluid burps into the fractures leading to a significant drop in the fluid pressure. This sudden drop in the fluid pressure reduces the solubility of fluid materials promoting deposition of vein followed by sealing of the pathways (Cox et al., 1991, 2001). Pathways thus remains sealed till the next cycle of fluid pressure build up, fracture reactivation and vein deposition. However, in between two such cycles of high fluid pressure, an intermediate low fluid pressure cycle persists, during which fluid pressure might not be substantially high to reactivate all the

pre-existing pathways. Thus, a high fluid pressure cycle is followed by a subsequent pulse of low fluid pressure causing selective reactivation of some of the pre-existing orientations. Hence, it is envisaged that, these cycles of high and low  $P_f$  conditions might have been repeated multiple times (n-times) until the fluid source was completely exhausted. In the present case, the low  $P_f$  condition is interpreted by  
470 discretely analyzing the cluster within the girdle distribution of pole to vein data in the lower hemisphere equal area projection. (see sect. 4.4). Such low  $P_f$  could not surpass the normal stresses of all the pre-existing pathways. And only the NNW-SSE oriented ones (related to the magnetic fabric of the metabasalts) having high dilation and slip tendencies were favorably oriented for reactivation and fluid flow. The above mechanism of *fault-valve action* is supported with field evidences showing occurrences  
475 of thick quartz veins enclosing angular chunks of metabasalt hosts with multiple sub-parallel fault planes (identified from the slickenside lineations), see Fig. 3d & 3e. This suggests that the process of fracturing, fracture reactivation through faulting and vein emplacement (*fault-valve action*) prevailed throughout the D3 deformation. Thus, the process of new fracture formation and reactivation were continuously persistent during the entire late D3 phase, with intermittent episodes of vein emplacement under both high  
480 and low  $P_f$  conditions.

## 7 Conclusions

In the present study, we commented on the vein emplacement mechanism of the Chitradurga greenstone belt (Dharwar craton, south India). We analysed the magnetic fabric data recorded from AMS analysis of  
485 the metabasalt that hosts the quartz veins. 3D Mohr circle and paleostress analysis have been used to



evaluate the vein emplacement vis-à-vis regional deformation. Following are the main findings and conclusions from the study:

1. The NW-SE oriented magnetic fabric recorded in the metabasalts (as evident from the AMS analysis) is a product of the D1/D2 regional deformation on account of NE-SW directed shortening. This fabric was also favourably oriented and therefore, suitable for fracture propagation in relation to the prevailing stress field.
2. D3 deformation manifested by NW-SE to E-W directed shortening was coeval with the sinistral movement along CSZ. It is concluded that during late D3 deformation all pre-existing fabrics and the ones constituting the riedel shear system were reactivated, with CSZ acting as a shear boundary.
3. The variably oriented fractures and faults i.e., the NNW-SSE, NW-SE, WNW-ESE, NE-SW and ENE-WSW oriented ones are identified as the P, Y, R, T, X and R' shear components of the riedel shear system. The NNW-SSE oriented shears (P, Y and R) are abundant owing to their favourable correspondence with the pre-existing AMS fabric.
4. Paleostress analysis using fault-slip data recorded from field studies reveals NNE-SSW directed extension, asserting reactivation under a WNW-ESE directed compression (related to D3 deformation).
5. Vein emplacement took place under both high and low  $P_f$  conditions. It is envisaged that multiple number of such alternating high and low  $P_f$  cycles prevailed in the process of fluid flow and vein emplacement in the region.

6. Vein emplacement took place along all possible orientations. Evidences of *fault-valve behaviour* and fluid induced fracture/fault reactivation have been recorded from field studies. However, the NNW-SSE trending orientations having higher values of slip and dilation tendencies, channelized fluid during both high and low  $P_f$  conditions, thereby attaining maximum vein thickness.

510 7. The process of fracture formation, reactivation and faulting prevailed under a far field compression related to late D3 deformation. However, intermittent episodes of fluid pressure build up led to fluid induced faulting, rupturing and vein emplacement in the region.

**Author contribution:** SB: conceptualization, methodology, data curation, formal analysis, writing.

515 TKM: supervision, conceptualization, methodology, data curation, funding acquisition, writing.

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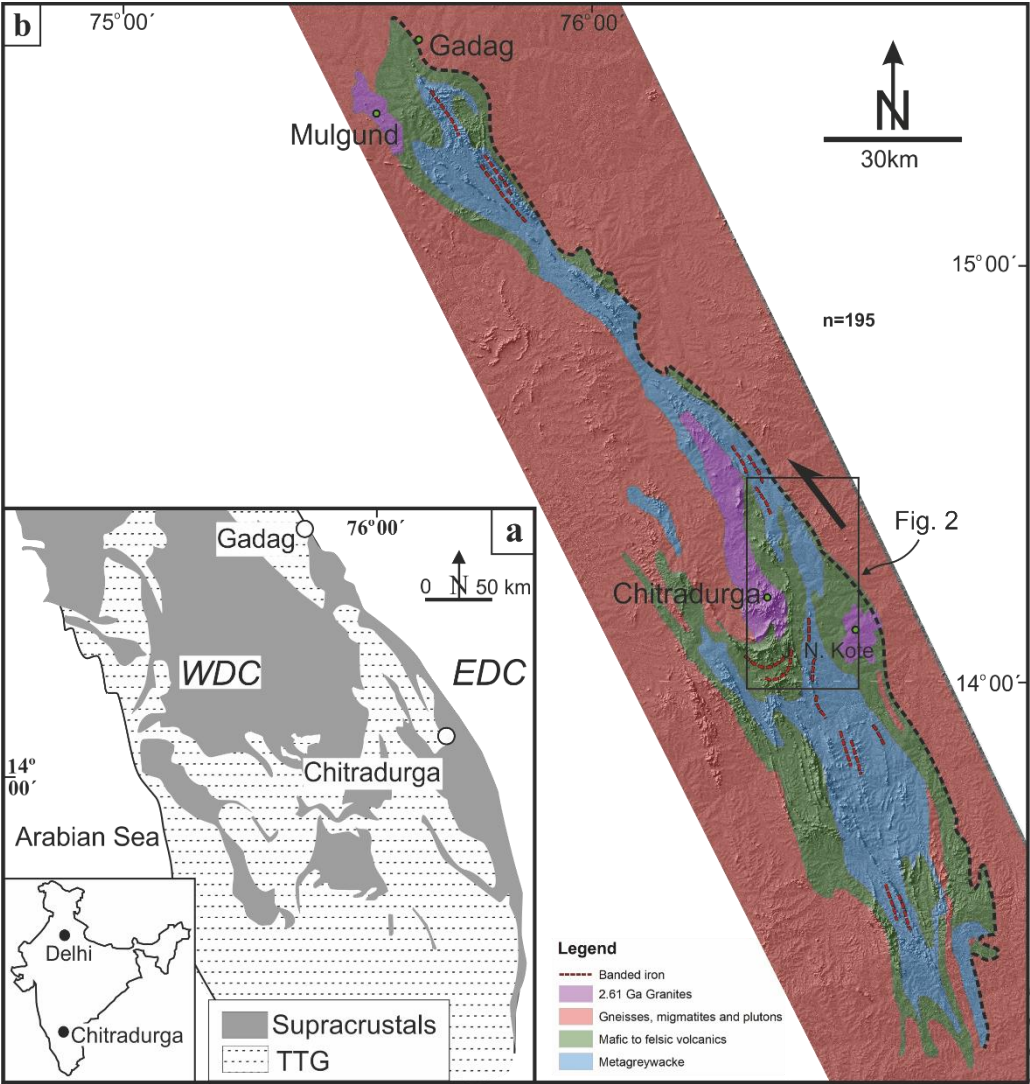
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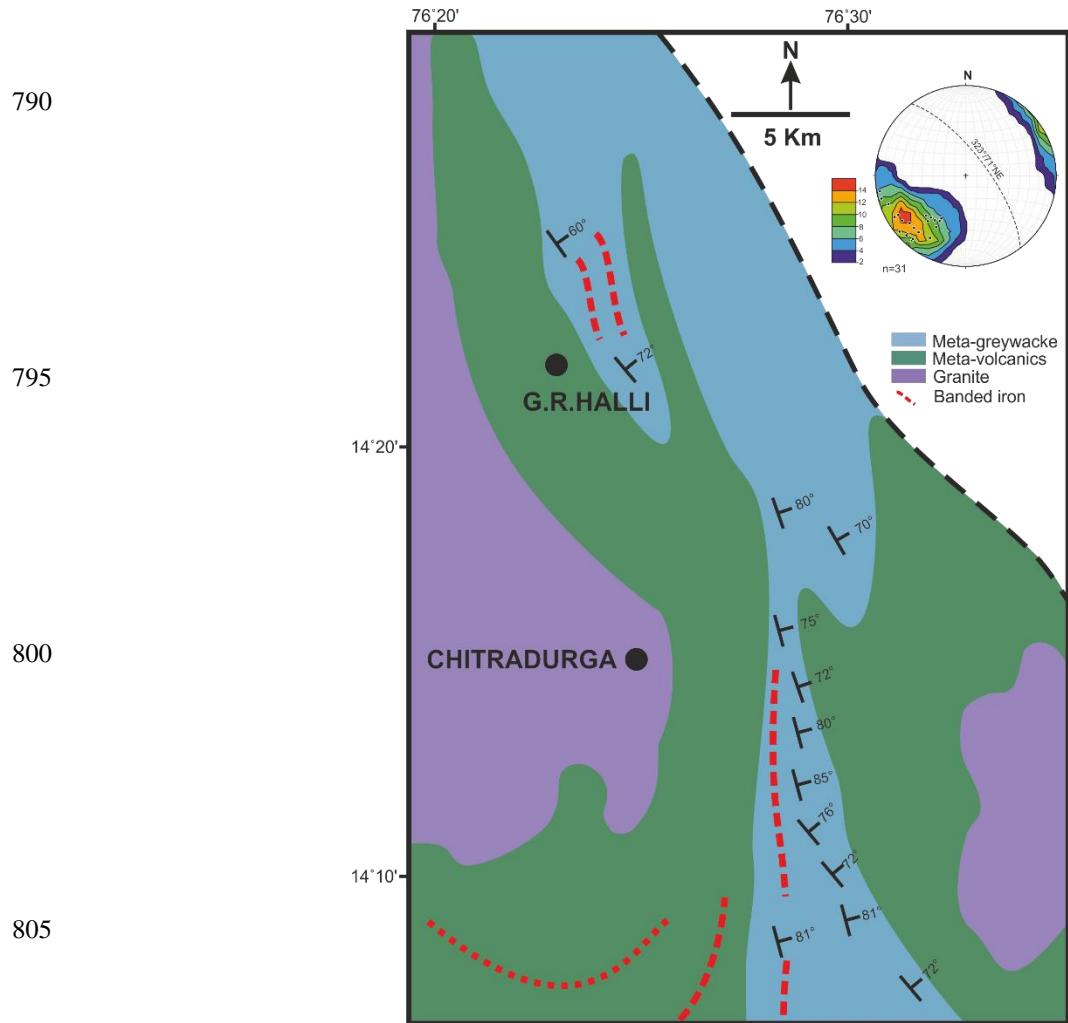
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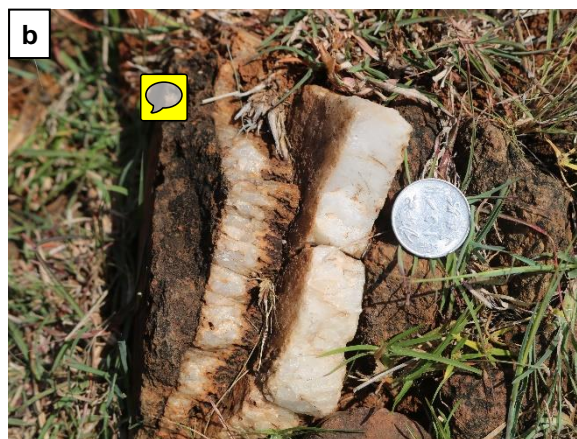
**Figure 01:** (a) Regional map of western Dharwar craton, South Indian Shield [after Chadwick et al., 2003]. Inset shows the map of India. EDC = Eastern Dharwar Craton; WDC = Western Dharwar Craton; (b) Regional geological map (DEM) of the Chitradurga Schist Belt [modified after Jayananda et al., 2013]. Dotted line (in b) marks the eastern boundary of the Chitradurga Schist Belt, representing the Chitradurga Shear Zone (CSZ). Rectangular box near Chitradurga demarcates the study area.



**Figure: 02:** Geological map of the study area showing the foliation trends of the supracrustals. Lower hemisphere equal area projection shows the pole to foliation planes recorded from the region. Note that the mean foliation (dotted great circle) is 323°/71°NE which is parallel to the CSZ (n= number data). Color scheme of the legend indicates variation in the contour density.



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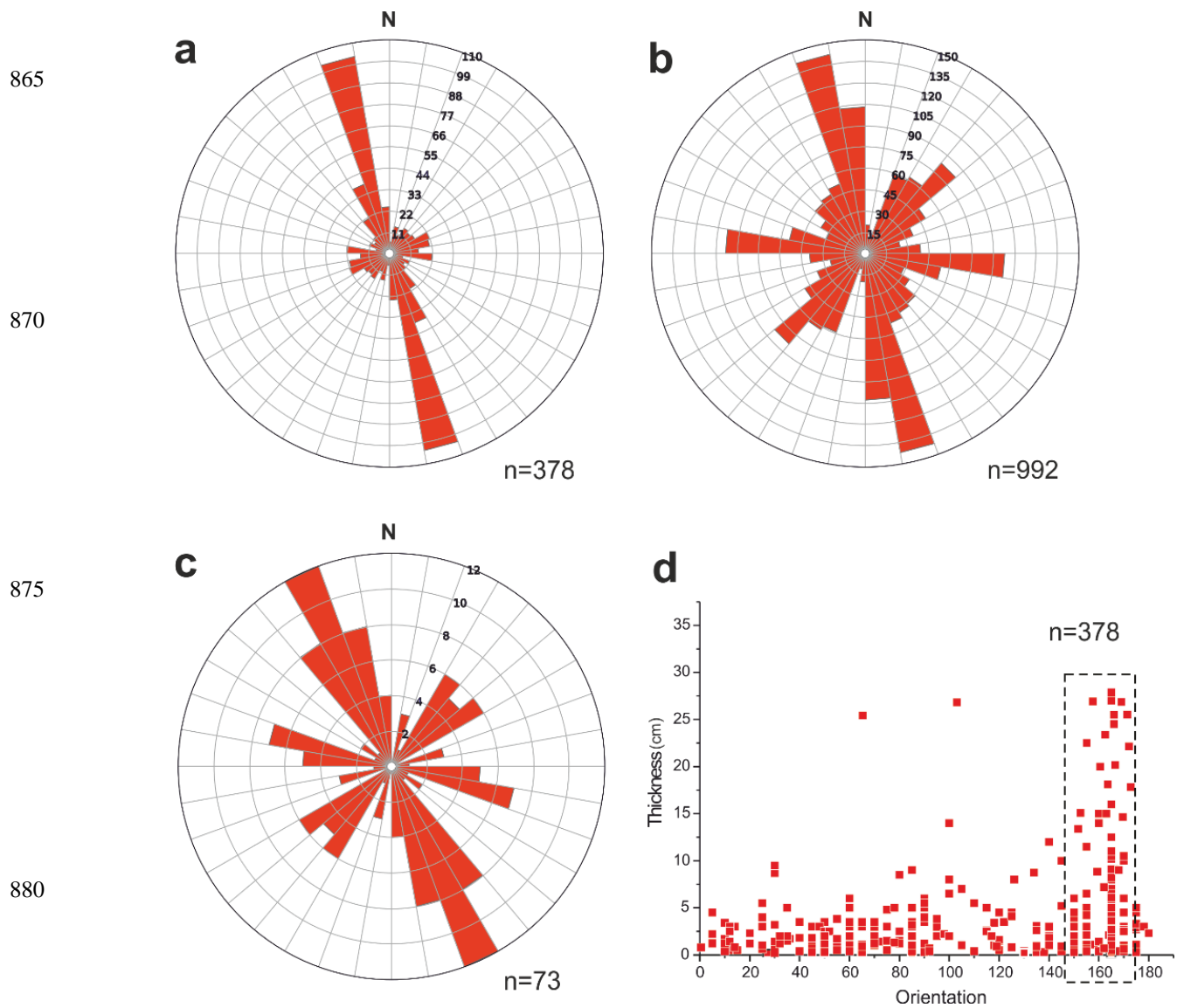
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**Figure 03.** Field photographs from the study area. (a) Criss-cross orientation of quartz veins in metabasalt (camera towards E). (b) Close-up of a quartz vein in metabasalt showing crystal growth direction perpendicular to the vein wall (camera towards NE). (c) Cross-cutting nature in quartz veins showing dextral displacement (marked by yellow half-arrows; camera towards N). (d) Wing cracks filled up with quartz veins associated with sinistral shearing (marked by yellow arrow; camera towards E). (e) NE dipping quartz vein showing slickenside lineations (maximum width recorded=120 cm), inset showing close up of the fault plane found in e. Marker pen placed along the orientation of the slickenside lineations. (f) Angular chunks of metabasalt (enclaves) enclosed within faulted quartz vein (camera towards NE). Dotted red line demarcates the enclave boundaries. Black arrow marks the slickenside lineation on the fault plane. (g) Fault planes in metabasalt showing congruous steps (marked by yellow arrow; camera towards E).

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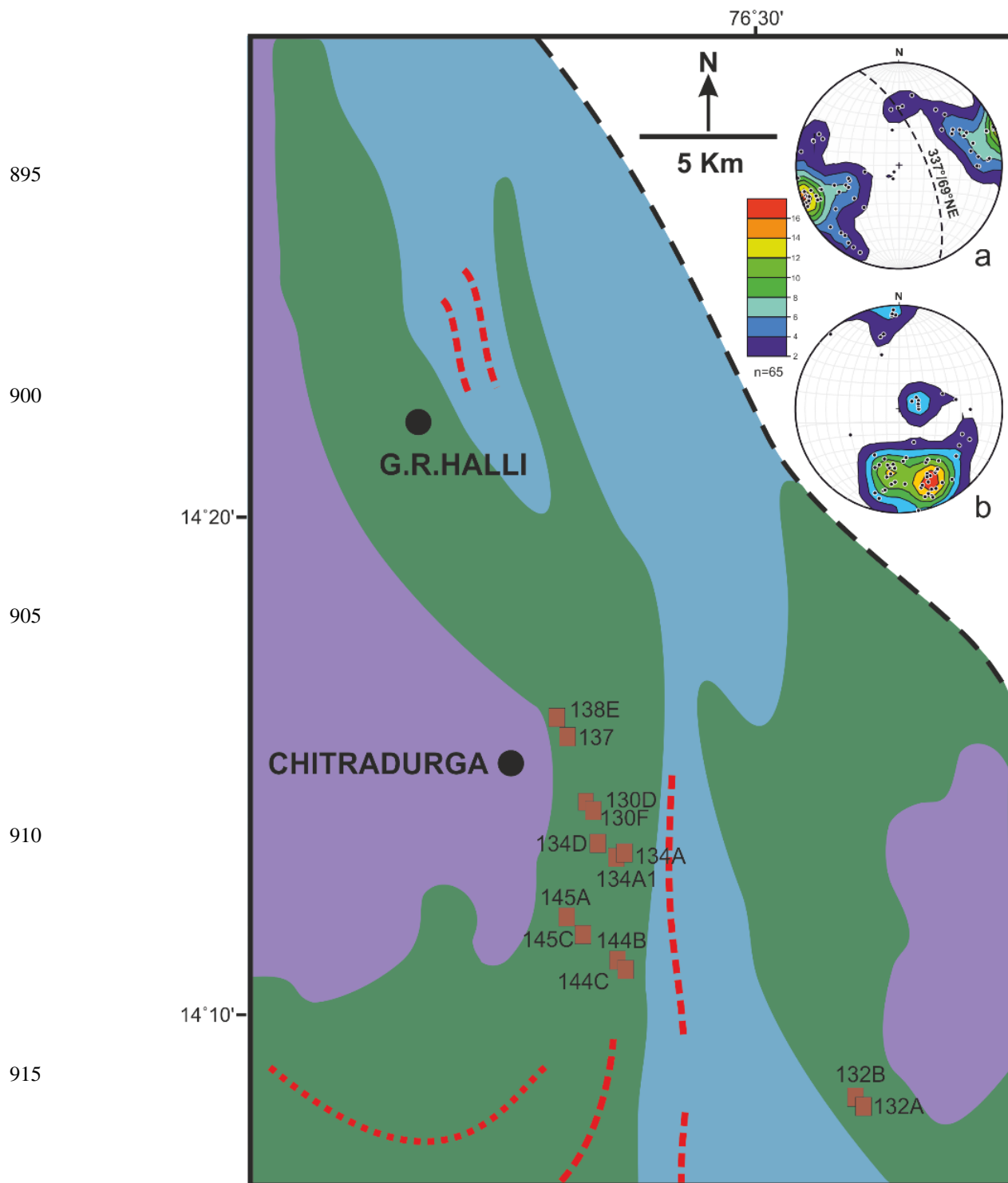
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**Figure 04.** Rose diagrams and graphs of structural data recorded from the study area. (a), (b) and (c) are the rose diagrams of the strike orientation of the quartz veins, fractures and fault planes respectively. Note that the veins are mostly NNW-SSE striking whereas the fractures and fault planes show variable orientations, with a NNW-SSE maxima and a WNW-ESE to NE-SW sub maxima. (d) Graph of vein orientation vs. thickness, showing maximum vein thickness along NNW-SSE (marked with orange box). n= number of data.





**Figure 05.** Map showing the location points (marked with brown boxes) from which oriented metabasalt samples for AMS analysis have been collected. (a) Lower hemisphere equal area projection of poles ( $K_3$ ) to magnetic foliation ( $K_1K_2$ ) plane. Mean orientation of  $K_1K_2$  plane (dashed great circle)=  $337^\circ/69^\circ E$  (b) Lower hemisphere equal area projection showing the distribution of magnetic lineation ( $K_1$ ). Color scheme of the legend indicates variation in the contour density.



**Figure 06.** Tensile strength determination of metabasalt samples. (a) Sample cores for Brazillian tensile strength (BTS) determination. Diameter: length=2:1. (b) Instruments used for measuring BTS. (c) Sample cores obtained after failure.

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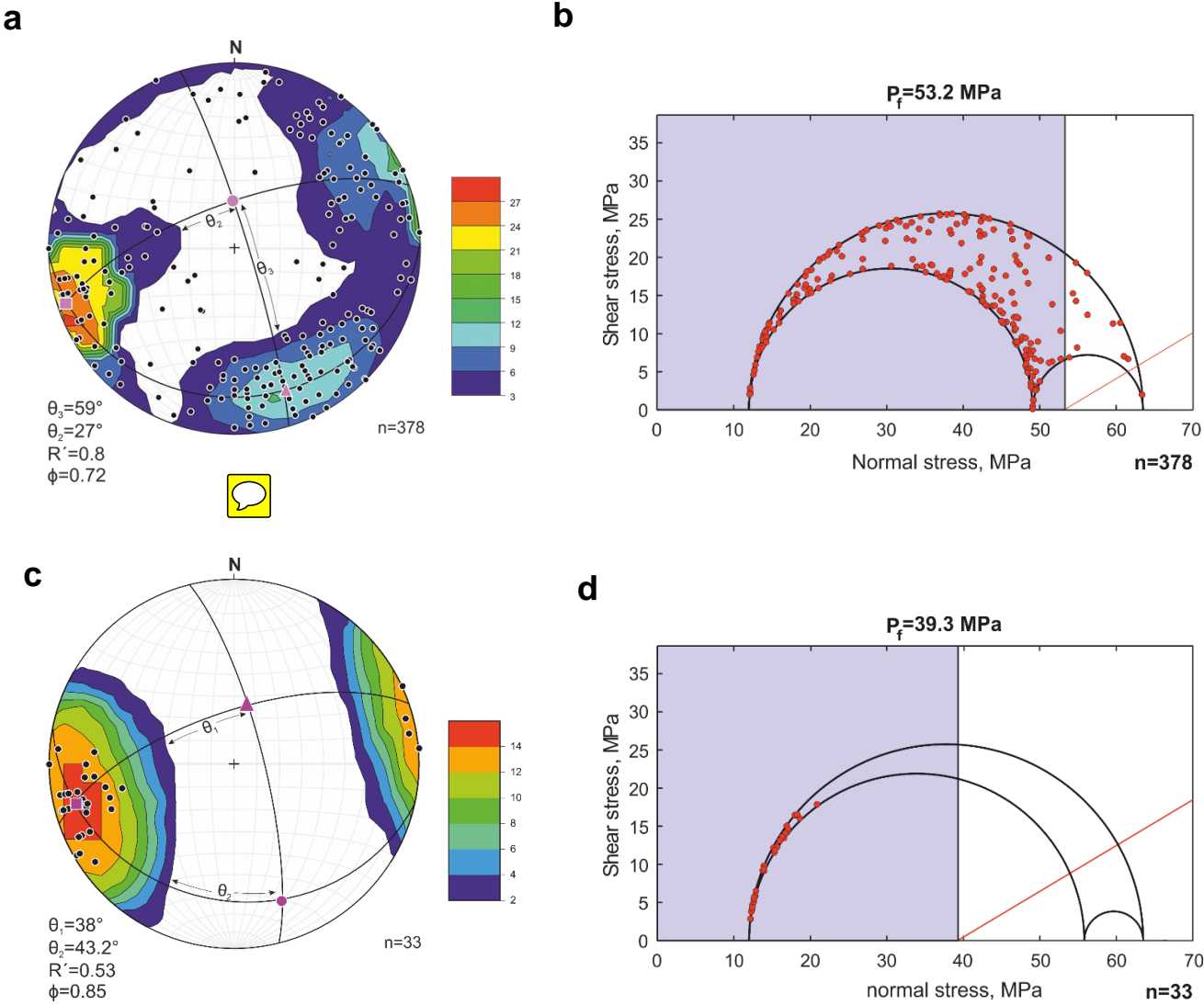
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**Figure 07.** The state of stresses and fluid pressure ( $P_f$ ) conditions determined from vein orientation data in the study area. (a) Lower hemisphere equal area projection of pole to veins shows girdle distribution, implying  $P_f > \sigma_2$  (following Jolly and Sanderson, 1997). The empty space devoid of any vein pole data helps to determine the position of  $\sigma_1$  (using Bingham statistics of the Stereonet 9 software) and thereby defines  $\sigma_1\sigma_2$  and  $\sigma_1\sigma_3$  planes. Angles  $\theta_2$  and  $\theta_3$  are measured which are used to determine the stress ratio ( $\phi$ ) and driving pressure ratio ( $R'$ ) respectively. Color scheme of the legends indicate variation in the

contour density. Pink circle ( $\sigma_1$ ), pink triangle ( $\sigma_2$ ) and pink square ( $\sigma_3$ ) respectively. (b) 3D Mohr circle diagram for high  $P_f$  conditions. Red line in the Mohr circle represents the reactivation envelope for cohesionless fractures. Vein pole data lying within the blue zone, i.e., to the left of the  $P_f$  (black) line represent fractures filled up with veins that are susceptible to reactivate (Fractend code available via Github, 2017). (c) Lower hemisphere equal area projection of poles to vein data forming the SW cluster in (a), this cluster distribution of vein pole data indicate  $P_f < \sigma_2$ . Cluster maxima defines  $\sigma_3$  axis. Angles  $\theta_1$  and  $\theta_2$  are measured and similarly  $\phi$  and  $R'$  are determined. (d) 3D Mohr circle diagram for low  $P_f$  condition. Only a limited range of fracture filled up with veins are susceptible to reactivate. Red dots represent pole to vein data, red line forms the reactivation envelope for cohesionless fractures.

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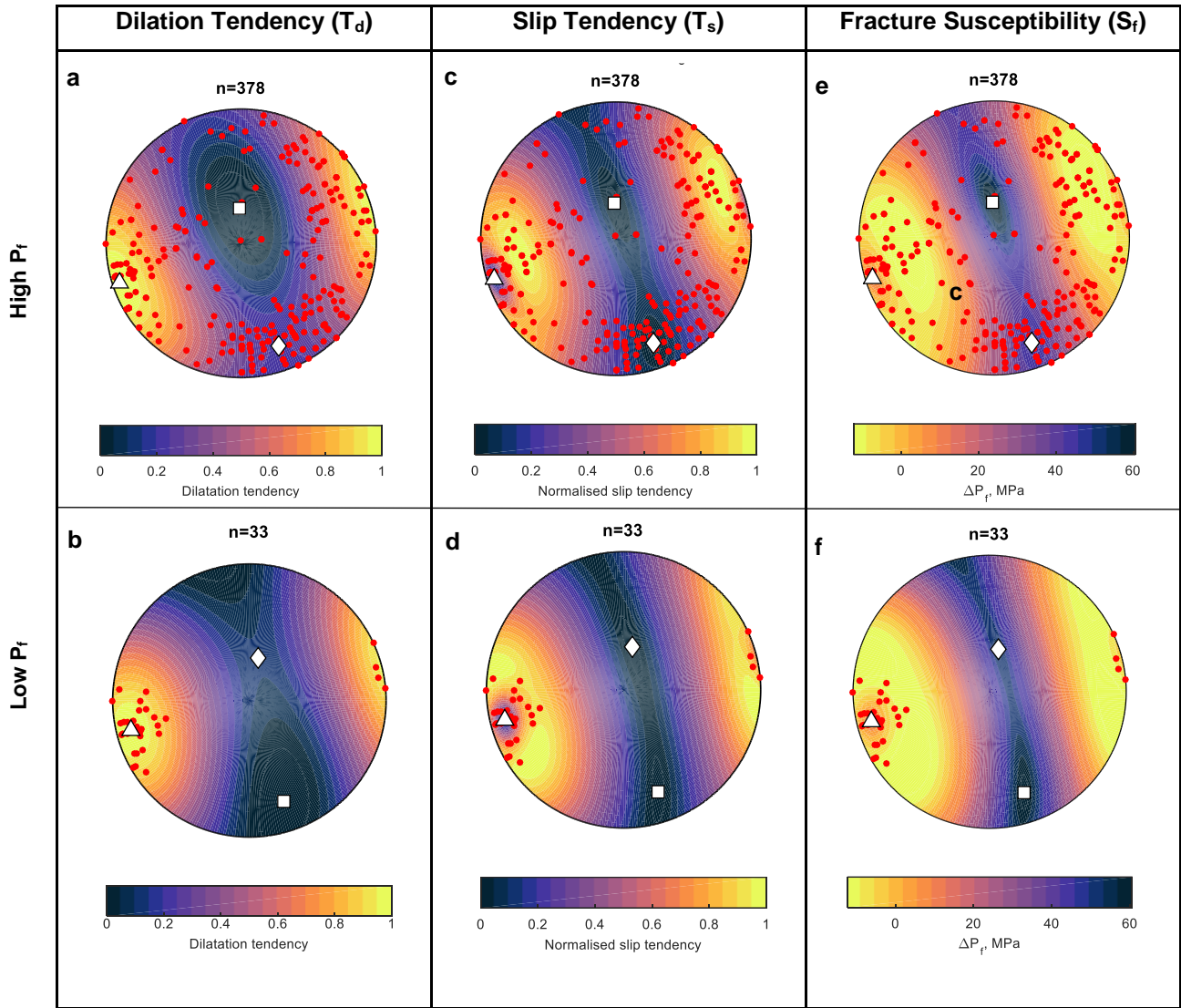
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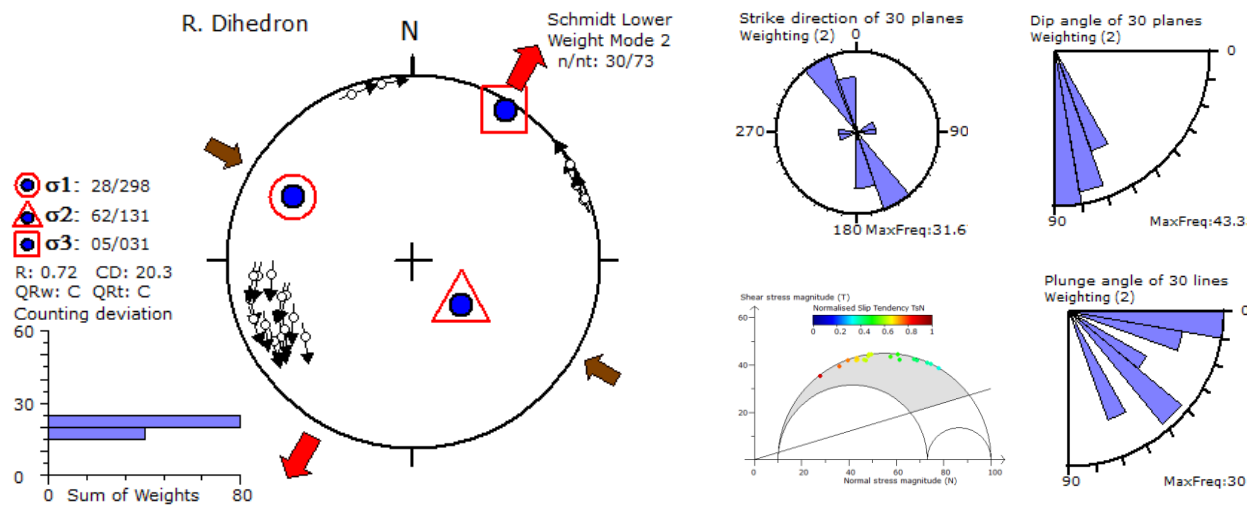
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**Figure 08.** Lower hemisphere equal area projection for dilation tendency, slip tendency and fracture susceptibility in a given fluid pressure condition and for a specific stress state (Fractend code available via Github, 2017). (a) and (b) represents dilation tendency for high and low  $P_f$ . (c) and (d) represents slip tendency for high and low  $P_f$ . (e) and (f) fracture susceptibility for high and low  $P_f$  conditions respectively. Warm color zones in (a) and (b), represents vein orientations with higher propensity for tensional opening. In (c) and (d) warm colors indicate vein attitudes that suffered shearing. In (e) and (f) the warm color

1040 zones stand for vein attitudes that are more susceptible to reactivate under low  $P_f$  variation. ‘Thermal’ color scheme from Thyng et al., 2016. White square ( $\sigma_1$ ), white diamond ( $\sigma_2$ ) and white triangle ( $\sigma_3$ ).

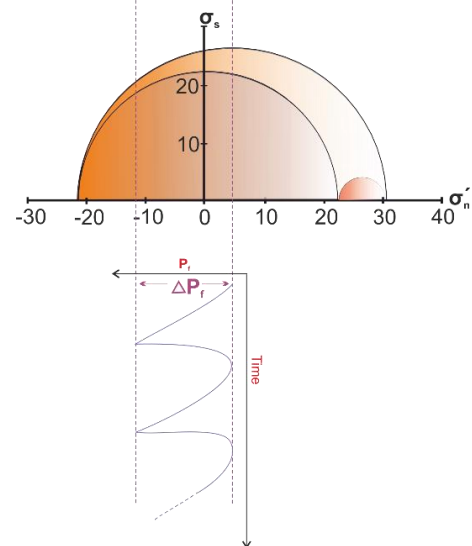
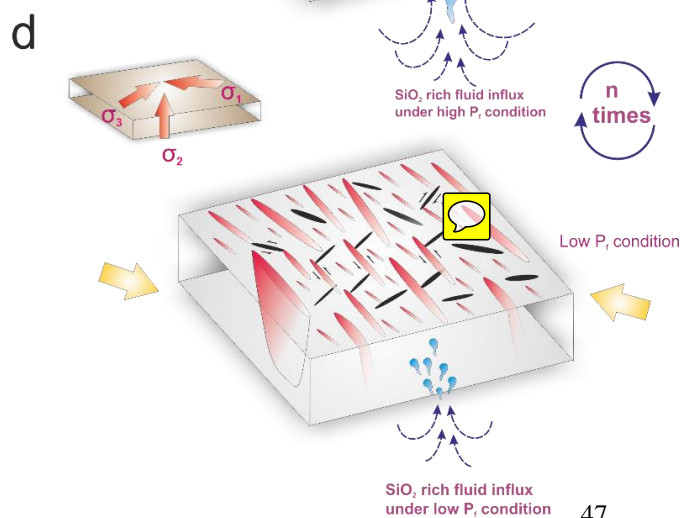
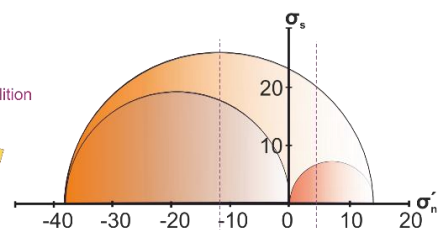
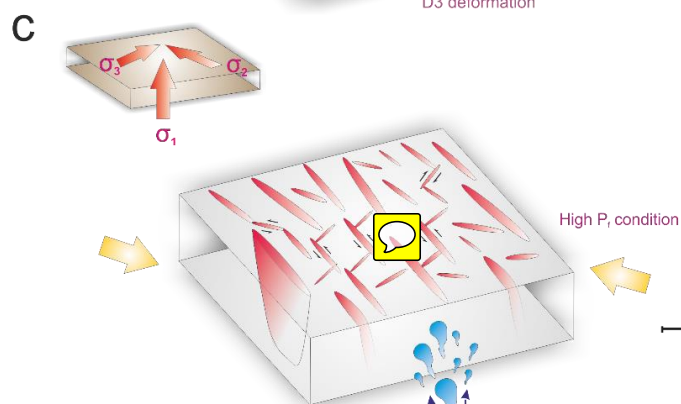
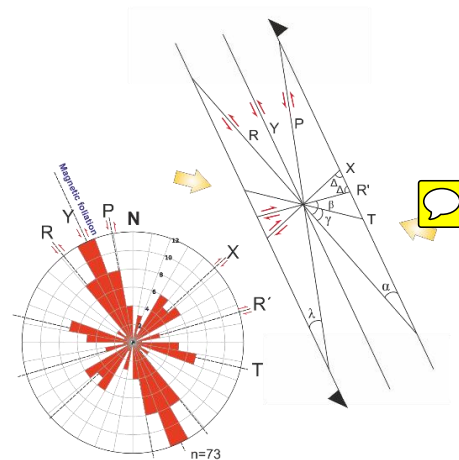
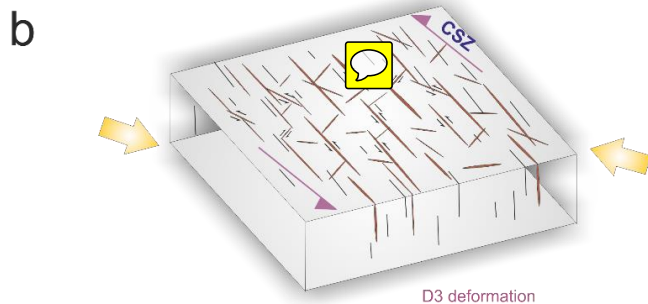
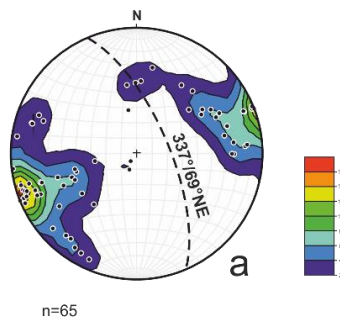
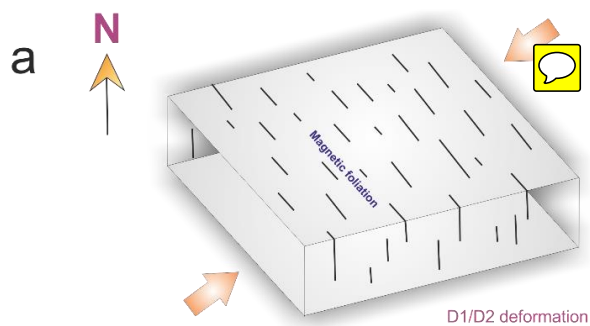
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1050 **Figure 09.** Paleostress analysis (using right dihedral method) of faults recorded in the metabasalts of the study area; for both left lateral and right lateral normal faults. Red arrow marks the extension direction ( $\sigma_3$ ) and pink arrow marks the principal compression direction. The histogram shows the minimum values for counting deviation.  $n$  and  $nt$  are the number of data accepted for tensor calculation and total number of data respectively.  $R$  (stress ratio) =  $(\sigma_2 - \sigma_3) / (\sigma_1 - \sigma_3)$ . Rose diagrams for fault plane strike, dip and plunge variations are also presented in the top right corner. 3D Mohr diagrams demonstrate possible areas of fault reactivation with variation in susceptibility, colored circles represent pole to the fault planes. The failure envelope for Mohr's circle is based on Byerlee (1978) initial friction angle of 16.7°. Note that the maximum extension is along NNE-SSW direction.

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**Figure 10** Schematic model showing formation and reactivation of fractures, along with vein  
1065 emplacement in the metabasalt host rock. (a) Development of the NNW-SSE to NW-SE oriented magnetic  
fabrics in the rock unit under a NE-SW shortening related to D1/D2 deformation. Lower hemisphere equal  
area projection shows mean orientation of the magnetic fabric  $\sim 337^\circ/69^\circ\text{NE}$ . (b) Formation of the Y, P,  
R, R', X and T shears related to the riedel shear system under a NW-SE to E-W shortening related to the  
1070 late D3 deformation (half arrows representing the shear zone boundary). The angles ( $\alpha$ ,  $\beta$ ,  $\gamma$ ,  $\lambda$  and  $\Delta$ )  
between the shear components are given after Logan et al. 1992.  $\Phi=30^\circ$  (angle of internal friction) is  
measured from UCS studies of the samples from the study area. Corresponding riedel shear model, with  
CSZ as the shear boundary and rose diagram showing orientations of the respective shear components.  
(c) and (d) showing vein emplacement under high  $P_f$  and low  $P_f$  conditions respectively (state of stresses  
along the fracture planes are given). Corresponding 3D-mohr circle diagrams quantifying the effective  
1075 normal stresses ( $\sigma_n' = \sigma_n - P_f$ ; in Mpa) under both high and low  $P_f$  conditions, difference in  $P_f$  ( $\Delta P_f \sim 13.9$   
MPa), obtained from the dashed lines representing the mean stress in each case. A conceptual graph shows  
multiple cycles (n-times) of high and low  $P_f$  conditions in the study area justifying *fault-valve action* that  
led to the emplacement of vein in the Chitradurga region.