Author's response

Reviewer#1 – Virginie Pinel

1. Main points

1) I enjoyed reading the introduction because the topic addressed is very important and this point is pretty well explained. But then I was somehow disappointed by the study itself. It is intended to evaluate the influence of geological data integrated into the modeling but only the stratigraphy and geometry of the plumbing system (see section 4) is considered. There is no real novelty in considering these aspects, which has been done in several studies (e.g. Cianetti et al, GJInt, 2012). I was expecting the authors to also take into consideration the existing faults after the long description of the structural/tectonic context of Colima volcano (fig1, section 2.1). In particular, the profile chosen for modeling cuts 2 faults of the Colima Rift, which are not considered in the models. Only a uniform extension applied at the lateral boundary is considered in some models. However, there are ways to consider a fault plane in 2D using a friction law (see Chaput et al, GRL 2014).

We thank the reviewer for the useful comments. The manuscript has been submitted for the special issue on the use of geological data for constraining numerical models. We focused our attention to geology (stratigraphic data, geometry of the feeding system) of the Colima Volcano area. However, we are aware the approach is not new, but it is new for Colima volcano. Moreover, it provides further insights on the limitations of FEM analysis when some geological features are unknown or not considered. The insertion of a constant extensive stress is not trivial, because it simulates the stress state that dominates the Colima rift over long times, affecting the computational domain. However, we agree that the fault movement (and the fault plane itself) may induce different perturbation in the stress state of the conduit feeding system area. However, although LISA cannot include a frictional law as in Chaput et al. (2014) and cannot provide the solution for two separated domains at the same time, in order to consider Reviewer#1's criticism, in the revised version we considered an approximate description of the effects of faults. In particular, since mature fault zones are generally made of complex highly deformed and low cohesive materials where most of the fault displacement is accommodated and surrounded by a fractured damage zone, in this revised version of the manuscript we have provided a new final configuration considering the faults of the Colima graben as "damage zones". Technically, we have selected two bands of elements by assigning more degraded elastic properties (as reported in Jeanne et al. 2017). Results with considering the fault are provided in the new Figure 7.

2) Model assumptions are not clearly described.

- It is in 2D but it is not explained whether a plane strain or a plane stress approximation is considered, which is a key information. Usually models are performed in plane strain, which means that there is a stress component out of plane.

We thank the Reviewer for such a point. Now we clearly stated that it is a plane strain in the text.

-The way the gravitational loading is applied remains unclear. When applying body forces lithostatic stress field should also be applied but when a topography is considered, some iterations are required to find the initial state of stress consistent with both the topography, the rheology and the body forces as described in Chaput et al, GRL, 2014 or Cianetti et al, GJInt, 2012. Also with a lithostatic stress field, the load applied at the reservoir boundaries has to be a superposition of the overpressure and the lithostatic component. It is not explained in the manuscript. Also if a lithostatic stress field is applied both the minimum and maximum stress field should increase with depth. From the figures shown in the result section it is not the case for the minimum stress sigma3 and I don't really understand why.

We described better this point in the text. The load applied to magma chambers is exactly the same requested by the reviewer (a superposition of the magmatic overpressure and the lithostatic component). Both σ_1 *and* σ_3 *increase with depth, as shown in Figure 4 where it can be seen* σ_3 *passes from zero to 110 MPa at depth.* σ_1 *passes from zero to ca 390 MPa. Probably, the reviewer was erroneously confused by the same colour scale applied to both Figures. In order to avoid confusion we clearly highlighted this point about colour scale in the revised text.*

3) Illustrations should be improved to help the understanding. In some cases, the dimensions of the numerical box represented are not clearly reported, titles are unclear. I will detail later on each figure. *Figures have been improved in this revised version.*

2. Minor points

1) Regarding the results and discussion of the Young modulus influence on the stress field, what matters are the ratios of the Young modulus considered in various layers and not the absolute value of the Young modulus in one given layer (I mean that if the Young modulus is mutliplied by 10 in each layer, no changes are expected except in the vicinity of the domain external boundaries). This fact is not clearly shown. Also I would recommend to cite the paper by Heap et al. published recently in the Journal of Volcanology and Geothermal Research (https://doi.org/10.1016/j.jvolgeores.2019.106684).

In the light of what reported in Heap et al. (2020) about the selection of the most appropriate Young's Modulus in modelling, we would like to point out that in our parametric study we aimed to show what influence has the choice of different values of Young's Modulus in each geological unit at changing different feeding system configurations (i.e. single chamber, double chambers not connected and connected with conduits). The results demonstrated that the changes are not only in the vicinity of the external boundaries as expected, but also (even small) around the shallow magma chamber and conduits.

2) Introduction: line 37, 41, before the chosen references list for numerical models I would put "e.g." because there are plenty of references that could be equally fairly cited here. Also I would add the reference to Cayol & Cornet, GRL, which is really a classical one. Line 57, I would suggest to also cite Albino et al., Geophysical journal international, 2010. *Added.*

3) Section 3.3 Line 213: it would be very helpful to show the mesh used. *Added in Figure 1 (panel c);* line 217, the boundary condition applied on the reservoir and dike walls should be explained. *We explained in the text.*

Line 229, the way gravity is expected to influence the failure condition is really depend on the rupture criterion considered (see for instance Albino, et al. JGR, 2018). *We specified this adding the suggested reference.*
Line 231, in Corbi et al, 2015, the trajectory of magma propagation is not influenced by gravity but by the deviatoric stress field induced by caldera unloading. *Thanks for such a comment. We corrected it in the text removing the reference.*

4) Section 4.2: Line 296 "During ascent to the surface, the dykes align themselves with the most energy-efficient orientation, which is roughly perpendicular to the least compressive principal stress axis σ3 (e.g. Gonnermann and Taisne, 2015; Rivalta et al., 2019)." this is true providing the magma driving pressure remains small compared to the deviatoric stress (see Pinel et al, JGR, 2017 and Maccaferri et al. G3, 2019). *We specified this in the text, also adding the suggested references.*

5) Section 5.1 Line 345, it would be important to show on a figure the reduced simulation domain selected for the sensibility analysis. Also for each unit, we would need to know the number of nodes considered (size of the vector space X). It is important because the larger variability of Unit B could be only due to the larger domain considered.
We added the number of nodes for each geological Unit, in Table 1 (beside the number of elements).

6) Figure 2: Figures labels and title should be improved, information of the number of nodes considered should be added. *We added the requested information in the captions.*

7) Figure 3: Figures labels and title should be improved, information of the number of node considered should be added. Limits of the different units should be shown. For panel A, it remains unclear to me which stress perturbation is considered as there is no reservoir.

We improved the labels of Figures 2-3 adding the requested information. We preferred to not indicate the limits of the different units because they would not be clear with this scale. For the panel (a) of Figure 3, the stress perturbation is only due to the lithostatic load.

8) Figure 5: The topography doesn't look the same on each panel, which makes comparison difficult. No indication is provided on the orientation of the maximum and minimum compressive stress. I don't understand the term "distensive". Once again I don't understand why sigma3 does not increase with depth.
Topography was corrected. The term "distensive" was changed into "extension". We do not understand to what refers the reviewer when talking about orientation of maximum and minimum compressive stress. We already replied earlier about the increase of σ_3 with depth.

Reviewer#2 – Adelina Geyer

<u>1) General points</u>

1) When citing previous published works use "e.g." because the lists are not exhaustive and the

cited articles are just a small example of the existing references. *We added "e.g." in the lists where citations are not exhaustive.*

2) The introduction is a bit confusing to me because the title (and objectives) of the manuscript are focused on stress field and the first paragraph of the introduction is about volcano deformation. I would recommend the authors to rethink the introduction pointing out the importance of calculating the stress field in volcanic areas, which are the components of the stress field (i.e. those processes affecting/modifying it, etc). Then, they can connect all this with the FEM as a "numerical tool" to quantify/predict the stress field in a volcanic area.

We agree to point out the issue of calculating the stress field in the volcanic areas within the introduction. We added this part in the Introduction.

3) The objectives of the work are presented in two different parts of the introduction (L68-74 and 83-86). I suggest merging them at the end of the introduction. *We merged the sentences at the end of the Introduction.*

4) To better evaluate the influence of the diverse geological details on the results obtained, it would be more appropriate to carry out first a parametric study on the studied parameters (e.g., Young's modulus, Poisson ratio, magma chamber geometry). Keeping all parameters constant and changing one parameter at a time in a systematic way, is what really allows estimating (and quantifying) the influence of the individual parameters on the numerical results obtained (see, for example, Kinvig et al. 2009; Geyer & Gottsmann 2010). Once the parametric study has been done, results obtained can be applied to the case studies.

The parametric study was carried out on Young's modulus but may be easily carried out for Poisson's ratio. In any case, the investigation of different parameters (i.e. rock mechanics and magma chamber geometry) would result in increasing the length of the paper, which is instead focused on influence of geological data (i.e. stratigraphy of the domain, feeding system geometry, effect of the rifting) on FEM simulations. However, we cited the papers mentioned by the reviewer in order to highlight the importance of the rock mechanics parameters.

5) The authors should be sure that all names mentioned in the text are included in the figures. For example, Figure 1 showing the geological setting of the CVC does not show the location of the Michoacan Block, the Chapala-Tula rift, etc.

We changed the citation in the text considering what reported in Norini et al. (2010-Figure 1) in which all mentioned geological structures are represented.

6) It would really help to include a sketch of the CVC plumbing system. *We added it in the new version of Figure 1 (panel d).*

7) The authors should show the mesh and also provide details about the size of the elements, not only the number. *We included the mesh used in our modelling in Fig. 1 – panel (c), and we provided more information in the text about the mesh elements of each geological unit.*

8) The authors should better describe how gravity is implemented and how is the resultant stress

field derived from it considering the selected mechanical properties of the computational domain. Also, since there is topography, I do not understand what the authors mean with "Gravity in the host rock (z <= 0)". Is gravity not assigned for z values > 0? This part should be clearly explained because the "background stress field" generated by the gravitational loading may have a strong influence on the results obtained.

We provided a better explanation in the text. We also removed "(z <= 0)".

9) Considering the size and depth of the deep magma chamber, I think that the domain boundaries are far too close to the area of study, specially to the W. This is also acknowledged by the authors (L382-389). Considering that the models are 2D (i.e. computational time is not too high compared to 3D models), it would have been safer to expand the limits of the computational domain further away from the magma reservoirs. The "displacement = 0 m" boundary condition has strong effects on the results obtained if the boundary is too close to the pressure source.

We showed the boundary effect in Figure 4. It is evident how the area comprising the feeding system (visible in Figs. 5-6-7) is not affected by any false result. To enlarge the domain would result in degrading of the details of the FEM simulation, which are already biased by the huge area at present considered for simulations.

10) L49-51: I do not understand this sentence. What do the authors mean by "boundary representation"? Please, be sure that you are not confusing the Boundary Element Method (BEM) with the Finite Element Method (FEM).

We revised the paragraph in the text in order to not be confusing. In particular, beside FEM, we aimed to describe another common way to describe the geological units by using BEM.

11) L55-58: I would mention also the use of FEM for fluid dynamics or thermal problems to illustrate their application to solve other type of physical equations, not only those related to rock mechanics (e.g., Bea 2010; Gutiérrez & Parada 2010; Gelman et al. 2013; Douglas et al. 2016). *Done.*

12) L59-60: Use "e.g." *Done.*

13) L60-62: Add references and indicate in GPa what is meant by "stiff" and "low". *Done.*

14) L67-69: Include some references to illustrate what kind of publications already exist. *Done.*

15) L74: I think something is missing in this sentence.

16) L81-83: Please, revise this sentence. I think that something is not correct in the English, a native English speaker should verify it. *Corrected in the text.*

17) L87-92: What overpressure? This sentence is confusing. All this paragraph should come much earlier in the introduction, when presenting the problematic the authors want to solve. If the idea is to highlight the limitations of the elastic approach used in the models, this section should be move to the "Methodology" section. *We specified: "estimate of magmatic overpressure".*

18) L95: The CVC acronym has been already explained. L112: Where is all this information shown in Figure 1? L130: "a.s.l."L186-188: What do the authors mean with "complex" structure? L193: Extension or extent?

Corrections made in the text. We changed the citation from Figure 1 to Norini et al. 2010 – Fig 1). For "complex structure" we referred to the dual magma chamber system.

19) L198: Indicate the website and what INEGI means. *Done.*

20) L215: Which geological units? The magma chamber? The rock layers? This sentence is confusing. *We referred to the extent of the rock layers, described in the following text and detailed in Table 2.*

21) L222-224: Since the authors have already extensively described it in the previous section maybe they should refer to their own text (and figure) here.

In the previous section (3.3 Modelling approach) we referred to Spica et al. 2017 but other parameters used in our modeling are described in other papers (i.e., Massaro et al. 2018, 2019) therefore we think it is useful add here these citations. We also added the reference to Figure 1d.

22) L224-227: Not sure which is the objective of this sentence, as the authors do not explain the overpressure assigned to their models in this paragraph. Is something missing? *No, in this sentence we only reported a general statement.*

23) L228: Commas are missing after between and with, otherwise the sentence is difficult to understand. *Done.*

24) L258: Please, add references. L260-261: Please, add references. Figures: Figure 1: Indicate the north arrow in (a). *Done for references. Figure 1: the North is on the top, left-side corner.*

25) Figure 4: The color different between Unit VD and GF is practically undistinguishable. It seems that the top-left image has a different orientation than the others. The selected color scale is strongly conditioned by the boundary effects at the right and left corners at the free surface. The authors should recalibrate the color scale so that the gravity stress field is visible also at shallower depths. Now is all in green.

We changed the colour of Unit GF. About the colour scales, they were set in a way they represent all the four panels, in order to facilitate comparison. We are aware of the similarity of green colors, and for this we separated the different colours with dashed line to indicate changes in the stress value.

26) Figure 5: It is really confusing to have to color scales for (a) and (b). It is difficult to compare the results between both models and the effect of the shallow reservoir. Has model b the gravitational loading implemented? It is strange to me to see that model provides negative sigma 1 values at such depths (i.e. 15 km).

The different colour scales were used, in this case, just for avoiding the problem highlighted in the *previous point by the reviewer. To have a common scale would result in too large stress classes (with the same colour) that would prevent the readability of each example. Both models have the gravitational loading implemented. You have to bear in mind that changing geological conditions results in changes in while stress in the simulation, which prevents the use of a common colour scale in LISA. The moderate negative σ_1 values are due to the effects of magma chamber overpressure with respect to the lithostatic load.*

27) Figure 6: I strongly recommend using another color scale, similar to the one in Figure 5 going from red to blue colors. In the sigma 1 picture many details are lost because of it.

It is not possible to freely set the colour scale in LISA. The alternative colour scales provided by LISA are grey-scale and red-blue but they do not provide a better visualization than this shown in Figures (rainbow colour scale). Unfortunately, the details of σ_1 are lost also in this case.

28) Figure 7: Same comment as in Figure 5. Is in the model in the middle gravity implemented? To facilitate the comparison among all pictures, the same color scale for all sigma 1 and for all sigma 3 should be assigned. Otherwise is very confusing because the same colors are sometimes <0 and other times >0.

Also in this case the gravitational loading has been implemented. As already stated before, the addition of different geological details changes the stress distribution and its value. For this, it is not possible to use the same colour scale for all the simulations, otherwise we would have very broad, poorly informative scale of stress values.

On behalf of the authors
Sincerely,

Silvia Massaro

Analysing stress field conditions of the Colima Volcanic Complex (Mexico) by integrating FEM simulations and geological data

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Abstract

In the last decades numerical methods have become very popular tools in volcanological studies, since capable of considering many relevant parameters in their calculations, such as the presence of multiple reservoirs, topography, and heterogeneous distribution of host rock mechanical properties. Although the widespread availability of geodetic data is keep growing, the influence of geological data on the numerical simulations is still poorly considered. In this work a 2D Finite Element Modelling is provided by using the LInear Static Analysis (LISA) software, in order to investigate the stress field conditions occurring around the Colima Volcanic Complex (CVC, Mexico) at increasing the details of geological and geophysical input data. By integrating the published geophysical, volcanological, and petrological data, we provide a first-order description of the domain of the CVC feeding system, considering either one or two magma chambers connected to the surface via dykes or isolated (not connected) in the elastic host rocks. We test the methodology by using a gravitational modelling with different geometrical configurations and constraints (i.e. magma chamber dimensions, depth, overpressure). Our results suggest that an appropriate set of geological data is of pivotal importance for improving the mesh generation procedures and the degree of accuracy of numerical outputs, aimed to more reliable physics-based representations of the natural systems.

1 Introduction

Magmatism and tectonism in volcanic active areas are strongly related to the regional and local stress fields, affecting both the orientation of faults and the location of volcanic vents, two fundamental aspects when interpreting volcanic unrest and forecasting volcanic eruptions (Geyer et al., 2016). The stress field around a magmatic source originates from three main contributions: (1) the background stress, composed of a vertical gravitational load and a lateral horizontal load corresponding to lithostatic confinement and tectonic regimes; (2) the stress field caused by the loading of the volcano edifice; and (3) the stress field generated by the magmatic overpressure in the chamber system (e.g. Martí and Geyer, 2009; Currenti and Williams et al., 2014). In recent years, a large number of semi-analytical and numerical solutions for the stress field state of geological and volcanological systems have been proposed (e.g. Cayol and Cornet, 1998; Simms and Garven, 2004; Manconi et al., 2007; Long and Grosfils, 2009; Currenti et al., 2010; Currenti and Williams et al., 2014; Zehner et al., 2015), taking into account the static elastic deformation in a multi-layered half-space (e.g. Dieterich and Decker, 1975; Bonafede et al., 2002; Wang et al., 2003; Gudmundsson and Brenner, 2004; Zhao et al., 2004; Pritchard and Simons, 2004; Gottsmann et al., 2006; Geyer and Gottsmann, 2010; Zhong et al., 2019). Following the successful application in mechanical engineering, the use of Finite Element Method (FEM) has been extensively introduced in Earth Sciences in order to investigate the effects of topography, lithologic heterogeneities, tectonic stresses and the gravity field on the Earth's surface deformation (e.g. Cailleau et al., 2003; 2005; Buchmann and Conolly 2007; Manconi et al., 2009; Masterlak et al., 2012), including volcanoes (e.g. Fujita et al., 2013; Carcho and Gàlan del Sastre, 2014; Bunney, 2014; Ronchin et al., 2015; Hickey et al., 2015; Cabaniss et al., 2019; Rivalta et al., 2019).

The use of FEM in volcanic areas has several examples, which vary from the influence of layered materials on the surface deformation process during volcanic inflation (e.g. Darwin volcano, Galapagos Islands; Manconi et al., 2007; Albino et al., 2010) to processes affecting chamber rupture (e.g. Grosfils, 2007; Long and Grosfils, 2009). FEM is also used in fluid dynamics and thermodynamics (e.g., Gutiérrez and Parada, 2010; Gelman et al., 2013) for solving issues related to motion of fluids and heat transfer.

The local stress around a volcanic feeding system strongly depends on the magma chamber geometry and on the mechanical properties of the layered host rock around it (e.g. Martì and Geyer, 2009), mainly due to broad changes in Young's modulus (e.g. Gudmundsson et al., 2011; Jeanne et al., 2017; Heap et al., 2020). For instance, limestones, lava flows, welded pyroclastic units and intrusive rocks can be very stiff (high Young's modulus; from ca. 1.7 to 27 GPa for limestones, Touloukian, 1981; ca. 5.4 GPa for volcanic rocks, Heap et al., 2020), whereas young and non-welded pyroclastic units may be very soft (low Young's modulus; ca. 1.7 – 3.1 GPa, Margottini et al., 2013). Consequently, the local stress may change abruptly from one layer to another (e.g., Gudmundsson, 2006). Irrespective of the scope of the numerical investigation, the importance of applying accurate rheological constraints to FEM modelling was discussed in many studies (e.g., Folch et al., 2000; Newman et al., 2001; Fernandez et al., 2001; Currenti et al., 2010; Geshi et al., 2012). This implies that geology of the volcanic area needs to be considered as more accurate as possible. However, few investigations have been carried out to assess the influence of the amount and quality of geological data into FEM computations (Kinvig et al., 2009; Norini et al., 2010, 2019; Cianetti et al., 2012; Ronchin et al., 2013; Chaput et al., 2014). To bridge this gap, in this work we use the Linear Static Analysis (LISA) software (version 8.0; www.lisafea.com) to study the subsurface stress behaviour in an elastic domain at Colima Volcanic Complex (CVC, Mexico) when improving the description of geological constraints.

The CVC area is a good candidate for testing the response of FEM software to different geological conditions, being constituted by a large volcanic complex (significant topographic load; Lungarini et al., 2005), a well-defined feeding system inferred from geophysical and petrological data (e.g. Spica et al., 2017; Massaro et al. 2018, 2019), and growth within a tectonic graben (bordered by normal faults; Fig. 1a) infilled by volcaniclastic material (variability of rock mechanical characteristics; Norini et al., 2010, 2019).

In this light, the present study proposes a contribution to a more proper use of FEM models for assessing the stress state pattern in volcanic areas at different levels of description of the geological features. In particular, we focus on the CVC by using the available published data of the inferred feeding system structure, in order to assess how the addition of geological and volcanological constraints (i.e. stratigraphy, geometry of the plumbing system, extensional tectonic regime, local fault systems) may, and at what extent, affect the model outputs (Fig 1b). Beside and beyond the evaluation of geological details on FEM outputs, we also obtained a picture of the large-scale stress distribution in the CVC subsurface.

2 The Colima Volcanic Complex (Mexico)

2.1 Geological framework

The Pleistocene-Holocene CVC is one of the most prominent volcanic edifices within the Trans-Mexican Volcanic Belt (TMVB) (Macías et al., 2006; Capra et al., 2016; Norini et al., 2019; Fig. 1a). In this area, the Rivera microplate and the Cocos plate subduct beneath the North America plate along the Middle American Trench, producing great deformation and fragmentation of the continental plate (Stock and Lee, 1994), and forming a triple junction that delimits the tectonic units known as the Jalisco Block (JB) and the Michoacán Block (MB) (Luhr et al., 1985; Allan, 1986; Rosas-Elguera et al., 1996; Rosas-Elguera et al., 1997; Ferrari and Rosas- Elguera, 1999; Rosas-Elguera et al., 2003; Frey et al., 2007). The three rifts of this system are the Tepic-Zacoalco (TZR), the Chapala-Tula (CTR), and the Colima Rift (CR) where the CVC is emplaced (Allan, 1986; Escudero and Bandy, 2017). The still active NS trending Colima Rift (CR) was formed during an extensional phase occurred after the Late Cretaceous–Paleogene compressive and transpressive phase (Allan, 1986; Serpa et al., 1992; Bandy et al., 1995; Cortés et al., 2010). The rifting phase deformed Cretaceous marine limestones, Jurassic–Tertiary metamorphosed clastic and volcaniclastic sediments, Cretaceous–Tertiary intrusive rocks and Tertiary-Quaternary volcanic deposits along sub-vertical crustal faults. While opening, CR was gradually filled with Pliocene–Quaternary lacustrine sediments, alluvium and colluvium (e.g. Allan, 1986; Allan et al., 1991; Norini et al., 2010). The geometry, kinematics and dynamics of the CR have been studied on the basis of field, seismic, and geodetic data, mainly collected in its northern and central sectors (see Fig. 1 in Norini et al., 2010).

The amount of vertical displacement of the northern and central sectors is estimated to be at least 2.5 km by adding the topographic relief of the bounding fault scarps (1.5–1.6 km) to the calculated sediment depth (Allan, 1985; Serpa et al., 1992). Field data and focal mechanism solutions are consistent with a direction of opening of the northern and central sectors oriented from E-W to NW-SE, with a mainly normal and minor right-lateral displacements of the bounding faults (Barrier et al., 1990; Suárez et al., 1994; Rosas-Elguera et al., 1996; Garduño-Monroy et al., 1998; Norini et al., 2010, 2019). In contrast to field and seismic evidence of long-term slightly dextral oblique extension, recent GPS geodetic measurements suggest a possible sinistral oblique extension of the CR (Selvans et al., 2011). In both cases, the stress regime is mainly extensional, with an approximately E-W orientation of the minimum horizontal stress in the basement of the CVC (Barrier et al., 1990; Suárez et al., 1994; Rosas-Elguera et al., 1996; Selvans et al., 2011; Norini et al., 2010, 2019).

The CVC stands within the central sector of the CR, on top of the Cretaceous limestones, Late Miocene-Pleistocene volcanic rocks, and Pliocene-Holocene lacustrine sediments, alluvium, and colluvium (Allan, 1985, 1986, 1991; Cortès, 2005; Norini et al., 2010). The volcanic complex is affected and displaced by the N-S/NNE-SSW-trending recent-active crustal faults of the CR, controlling the geometry and location of the volcano feeding system (Fig. 1a). Indeed, the CVC was formed by three andesitic stratovolcanoes aligned parallel to the CR bounding faults: the northern inactive Cantaro volcano (2900 m a.s.l.), following by the inactive Nevado de Colima (4255 m a.s.l.) and, in the southern part, the youngest and active Volcán de Colima (3763 m a.s.l.) (Norini et al., 2019 and reference therein).

2.2 Eruptive activity

The eruptive history of the CVC started in the northeast area with the formation of Cantaro volcano at ca. 1-1.5 Ma. The volcanic activity of the Nevado de Colima started at ca. 0.53 Ma. It is composed of voluminous andesitic lava domes and flows and pyroclastic deposits associated with caldera forming eruptions and numerous partial sector collapses (Robin et al., 1987; Roverato et al., 2011; Roverato and Capra, 2013; Cortès et al., 2019). The youngest Volcán de Colima, now considered one of the most active volcanoes of the world, consists of the Paleofuego edifice that suffered several sector collapses, with the formation of a horseshoe-shaped depression where the new active cone (also known Volcán de Fuego) grew up, through Merapi and Soufrière type dome collapses, extrusion of lava flows, Vulcanian and occasionally sub-Plinian explosive eruptions (Saucedo et al., 2010; Massaro et al., 2018, 2019). The activity of both Nevado and Volcán de Colima volcanoes also included several sector collapses, occurred frequently in the Upper Pleistocene and Holocene, repeatedly devastating the floor of the Colima Rift down to the Pacific Ocean (Robin et al., 1987; Luhr and Prestegaard, 1988; Stoopes and Sheridan, 1992; Capra and Macias, 2002; Cortès, 2005; Roverato et al., 2011).

2.3 The CVC plumbing system

Spica et al. (2017) indicate a 15 km-deep low velocity body (LVB) as the CVC deep magma reservoir. Its horizontal extension seems to be delimited by the borders of the CR, suggesting a structural control of the normal fault system on it (Spica et al., 2014). The LVB has an extent of ca. 55 km × 30 km in the N-S and E-W directions respectively, showing a mean thickness < 8 km. Escudero and Bandy (2017) obtained a higher resolution tomographic image of the subsurface in the CVC area, showing that the most active magma generation zone is presently under the Fuego de Colima edifice. Here, the ambient seismic noise tomographic study proposed by Spica et al. (2014) confirmed the presence of a shallow magma chamber above ca. 7 km depth, as also demonstrated by petrological studies (Medina-Martinez et al., 1996; Luhr, 2002; Zobin et al., 2002; López-Loera et al., 2011; Reubi et al., 2013, 2019; Macìas et al., 2017). Cabrera-Gutiérrez and Espíndola (2010) suggested the shallow active magma storage has a volume of ca. 30 km^3. The shallow magma chamber is connected to the surface by a dyke/conduit system, whose path is facilitated by the presence of the CR fault zone, which provides a natural pathway for fluids (e.g., Allan, 1986; Norini et al., 2010, 2019). The arrangement of dykes and the alignment of volcanic centres of CVC suggest that the dykes swarm draining the magma chambers developed along the NNE-SSW-trending, steep, eastward dipping normal fault exposed on the northern CVC flank (Norini et al., 2010, 2019).

Taking into account the previous information, Massaro et al. (2018) provided a first-order geometrical reconstruction of the Fuego de Colima feeding system during the 1913 sub-Plinian eruption, by using volcanological data (Saucedo et al., 2010, 2011; Bonasia et al., 2011) as input and constraints for numerical simulations. Results showed good matches for a hybrid configuration of the shallow conduit-feeding system (i.e., dyke developing into a shallower cylindrical conduit). The best-fit dyke geometry has width in the range from 200 m to 2000 m and thickness of ca. 40 m, with the cylindrical conduit diameter similar to the dyke thickness. The shallow magma chamber top was set at 6 km of depth, and dyke-cylinder transition at 500 m below the summit, as also inferred from geophysical data (Salzer et al., 2014; Aràmbula et al., 2018).

3 Methods

In this study, we used the commercial 8.0 version of LISA software (www.lisafea.com). LISA is a general-purpose Finite Element Analysis (FEA) software developed in the '90s based on the formulations proposed by Rao (1989). Since then, formulations from many other sources were also integrated (Bathe, 1990; Michaeli, 1991; Schwarz, 1991; Babuska et al., 1995). Despite FEA was originally used for structural analysis (Rao, 1989; 2013), it is also able to successfully predict the stress-strain behaviour of rock masses accounting for elastic models, in particular the deformation and failure mechanisms even in layered rock masses (Gabrieli et al., 2015).

Simplifying techniques in structural FEA can give valuable insights into local stresses more rapidly and efficiently than a full 3D model. Here we considered a 2D model throughout a complex structure (i.e. dual magma chamber feeding system, rift system, rock layering, and faults), in order to investigate the stress behaviour induced in the host rocks in response to the increasing detail of geological data used to constrain the model.

3.1 Modelling approach

Taking into account the works of Norini et al. (2010, 2019), we simulated the stress field of the CVC plumbing system considering an E-W cross-section, which is parallel to the extension associated to the active Colima Rift (Norini et al., 2010), shown in Figure 1a-b (a-a').
Since the extent of the CVC magma chambers in the NNE-SSW direction is typically much longer than the dimensions of the E-W cross section (Spica et al., 2017), 2D solutions of either numerical or analytical models describing E-W elongated magma chambers in the crust can be reasonably adopted (Jaeger et al., 2009; Costa et al., 2011). A topographic profile and 2D plane along the chosen E-W cross-section of the CVC area was obtained in ESRI ArcGIS from a Digital Elevation Model (DEM; resolution 50 m; Instituto Nacional de Estadística y Geografía - INEGI https://en.www.inegi.org.mx/). This cross section was imported into Autodesk Auto-Cad R13 and approximated to a third-degree spline. Finally, the IGES file was imported into LISA, where the mesh discretization was performed. The domain was discretized by three and four-node finite elements (Table 1; Fig. 1c). The volcanic

area domain extends 60 km horizontally and 30 km below the surface set in an *x-z* Cartesian Coordinate System. Zero normal displacements are assigned at the bottom and the lateral boundaries of the domain, while the upper boundary representing the ground surface is stress free (Fig. 1c). The analysis is carried out by using a plane strain approximation, implying that the deformation in the third direction is assumed to be negligible.

FEM of geological structures requires accurate discretization of the computational domain such that geological units are represented correctly. Zehner et al. (2015) reported that the unstructured tetrahedral meshes on a complex geological model has to fulfil the following requirements: i) sufficient mesh quality: the tetrahedrons should not be too acute-angled, since numerical instabilities can occur, ii) incorporation of geometry for defining boundary conditions and constraints, iii) local adaption, which is a refinement of the mesh in the vicinity of physical sources in order to avoid numerical errors during the simulation. Considering these requirements, in this work we adopt as the best discretization a mesh with 4660 plane continuum elements for the E-W cross-section. The size of finite elements was refined in the regions with higher gradients, especially near the contours of the magmatic feeding systems.

In our simulations, the extent of the rock layers (Table 2) is referred to the model of Norini et al. (2010, 2019). Magma chambers and dykes are considered as pressurized finite-size bodies in an elastic crustal segment, acting as fluid-filled holes. The boundary condition (pressurization) is provided by applying internal forces that act on the walls. This approach has been extensively used in several analytical and numerical models that treat magma reservoirs as internally pressurized ellipsoidal cavities within an elastic half space, in order to gain insight into the behaviour of magma plumbing systems (Pinel and Jaupart, 2004; Gudmundsson, 2006; Grosfils, 2007; Andrew and Gudmundsson, 2008; Hautmann et al., 2013; Currenti and Williams, 2014; Zhong et al., 2019).

The geometrical configuration set for the CVC feeding system (i.e. the shape and dimensions of the magmatic chambers) derives from the literature (Spica et al., 2014, 2017; Massaro et al., 2018, 2019) and it is simplified in Figure 1d. The overpressure in magma chambers may be produced by a variety of processes, including fractional crystallization, volatile exsolution and magma recharge, leading to deviatoric stresses in the country rock that may be tens of MPa in magnitude (Jellinek and DePaolo, 2003; Karlstrom et al., 2010).

Previously published studies indicate that differences between, and problems with, elastic models derive principally from the key role played by gravity (e.g. Albino et al., 2018). Gravity plays a first order role on bedrock failure conditions (Gerbault, 2012), on the geometry of magma propagation with respect to an edifice load and on buoyancy contrasts driving magma upward (Lister and Kerr, 1991; Watanabe et al., 2002). However, in a wide variety of simulations of natural phenomena the gravitational effects are often incorporated either incorrectly or incompletely (e.g. Grosfils, 2007). Some authors argued on whether it is appropriate or not to account for the gravity body force in numerical models of volcanic inflation (e.g. Currenti and Williams, 2014; Grosfils et al., 2015). When the gravitational loading is not included in the model, the volcanic deformation results from a change with respect to a stage previously at equilibrium (e.g. Gerbault et al. 2018). In this work, we carried out simulations considering the effect of the gravitational loading. Gravity in the host rock is implemented via body forces. The model initial condition has a pre-assigned lithostatic stress, whose computation, in presence of topography and material heterogeneities, is not trivial because it requires applying the gravity load preserving the original not deformed geometry of the mesh (Cianetti et al., 2012). Since the presence of a lithostatic stress field, the load applied at the reservoir boundaries represents a superposition of the magmatic overpressure and lithostatic component.

We also took into account the effect of the existing faults of the Colima Graben (CG) system even if LISA cannot include a frictional law to represent the fault movement (i.e. Chaput et al., 2014). As reported in Jeanne et al. (2017 and reference therein) the damage induced by faults increases from the host rocks to the fault core implying the reduction in the effective elastic moduli represented by a progressive decrease in Young's Modulus. Considering the evaluation of fault zone elastic properties provided by Jeanne et al. (2017), we represented the faults bordering the CG as two damage zones inclined of ca. 70° and with a thickness of ca. 1 km, showing reduced elastic properties with respect to the surrounding host rocks down to 10 km in depth.

It is important to note that we chose to represent the different simulations using different colour scales. Although such a choice makes more difficult a visual comparison of the simulation outputs and it needs to be kept in mind looking at the different figures, it preserves the necessary details of stress distribution, which would have been lost using a common colour scale for all the figures in LISA.

4 Geological data

In this work, we used geological information available in literature as input data, in order to estimate the stress variations around the CVC magmatic plumbing system. Here we briefly describe the main geological features taken into account in LISA simulations.

4.1 Stratigraphy

Four units forming the CVC system were defined from the available geological data (Table 2): i) Basement (Unit B): cretaceous limestones and intrusive rocks forming the bed-rock underlying the CVC; ii) Graben fill deposits (Unit GF): Quaternary alluvial, colluvial, and lacustrine deposits filling the graben; iii) Fuego de Colima deposits (Unit FC): andesitic lavas and pyroclastic deposits forming the Paleofuego-Fuego de Colima edifices; and iv) Volcaniclastic deposits (Unit VD): volcaniclastic deposits covering the southern flank of the CVC (e.g. Cortés et al. 2010; Norini et al., 2010, 2019). Being the area interested by FEM extended down to 30 km, it is evident how Unit B is dominant with respect to the others, which occupy only few km in the upper part of the simulated domain. We assumed constant mechanical characteristics within each Unit (Table 2). In particular, Unit B was considered mechanically homogeneous with elastic properties of a carbonate, due to the lack more detailed information of deeper lithologies (Norini et al., 2019).

Deformation within the brittle upper crust is described by elastic material behaviour. For each Unit we fixed typical rock mass properties, density (ρ), Young's Modulus (E) and Poisson's Ratio (ν) (Table 2). The rock masses are considered dry, in order (eventual) pore pressure to be neglected. Only for Unit GF a higher value for the Poisson's Ratio was used close to the surface in order to mimic high water content in the graben sediments. The maximum thickness of the graben fill (about 1 km) was assumed from the literature (Allan, 1985; Serpa et al., 1992; Norini et al., 2010, 2019). For Units B and GF rock mass proprieties were derived from Hoek and Brown (1997) and Marinos and Hoek (2000), while for volcanic materials (units FC and VD; Table 2) were estimated according to the approach proposed by Del Potro and Hürlimann (2008). This information allowed Norini et al. (2019) to derive the equivalent Mohr-Coulomb properties for the stress ranges expected in the different sectors of the CVC. In addition, in order to describe the effects of the CG faults on stress field distribution, the mechanical properties were locally degraded in proximity of the faults themselves.

4.2 The geometry of the plumbing system

The geometry of the E-W cross-section of the CVC plumbing system was modelled taking into account the previous subsurface information described in Section 4.1. In our 2D model, we assumed the CVC composed of a two magma chambers connected by dykes and to the surface by a conduit (Fig. 1d). The shape of the magma chambers and dykes are represented by elliptical cross-sections with the major (2*a*) and minor (2*b*) axes.

Generally, the magma chambers have a sill-like shape that is often imaged in seismic studies of volcanoes and rift zones (Macdonald, 1982; Sinton and Detrick, 1992; Mutter et al., 1995; MacLeod and Yaouancq, 2000; Singh et al., 2006; Canales et al., 2009). Most of them are not totally molten but rather a mixture of melt and crystal mush (i.e. Parfitt and Wilson, 2008). Various estimates have been made to infer the actual amount of melt in a magmatic body, showing that it is only ca. 10% of the total chamber volume (Gudmundsson et al., 2012 and reference therein).

Spica et al. (2017) described a 15 km-deep low velocity body (LVB) with its top at ca. 15 km of depth and with an estimated volume of ca. 7000 km^3, representing the deep magmatic reservoir of CVC. Assuming the melt as 10%, the deep magma chamber volume would be ca. 700 km^3. Simplifying this volume in an elliptical sill-like geometry, the dimensions (i.e. *2a, 2b, 2c* axes) have to be scaled according to those of LVB (55 × 30 × 8 km; Spica et al., 2017). We therefore fixed $2a$ = 14 km, $2b$ = 3.6 km, $2c$ = 26 km as the dimensions of the deep magma chamber, being $2c$ elongated in NW-SE direction.

For the shallow part of the feeding system, we have no detailed geophysical constraints. However, Massaro et al. (2019) reproduced through numerical modelling the nonlinear cyclic eruptive activity at Fuego de Colima in the last 20 years, using a shallow magma chamber volume in the range of 20-50 km^3, also according to the estimation of Cabrera-Gutiérrez and Espindola (2010). Assuming a volume of 30 km^3, we fixed $2a$ = 3.5 km, $2b$ =2 km, $2c$ = 8 km as dimensions of the shallow magma chamber.

Numerous theoretical and field studies have established that host rock stresses dictate the magma pathways (e.g. Maccaferri et al., 2011; Gudmundsson, 2011). During ascent to the surface, the dykes align themselves with the most energy-efficient orientation, which is roughly perpendicular to the least compressive principal stress axis σ_3 (e.g. Gonnermann and Taisne, 2015; Rivalta et al., 2019), providing the magma driving pressure remains small compared to the deviatoric stress (Pinel et al., 2017; Maccaferri et al., 2019). This behaviour, however, can be modulated in the presence of significant variations in fracture toughness of the surrounding rock due to stratification (Maccaferri et al., 2010) or to old and inactive fracture systems (Norini et al., 2019). Although for oblate magma chambers the propagation of dykes is most probable from the tip areas, in our simulations the orientation of dykes is assumed vertical, because of the preferential pathways represented by the CR fault planes (Spica et al., 2017).

Although, for decades, magma conduits were modelled as cylinders, because of easiness of their mathematical treatment, geophysical data and field observations highlight the importance and peculiarities of dykes in magma transport and hence the need to adopt more realistic geometries (Costa et al., 2009; Hautmann et al., 2013; Tibaldi, 2015). It is important to stress that although all cavities/inclusions in a medium modify the local stress field and concentrate stresses, the induced perturbation depends mainly on the geometry of the cavity/inclusion (Savin, 1961; Boresi et al., 1985; Tan, 1994; Saada, 2009). We set the dimensions of feeder dykes in agreement with Massaro et al. (2018): deep dyke $2a_d$ = 2 km; shallow dyke $2a$ varies from 1 km at bottom to 500 m in the upper part of the volcano; width of both deep and shallow dyke $2b_d$ = $2b$ = 100 m (Fig. 1d), although the exact value of the latter is not crucial for the purposes of this study. Moreover, it is worth noting that it is not the aim of this work to provide the conditions for the magma chamber rupture, being LISA accounting only for the elastic regime. For these reasons, the selected magma overpressures (ΔP) acting on the magma reservoirs and dykes have to be less than the tensile strength of the rocks. We therefore fixed ΔP at 10 MPa and 20 MPa for the 15 km-deep chamber, and 5 MPa for the 6 km-deep one. For the dykes and conduit, the magmatic overpressure is fixed at 10 MPa in the deeper dyke and 5 MPa in the shallower dyke, except for the upper 500 m of the shallower conduit where overpressure is set at 0.4 MPa.

To take into account the effect of both far field extensive regime and CG around the magma feeding system, we applied a uniform extension at the lateral boundaries of the domain (as reported in Martì and Geyer, 2009) of 5 MPa and included two damage zones with reduced rock elastic moduli and density (i.e. E = 1 GPa, ν = 0.20; Jeanne et al., 2017; ρ = 1850 kg/m^3).

5 Results

The first part of this section is focused on a sensitivity analysis of Young modulus variation, aimed to quantify the numerical effects of approximation of this important rock property on FEM outputs. The second part of this section describes the model outputs when adding complexity to the input geological/geophysical data.

Considering the E-W cross-section (a-a'; Fig. 1a), we provided six domain configurations with increasing geological complexity: i) "*homogeneous lithology model*" in which the volcanic domain is only composed of andesite rocks; ii) "*not homogeneous lithology model*" where different geological units are considered; iii) "*single magma chamber model*" composed of a not homogeneous lithology and a 15 km-deep magma chamber; iv) "*dual magma chamber model*" composed of a not homogeneous and 6 km- and 15 km-deep magma chambers; v) "*conduit feeding system model*" composed of not homogeneous lithology, 6 km- and 15 km-deep magma chambers connected through a deep-dyke, and a shallow conduit connecting to the surface; vi) "*extensional model*", in which we added a 5 MPa horizontal extensional stress (far field) and, vii) "*faulted model*", in which two damaged zones mimicking the CG faults were added to the "*extensional model*" (local stress) (Fig. 1b).

The number of nodes in the *only substratum* and *single magma chamber* models is set at 4426, for the dual magma chamber model is set at 4161, and at 3737 for the *conduit feeding system* and *faulted* models.

5.1 Sensitivity analysis on selected input parameters

In order to quantify the influence of Young Modulus selection on the model outputs, we performed a sensitivity test using the single magma chamber model as reference case. We evaluated the influence of varying the Young Modulus in each geological Units on the principal stresses σ_1 and σ_3. Taking into account the material properties used in the simulations (Norini et al., 2010, 2019; Table 2) as reference values, we compared the stress state of the computational domain at changing (±) Young Modulus by an order of magnitude. This variation has been separately applied to each Unit, in order to assess what is the effect of changing material properties on model outputs. This sensitivity analysis, although incomplete, may lead to raise awareness on the selection of input data when running a FEM. The sensitivity analysis was carried out on a reduced simulation domain (the *x*-axis was set to 35 km) in order to diminish the influence of binding effects that are present along domain borders.

We used the Euclidean norm (L2) method for illustrating the results of the sensitivity analysis. The L2 norm applied on a vector space *x* (having components *i = 1,...n*) is strongly related with the Euclidean distance from its origin, and is equal to:

$$||x||_2 = \sqrt{\sum_i^n xi^2} \quad (1)$$

In our case, the vector space *x* is composed of all nodes of the computational domain (Table 1). We defined x_{ref} the vector containing the results for the maximum and minimum principal stress when using the selected values of material properties (Table 1) and *x(-)*, *x(+)* the vectors at varying the Young Modulus of one order of magnitude in each Unit.

We evaluated the global variation of stress in the proposed geometrical configurations of the domain (i.e. not homogeneous lithology, single magma chamber, dual magma chamber, and dual magma chamber with conduits models) calculating the global relative variation in L2 as follow:

$$L_2(-) = \frac{||x_{ref} - x(-)||_2}{||x_{ref}||_2} \quad (2)$$

$$L_2(+) = \frac{||x_{ref} - x(+)||_2}{||x_{ref}||_2} \quad (3)$$

In Figure 2 are reported the global relative variations in L2 of the principal maximum stress σ_1 and principal minimum stress σ_3 caused by the variation of Young's Modulus in each Unit. All the geometric configurations show variability less than 15%, with few exceptions within Unit B that have variability over 30% (Fig. 2). It is worth noting that the spatial distribution of the major variations seems to not significantly affect the final stress distributions, because: i) they are located near the mesh borders (Fig. 3a, b); and, ii) when not at the mesh borders, the variations are limited to few % (Fig. 3c, d). It means that changing the Young's Modulus of one order of magnitude produces variation in FEM outputs distributed over a large domain and the change affecting the single nodes is limited to few %.

5.2 Homogeneous and not homogeneous lithology

We carried out LISA simulations considering the effect of the gravitational loading on the homogeneous and not homogeneous lithology on FEM outputs. In Figure 4 we reported a gravity loading model for E-W cross-section of the CVC system. We first considered the homogeneous rock composition composed by only andesitic lavas (Fig. 4a) and then by carbonates (Unit B), alluvional, volcaniclastic and pyroclastic deposits (Units GF and VD; Fig. 4b). We analysed the principal stresses σ_1 and σ_3 acting on the system, which correspond to the maximum and minimum stress at a point, respectively.

Figure 4 shows the patterns of the minimum principal stress σ_3 (panels i-ii) and of the maximum principal stress σ_1 (panels iii-vi), highlighting very slight differences between the homogeneous and not homogeneous lithology cases. It is very important to stress that the *x-z* zero displacement assigned at the bottom and the lateral boundaries of the domain created substantial artefacts in the results (i.e. curved patterns of stress). The artefacts are also evident when considering σ_3 (panels i-ii) where the boundary effect on *x*-axis is amplified by the presence of the upper free surface. For this reason, the only area to be considered as unperturbed is the central part of the entire domain, and it extends ca. 30 km horizontally and ca. 15 km vertically (within the blue contour in Fig. 4).

5.3 Gravitational modelling using the inferred feeding system geometry

We progressively add the elements of the conduit/feeding system of the CVC to FEM under the effect of the gravitational loading. Three cross-section profiles (Figs. 5, 6) show increasing complexity of the feeding system starting from a single magma chamber, passing to two magma chambers, then adding the conduits, and, finally, considering the effects of faults.

Figure 5a describes the distribution of the minimum principal stress σ_3 (panel i) and the maximum principal stress σ_1 (panel ii) at magma chamber overpressure of 10 MPa, showing how the insertion of the pressurized magma chamber modifies the lithostatic stress. No significant differences in magnitude and pattern of stresses are visible when having a magma chamber overpressure of 20 MPa (Appendix 1a).

The addition of the shallow magma chamber significantly changes the values and pattern of both σ_3 and σ_1 (Fig. 5b). In particular, σ_3 and σ_1 stresses describe a typical inflation pattern produced by overpressurised magma chamber(s) (Anderson, 1936; Gudmundsson, 2006), producing well-defined stress arches of σ_3 (red dotted lines in Figs. 5bi) and divergent strong gradients of σ_1, well developed around the larger magma chamber (Fig. 5bii). Stress arch is a common phenomenon occurring in continuous materials as response to applied pressure. It has been proved to have great influences on the self-stabilization of soils or rock masses (Huang and Zhang, 2012), and may influence mechanisms of caldera collapse (Holohan et al., 2015). Very slight differences in magnitude and pattern of stresses appear when using 10 MPa (Fig. 5b) or 20 MPa of deep magma chamber overpressure (Appendix 1b).

Figure 6 shows the effect of adding two conduits connecting the deep and shallow magma chambers. It is evident how the insertion of the conduits in the feeding system of CVC dramatically changes the stress distribution, with disappearance of the stress arch and an almost constant stress in the computational domain except than on the tips of the deep magma chamber.

5.4 Extensional field stress

In order to explore the influence of the extensional far field stress on stress patterns (Fig. 1a), we run simulations applying 5 MPa of extensional stress to the FEM domain, which is a typical low value for rift zones (Turcotte and Schubert, 2002; Moecck et al., 2009; Maccaferri et al., 2014; Sulpizio and Massaro, 2017; Fig. 7).

In the case of a single magma chamber (with 10 MPa overpressure; Fig. 7, panels i-ii), the addition of extensional far field stress reduces the confinement effect due to the no displacement condition imposed along the *x-z* directions (plane strain approximation). The effect of the extensional field stress on double magma chamber configuration (with 10 MPa overpressure in the deep chamber and 5 MPa in the shallower one) produces slight changes in stress magnitude and pattern for both σ_3 and σ_1 (Fig. 7, panels iii-iv) with respect to Figure 5b. The same applies also for the complete feeding system configuration, in which the attrition of the far field stress slightly changes the intensity of the stresses and patterns (Fig. 7, panels v-vi). Using 20 MPa overpressure in the deep magma chamber does not significantly affect the model outputs (Appendix 2).

5.5 Faults bordering the Colima Rift

In order to reproduce the effect of faults bordering the Colima Rift on the final feeding system configuration, we added two damage zones by degrading the elastic properties of a volume of rock mass.-The insertion of the two zones of weakness does not alter significantly the stress distribution observed in Figures 7v and 7vi, with only reduction of both σ_1 and σ_3 values in the surroundings of the damage zones (Figs. 7vii and 7viii). The different distance of the two damage zones to the feeding system (especially the deep magma chamber) produces a small asymmetry in both σ_1 and σ_3 patterns with respect to simulations without damage zones (Figs. 7v-viii).

6 Discussions

6.1 FEM analysis at increasing geological details

The presented FEM model of the CVC highlighted some important characteristics of crustal stress distribution at changing geological constraints used as input conditions (Spica et al., 2014, 2017; Massaro et al., 2018). Although the results have to be considered as a first order approximation, the changes in stress distribution are evident and useful for the understanding of limitations and advantages of FEM.

Under the assumptions of plane strain, gravitational loading, and overpressured magma chambers and dykes, the use of homogeneous or not homogeneous lithology for FEM provides negligible effects in stress intensity and pattern (Fig. 4). This is because the upper Units (Units FC, VD, GF; Table 2) represent only a limited part of the simulated domain, which in the remaining part results entirely composed of the assumed homogeneous basement (Unit B; Table 2). This does not mean that the influence of the upper Units may be still negligible using smaller scales of the simulated domain.

Analysing the FEM outputs with the single magma chamber, it emerges how the overpressures, ΔP, only limited the effects of gravitational loading. The use of a dual magma chamber geometry better describes the inflation induced by overpressure within magma chambers, with the formation of the stress arch in the minimum compressive stress σ_3 plot. It is important to highlight that for both single and dual magma chamber models, the change of internal overpressure from 10 to 20 MPa slightly changes the magnitude of the stress but not their general patterns (Appendix 1-2).

The presence of dykes in the magma feeding system dramatically change the σ_3 and σ_1 patterns (Fig. 6). Indeed, they become quite homogeneous throughout the computational domain, with the only exception of sidewall effects induced by the zero displacement conditions, already discussed in Figure 4.

The addition of extensional field stress of 5 MPa reduces the sidewall effects and produces an almost homogeneous stress distribution in the upper part of the computational domain, above the top of the deep magma chamber. This, along with the additional inclusion of the damage zones introduced to mimic the effects of CG faults, describes a close to equilibrium volcanic system, in which volcanic overpressure and lithostatic stress almost equilibrate each other (Sulpizio et al., 2016).

6.2 Some implication of the stress state of the CVC inferred from FEM

The results obtained with the insertion of the full feeding system and far field stress on the FEM highlight an almost homogeneous stress distribution in the CVC area. This means that the shape of the dual magma chamber feeding system model and far field stress provide a stable geometry, which limits the stress changes to few MPa. All the large stress variations are located at the tips of the magma chambers, as expected for pressurized or under-pressurized cavities in the lithosphere (Martì and Geyer, 2009). This means that the whole feeding system is in a quasi-equilibrium state, and, as an example, any overpressure created by input of new magma is adjusted by increasing the magma chamber volume or erupting at the surface. Even if we consider the scenario of complete emptying the upper conduit and part of the shallow magma chamber, as occasionally occurred during the past sub-Plinian and Plinian eruptions (Luhr et al., 2002; Saucedo et al., 2010; Massaro et al., 2018), this would result in the restoration of the stress arch, which is still a stable stress configuration. Even the complete emptying of the shallow magma chamber probably would be ineffective for triggering a large collapse (caldera forming) of the feeding system. This latter event would be possible only if a large depressurization of the deeper magma chamber would occur, but it implies the eruption of tens to hundreds of km^3 of magma, which seems not very likely provided the current stress distribution in CVC.

Beside and beyond the limitations due to the first order approximation of the FEM analysis, other sources of uncertainties in the discussion about present and future stress state of the CVC come from not considering gravity-driven processes, such as volcano spreading due to plastic deformation of the GF Unit (Norini et al., 2010, 2019) or pressurization of the shallower conduit (Massaro et al., 2018), and detailed regional tectonics (Norini et al., 2010, 2019). The effect of the two fault systems bordering the Colima Rift were simulated by degrading the mechanic properties of rocks in an area of about 1 km width up to a depth of 10 km. Although the effects are negligible at the scale of the computational domain, it cannot be excluded some local significant effects that cannot be resolved using the described approach.

7 Conclusions

The increasing details of geological and geophysical data to FEM simulation at Colima Volcanic Complex (Mexico) showed the importance of using the most accurate input data in order to have reliable outputs. In particular, the data here presented highlighted how the use of simplified models produces unreliable outputs of the stress state of the volcano subsurface.

Beside and beyond the results obtained by analysing the influence of detailing geological and geophysical data, the FEM of CVC confirms the close to equilibrium state of the volcano, which is the expected stress distribution induced by a feeding system directly connected to the surface.

This means that any overpressure created by input of new magma is adjusted within the feeding system, sometimes triggering eruptions. The complete emptying the upper conduit and part of the shallow magma chamber, as occasionally occurred in the past, originating sub-Plinian and Plinian eruptions, would result in the restoration of the stress arch, which is still a stable stress configuration. Descends that large magnitude, caldera forming eruptions are possible only if the bigger deep magma chamber is also involved and significantly emptied during an eruption.

Appendices

Appendix 1

E-W gravitational modelling of the CVC domain (stratified lithology) for all configurations investigated. The magnitude and pattern of the principal stress account for a) single magma chamber model (number of nodes: 4426); b) dual magma chamber model (number of nodes: 4161); c) dual magma chamber with conduits model (number of nodes: 3737). The dimension of the deep magma chamber: $2a$ = 14 km and $2b$ = 3.6 km at 15 km of depth; shallow magma chamber: $2a$ = 3.5 km and $2b$ = 2 km at 6 km. The magmatic overpressure is 20 MPa for the deep chamber, and 5 MPa for the shallower. Black dotted lines highlight the passage from different stress values. Note that the scale of stress values are different for each panel in order to maximise the simulation details.

Appendix 2

E-W gravitational modelling of the CVC domain (stratified lithology) considering a far extensional stress field of 5 MPa for all configurations investigated. The magnitude and pattern of the principal stress account for a) single magma chamber model model (number of nodes: 4426); b) dual magma chamber model (number of nodes: 4161); c) dual magma chamber with conduits model (number of elements: 3737). The dimension of the deep magma chamber: $2a$ = 14 km and $2b$ = 3.6 km at 15 km of depth; shallow magma chamber: $2a$ = 3.5 km and $2b$ = 2 km at 6 km. The magmatic overpressure is 20 MPa for the deep chamber, and 5 MPa for the shallower. Black dotted lines highlight the passage from different stress values. The red arrows indicate the direction of the applied far field stress. Note that the scale of stress values are different for each panel in order to maximise the simulation details.

Code/Data Avaiability

The LISA code is available at https://lisafea.com/.

Author's contribution

SM, RS, AC, GN and GG conceived the study. SM and RS wrote the bulk of the manuscript with the input of all the co-authors. SM and GL compiled the numerical simulations and formulated the adopted methodology. MP and SM carried out the sensitivity analysis. RS, AC, SM, GN, GG, LC, GL, MP and AG worked on the interpretation of the results.

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Table 1 - Element types used in LISA analysis considering the final conduit feeding system configuration – Fig.1d, panel vi)

E-W cross-section (a-a')		Element Type	Elements	Nodes
FC	Fuego de Colima	quad4-tri3	372	384
VD	Volcanic Deposits	quad4-tri3	245	273
GF	Graben Fill	quad4-tri3	456	338
B	Basament	quad4-tri3	3088	2907
CG	Colima graben	quad4-tri3	48	71

Total Elements: 4209

Table 2 - Rock mass and mechanical properties of the geological Units used in the finite-element model (from Norini et al., 2010, 2019).

Acronym	Model Unit	Rock Type	Density (kg/m^3)	Young's Modulus (MPa)	Poisson's ratio ν
FC	Fuego de Colima	Andesitic lavas and pyroclastic deposits forming the Paleofuego-Fuego de Colima	2242	1.4×10^3	0.30

		volcano			
VD	Volcaniclastic deposits	Pyroclastic and epiclastic deposits covering the southern flank of the CVC	1539	1.7×10^3	0.32
GF	Graben Fill	Quaternary alluvial, colluvial, lacustrine deposits filling the graben	1834	1.5×10^3	0.35
B	Basement	Cretaceous limestones and intrusive rocks forming the bed-rock underlying the CVC	2650	3.6×10^4	0.30

Figures Captions

Fig. 1 (a) Morphotectonic map of the Colima Volcanic Complex (NC=Nevado de Colima volcano; FC=Fuego de Colima volcano) and Colima Rift with the main tectonic and volcano-tectonic structures (NCG =Northen Colima Graben; CCG= Central Colima Graben, from Norini et al., 2019). In the inset, the location of the Colima Volcanic Complex (CVC) within the Trans-Mexican Volcanic Belt (TMVB) is shown in the frame of the subduction-type geodynamic setting of Central America (from Davìla et al., 2019); (b) general sketch of the geometrical configurations used in LISA; (c) example of mesh of the investigated area for the dual magma chamber model with conduits (case v in panel (b), considering zero-displacement along the bottom and left and right sides. Note that for case (vi) in panel (b) the zero-displacement is removed from the lateral sides; (d) sketch of the Fuego de Colima feeding system composed of a 15 km-deep magma chamber connected to surface via a 6 km-deep magma chamber and dykes. ΔP_{chs} and ΔP_{chd} are the magmatic overpressures in the shallow and deep chambers, respectively (modified from Massaro et al., 2019).

Fig. 2 Results of the sensitivity analysis carried out on the Young's Modulus variations within each rock layer of the domain considering different configurations (stratified substratum model – nodes: 4426; single magma chamber model – nodes: 4426; dual magma chamber model – nodes: 4161; dual magma chamber with conduits model – nodes: 3737). For each geological Unit (B, FC, GF, VD), the relative global variation in L_2 (%) is provided for σ_1 and σ_3. The x(-) and x(+) vectors indicate the Young's Modulus variation by an order of magnitude with respect to x_{ref} vector, containing the stress values calculated by using the values of material's properties indicated in Table 2.

Fig. 3 Spatial variation (%) of the L_2 norm's components at varying Young's Modulus for selected cases of Units B and VD: (a) Unit B in the stratified substratum model (nodes: 4426); (b) Unit B in the single magma chamber model (nodes: 4426); (c) Unit B in the dual magma chamber model (nodes: 4161); (d) Unit VD in the dual magma chamber with conduits model (nodes: 3737). Symbols *x*(-) and *x*(+) have the same meaning of Figure 2.

Fig. 4 E-W gravitational modelling of the CVC domain. The scale of the mesh is expressed in Unit of Design (1 UD = 1 km). The domain extends 60 km along the *x*-axis, and 30 km along the *z*-axis. The number of nodes used in the mesh is set to 4426. The magnitude and pattern of the principal stresses (dotted black lines) are reported for (a) the homogeneous stratigraphy (Unit FC =andesitic lavas and pyroclastic deposits) and for (b) the not homogeneous stratigraphy (Unit FC; Unit B= Cretaceous limestones and intrusive rocks forming the bed-rock underlying the CVC; Unit GF= Quaternary alluvial, colluvial, and lacustrine deposits filling the graben; Unit VD= volcaniclastic deposits covering the southern flank of the CVC). The blue line contours the unperturbed part of the domain, which extends ca. 30 km horizontally and ca. 25 km vertically. Note that the scale of stress values is the same for the all simulations.

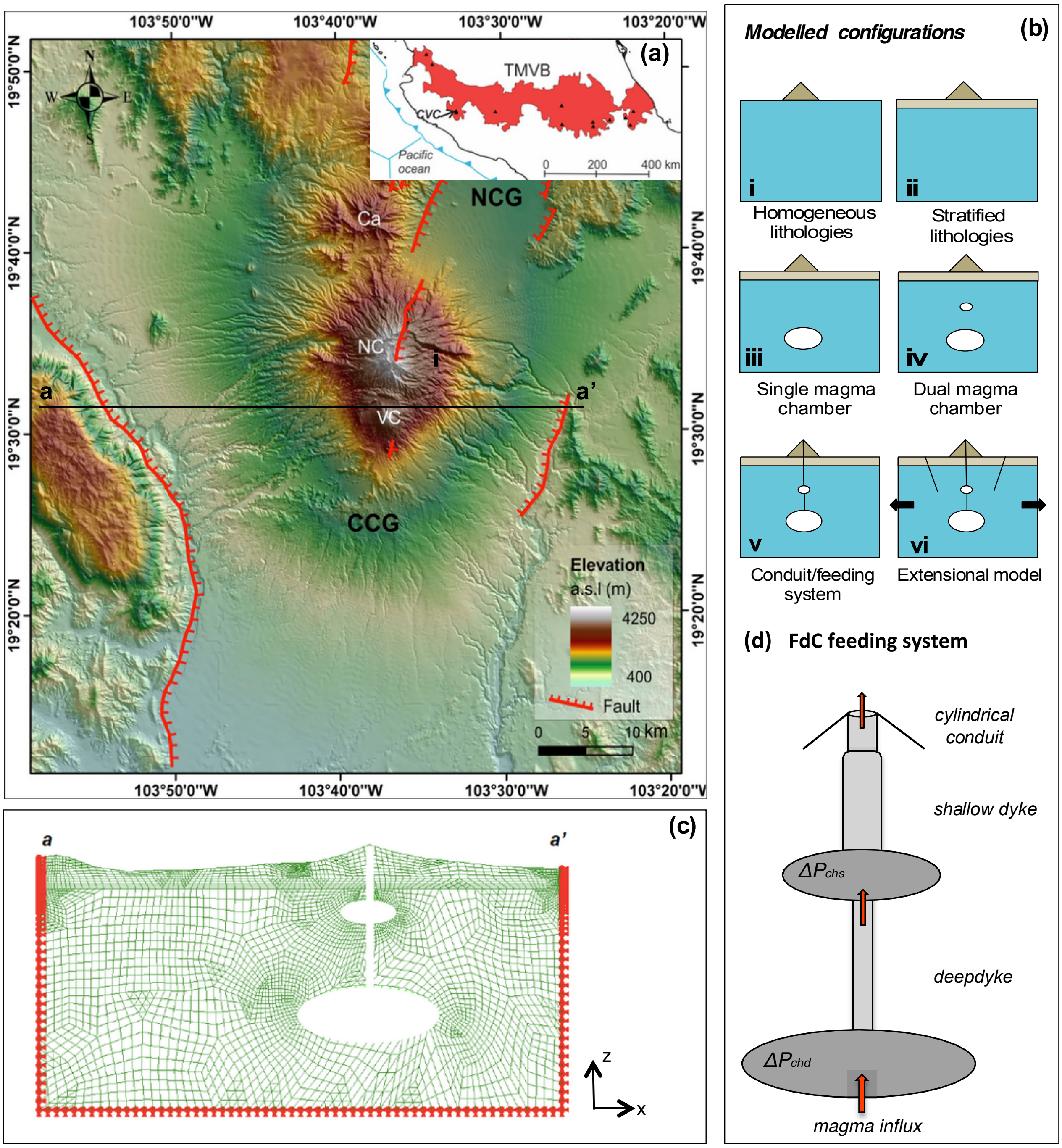
Fig. 5 E-W gravitational modelling of the CVC domain with a not homogeneous stratigraphy. The magnitude and pattern of the principal stresses are reported for (a) the single magma chamber model represented by a magma chamber ($2a$ = 14 km and $2b$ = 3.6 km) at 15 km of depth, and (b) the dual magma chamber model composed of a 15 km-deep magma chamber ($2a$ = 14 km and $2b$ = 3.6 km) and a shallow 6 km-deep one ($2a$ = 3.5 km and $2b$ = 2 km). The magma chambers are not connected. The magmatic overpressures are set to 10 and 5 MPa for the 15 km-deep and 6 km-deep magma chambers, respectively. The number of nodes is set to 4426 and 4161 for the single and dual magma chamber models, respectively. Black dotted lines highlight the passage from different stress values. The red dotted line in panel (b-i) indicates the formation of the stress arch. Note that the scale of stress values are different for each panel in order to maximise the simulation details.

Fig. 6 E-W gravitational modelling of the CVC domain with a not homogeneous stratigraphy accounted for a dual magma chamber system connected by dykes via surface (deep magma chamber, $2a$ = 14 km and $2b$ = 3.6 km at 15 km of depth; shallow magma chamber, $2a$ = 3.5 km and $2b$ = 2 km at 6 km od depth). The magnitude and pattern of the principal stresses are shown. The number of nodes used is set to 3737. The magmatic overpressures are set to 10 and 5 MPa for the 15 km-deep and 6 km-deep magma chambers, respectively. The black dotted lines in panel (ii) highlight the passage from different stress values. Note that the scale of stress values are different for each panel in order to maximise the simulation details.

Fig. 7 E-W gravitational modelling of the CVC domain with a not homogeneous stratigraphy considering the extensional field stress. The magnitude and pattern of the principal stresses are shown for the single magma chamber model (panels i-ii), the dual magma chamber model (panels iii-iv), the dual magma chamber with conduits model (panels v-vi-vii-viii). Note that in panel vii-viii the faults bordering the Colima graben are shown. For all configurations an extensive far-field stress of 5 MPa is applied at the lateral boundaries of the domain. In panels vii-viii the additional effect of the local extensive field is simulated using a reduced values of material's properties (Table 2). The magmatic overpressures are set to 10 and 5 MPa for the 15 km-deep and 6 km-deep magma chambers, respectively. Black dotted lines highlight the passage from different stress values. The red arrows indicate the direction of the applied far field stress. Note that the scale of stress values are different for each panel in order to maximise the simulation details.

Figures

Figure 1



(a)
103°50'0"W
103°40'0"W
103°30'0"W
103°20'0"W
19°50'0"N
19°40'0"N
19°30'0"N
19°20'0"N
TMVB
CVC
Pacific ocean
0 200 400 km
NCG
Ca
NC
VC
CCG
a
a'
Elevation a.s.l (m)
4250
400
Fault
0 5 10 km
(b)
Modelled configurations
i Homogeneous lithologies
ii Stratified lithologies
iii Single magma chamber
iv Dual magma chamber
v Conduit/feeding system
vi Extensional model
(c)
a
a'
z
x
(d) FdC feeding system
cylindrical conduit
shallow dyke
ΔP chs
deepdyke
ΔP chd
magma influx

Figure 2

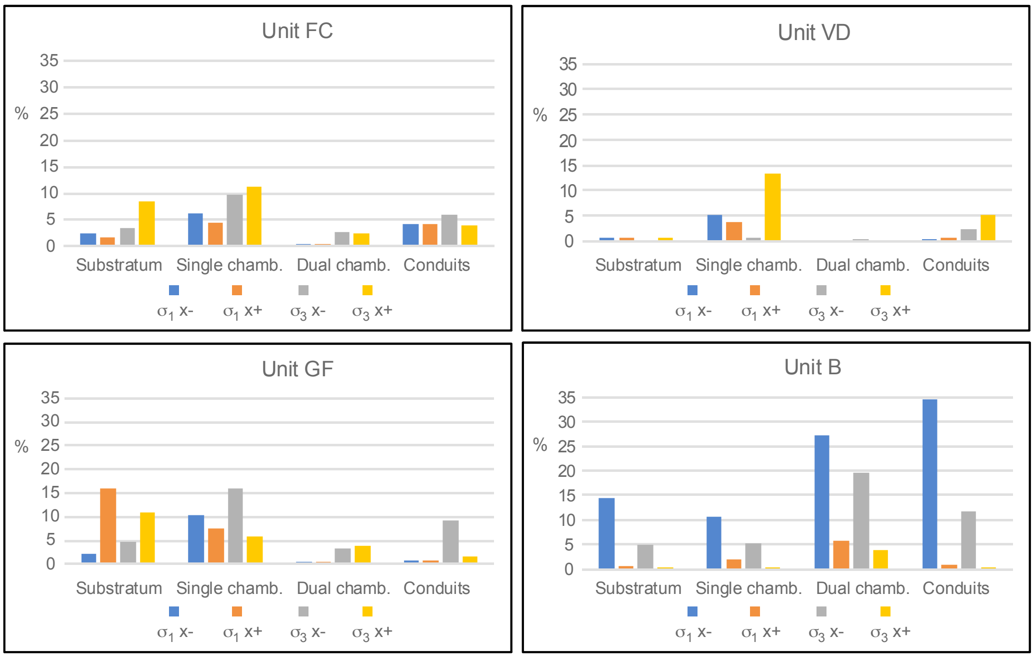

Unit FC
Unit VD
Unit GF
Unit B
%
35
30
25
20
15
10
5
0
Substratum
Single chamb.
Dual chamb.
Conduits
σ1 x-
σ1 x+
σ3 x-
σ3 x+

Figure 3

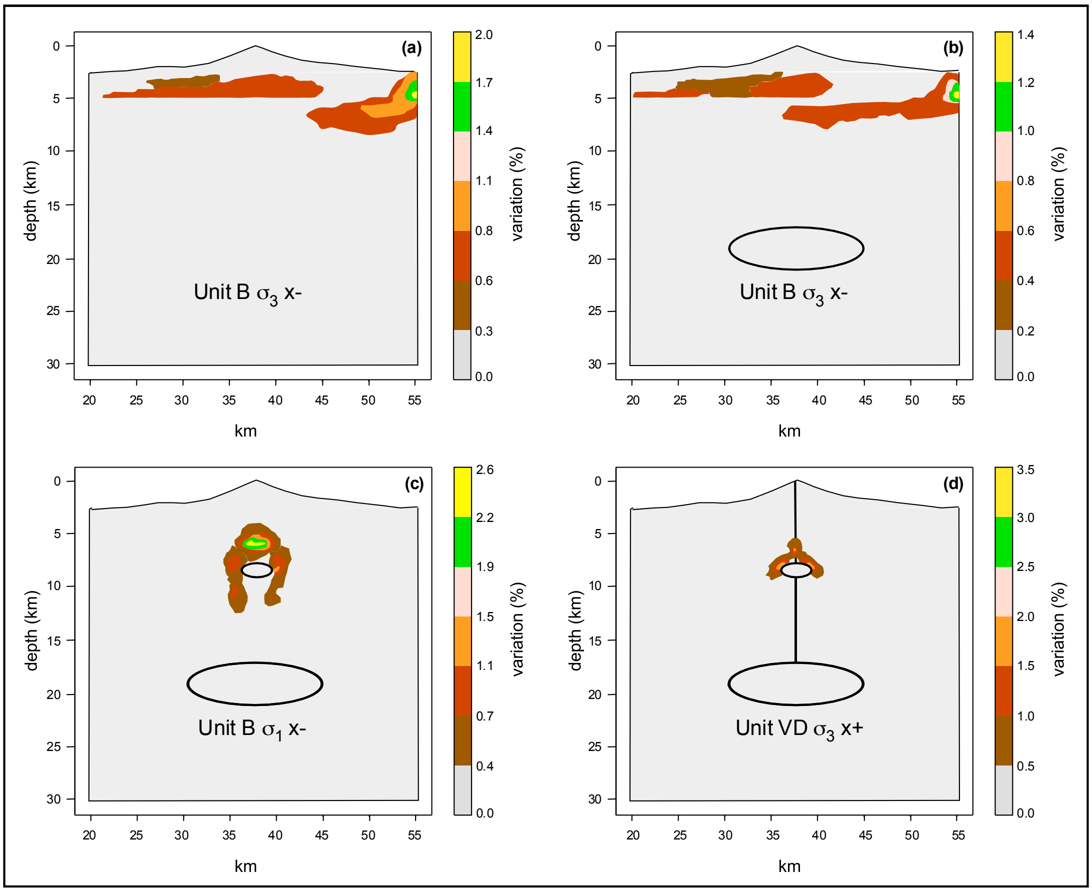
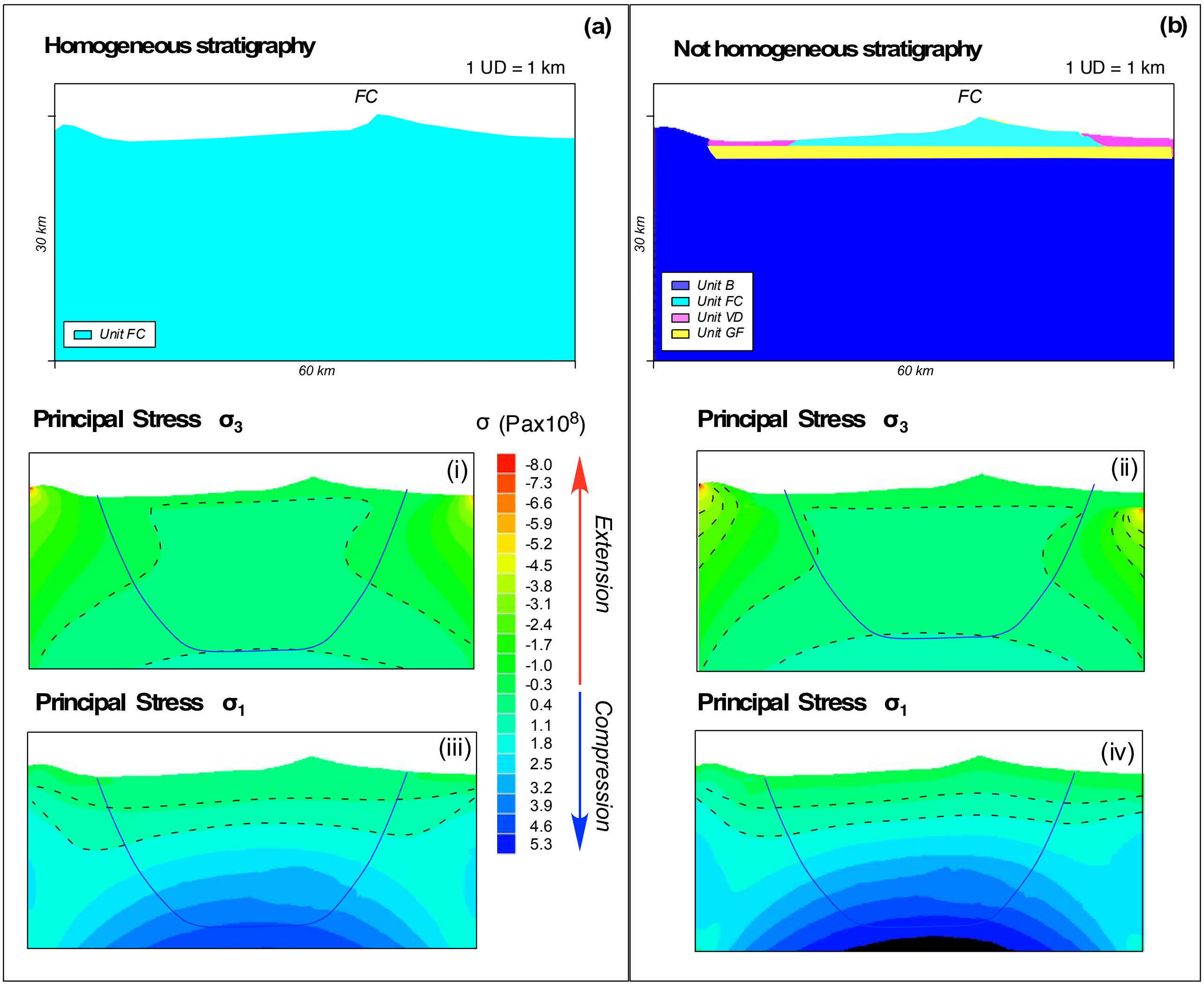

(a)
Unit B σ_3 x-
(b)
Unit B σ_3 x-
(c)
Unit B σ_1 x-
(d)
Unit VD σ_3 x+
depth (km)
km
variation (%)

Figure 4



(a)
Homogeneous stratigraphy
1 UD = 1 km
FC
30 km
60 km
Unit FC
(b)
Not homogeneous stratigraphy
1 UD = 1 km
FC
30 km
60 km
Unit B
Unit FC
Unit VD
Unit GF
Principal Stress σ3
Principal Stress σ1
σ (Pax10^8)
-8.0
-7.3
-6.6
-5.9
-5.2
-4.5
-3.8
-3.1
-2.4
-1.7
-1.0
-0.3
0.4
1.1
1.8
2.5
3.2
3.9
4.6
5.3
Extension
Compression
(i)
(ii)
(iii)
(iv)

Figure 5

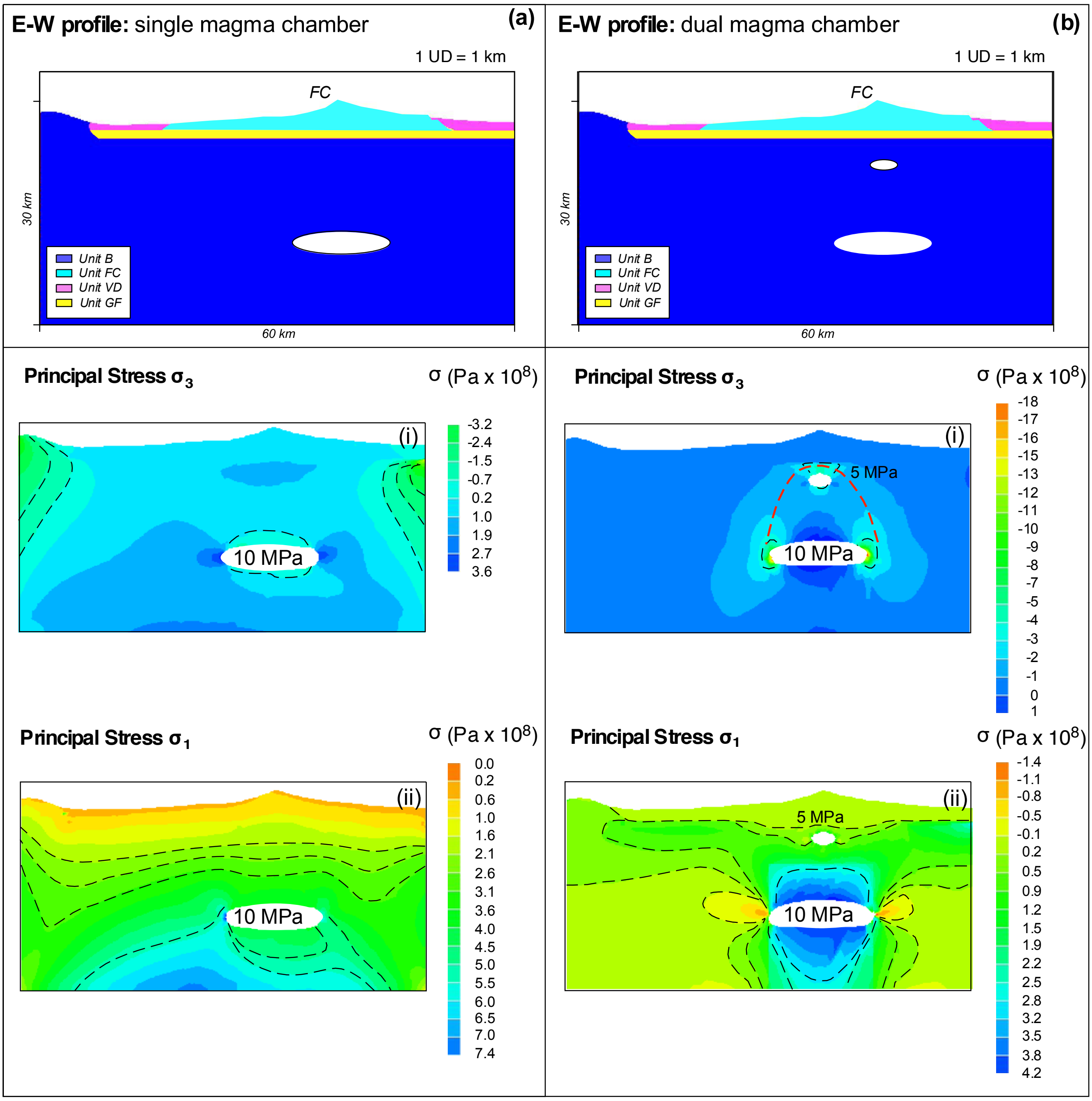

E-W profile: single magma chamber
(a)
1 UD = 1 km
FC
30 km
60 km
Unit B
Unit FC
Unit VD
Unit GF
E-W profile: dual magma chamber
(b)
1 UD = 1 km
FC
30 km
60 km
Unit B
Unit FC
Unit VD
Unit GF
Principal Stress σ3
σ (Pa x 10^8)
(i)
10 MPa
-3.2 -2.4 -1.5 -0.7 0.2 1.0 1.9 2.7 3.6
Principal Stress σ3
σ (Pa x 10^8)
(i)
5 MPa
10 MPa
-18 -17 -16 -15 -13 -12 -11 -10 -9 -8 -7 -5 -4 -3 -2 -1 0 1
Principal Stress σ1
σ (Pa x 10^8)
(ii)
10 MPa
0.0 0.2 0.6 1.0 1.6 2.1 2.6 3.1 3.6 4.0 4.5 5.0 5.5 6.0 6.5 7.0 7.4
Principal Stress σ1
σ (Pa x 10^8)
(ii)
5 MPa
10 MPa
-1.4 -1.1 -0.8 -0.5 -0.1 0.2 0.5 0.9 1.2 1.5 1.9 2.2 2.5 2.8 3.2 3.5 3.8 4.2

Figure 6

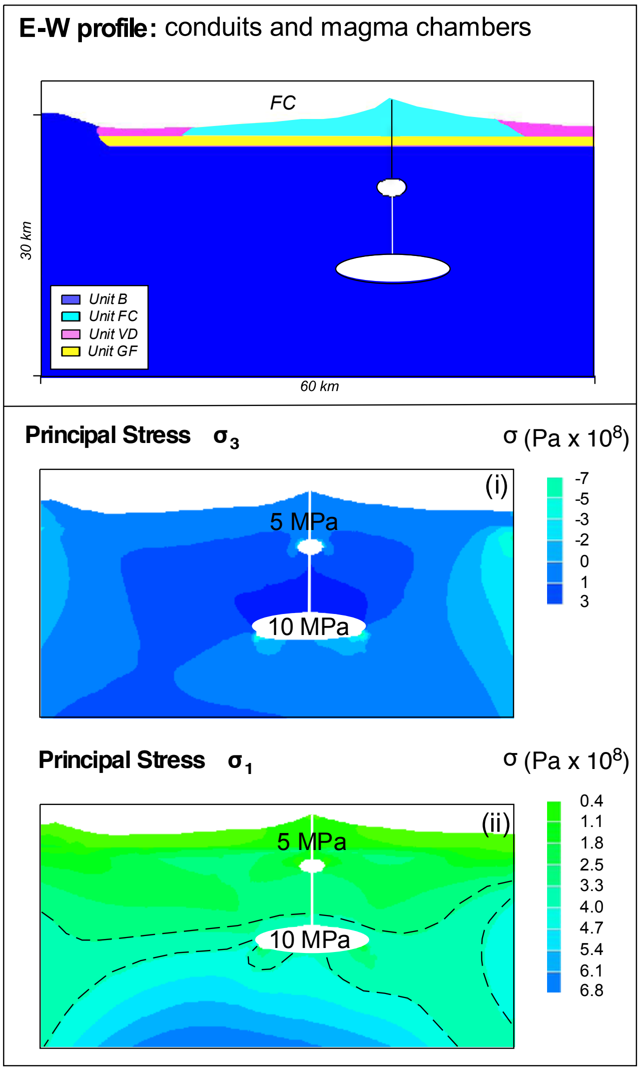
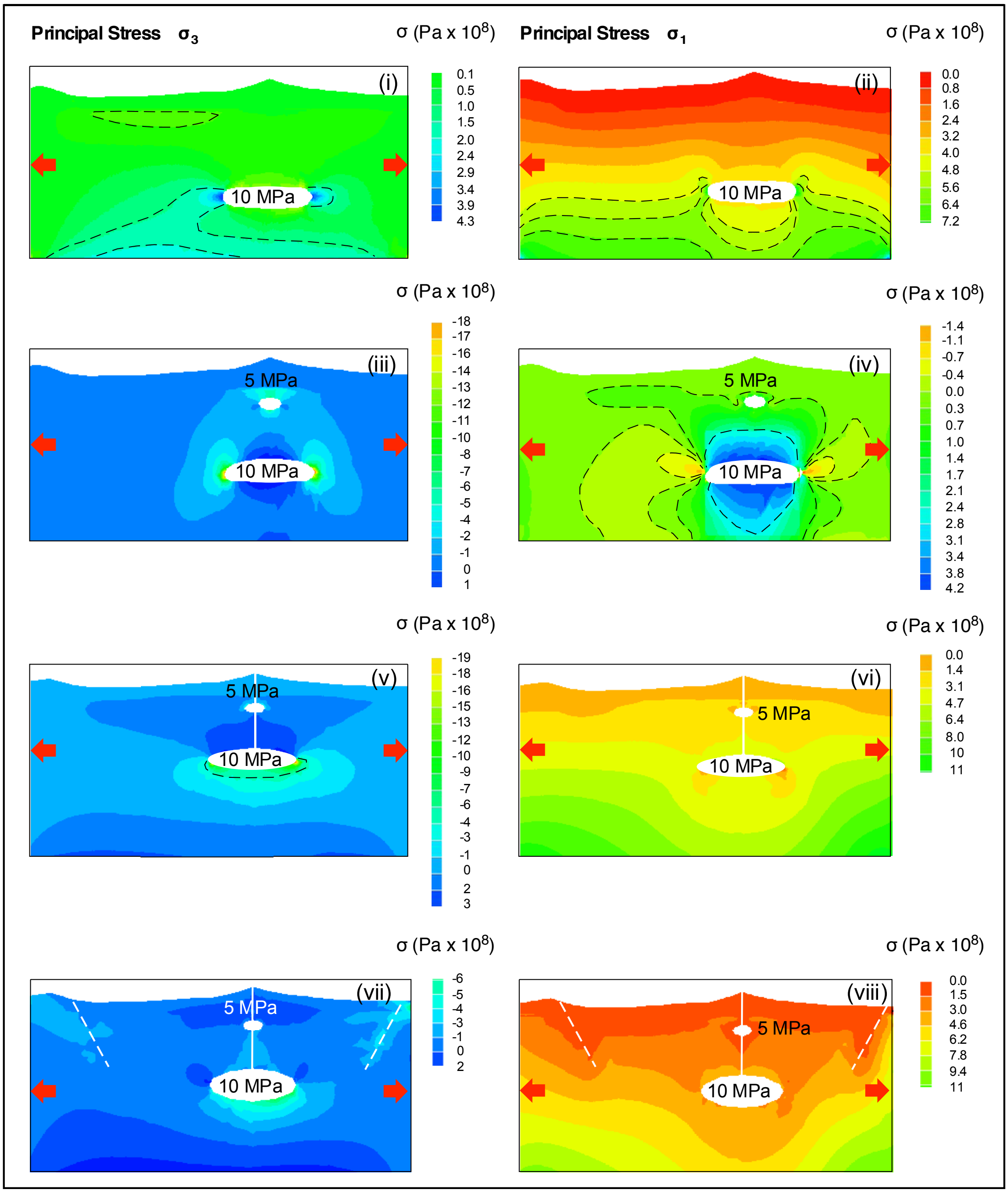

E-W profile: conduits and magma chambers
FC
30 km
60 km
Unit B
Unit FC
Unit VD
Unit GF
Principal Stress σ3
σ (Pa x 10^8)
(i)
5 MPa
10 MPa
-7
-5
-3
-2
0
1
3
Principal Stress σ1
σ (Pa x 10^8)
(ii)
5 MPa
10 MPa
0.4
1.1
1.8
2.5
3.3
4.0
4.7
5.4
6.1
6.8

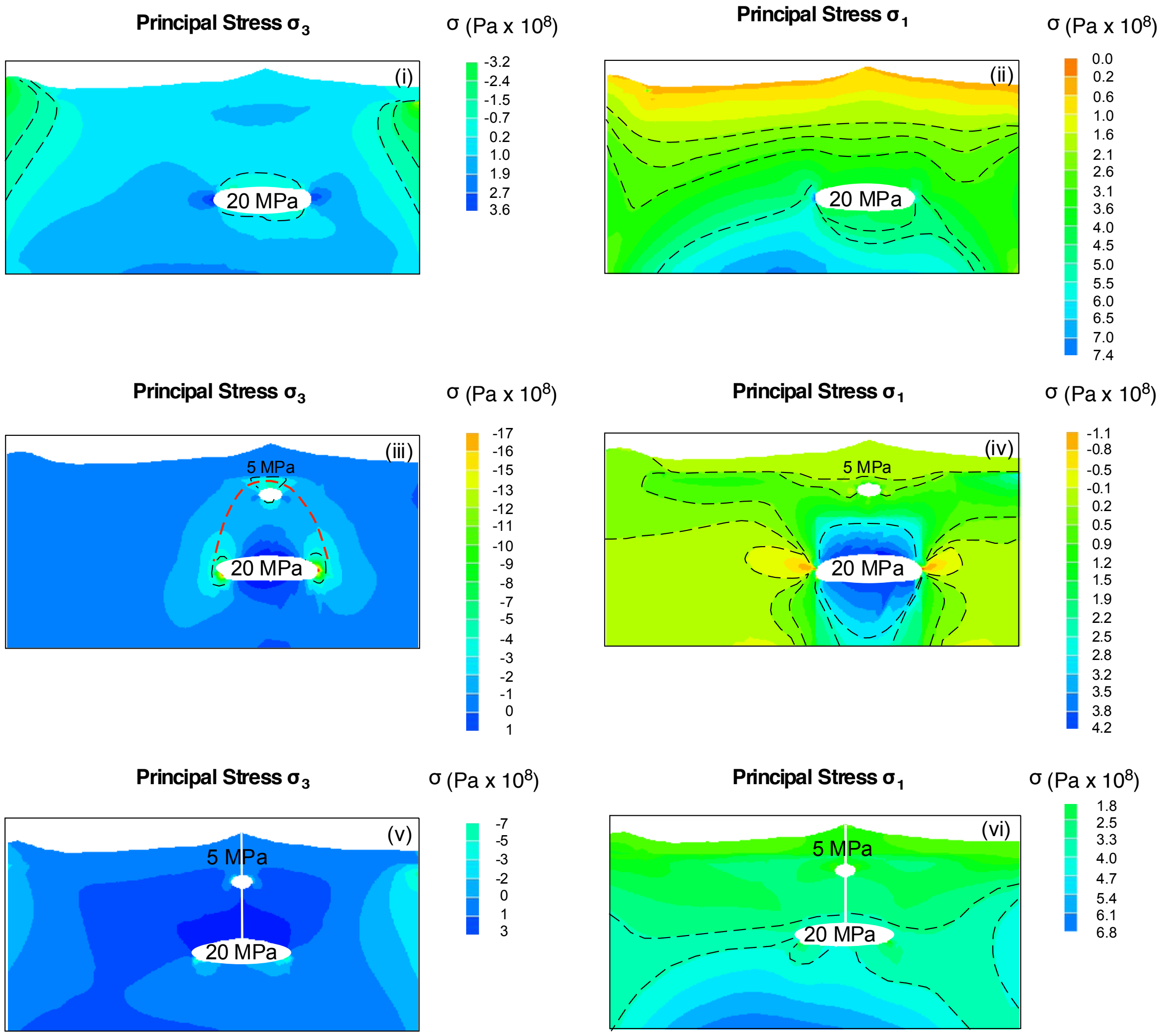
Figure 7



Principal Stress σ3
σ (Pa x 10^8)
0.1 0.5 1.0 1.5 2.0 2.4 2.9 3.4 3.9 4.3
(i)
10 MPa
Principal Stress σ1
σ (Pa x 10^8)
0.0 0.8 1.6 2.4 3.2 4.0 4.8 5.6 6.4 7.2
(ii)
10 MPa
σ (Pa x 10^8)
-18 -17 -16 -14 -13 -12 -11 -10 -8 -7 -6 -5 -4 -2 -1 0 1
(iii)
5 MPa
10 MPa
σ (Pa x 10^8)
-1.4 -1.1 -0.7 -0.4 0.0 0.3 0.7 1.0 1.4 1.7 2.1 2.4 2.8 3.1 3.4 3.8 4.2
(iv)
5 MPa
10 MPa
σ (Pa x 10^8)
-19 -18 -16 -15 -13 -12 -10 -9 -7 -6 -4 -3 -1 0 2 3
(v)
5 MPa
10 MPa
σ (Pa x 10^8)
0.0 1.4 3.1 4.7 6.4 8.0 10 11
(vi)
5 MPa
10 MPa
σ (Pa x 10^8)
-6 -5 -4 -3 -1 0 2
(vii)
5 MPa
10 MPa
σ (Pa x 10^8)
0.0 1.5 3.0 4.6 6.2 7.8 9.4 11
(viii)
5 MPa
10 MPa

Appendix 1

Appendix 1



Appendix 2

Appendix 2