Numerical Simulation of <u>Present dayContemporary</u> Kinematics at the Northeastern <u>Margin of the Tibetan Plateau and its implications</u> for seismic hazard assessment

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Abstract. The slip rates of active faults at the northeastern margin of the Tibetan Plateau (NETP) must should be clarified to understand the lateral expansion of the Tibetan Plateau and assess the seismic hazards in this region. To obtain the continuous slip rates of active faults at the NETP, we constructed a three-dimensional geomechanicsnumerical model of the NETP. The model explains the fault systems, topographic undulations, and crustal stratigraphy of the study area. It which includes a complex 3D fault system. The model also accounts for the physical rock properties, gravity fields, fault friction coefficients, initial erustal stresses, stress and boundary conditions. The Then we presented the long-term kinematics of NETP according to the horizontal and vertical erustal velocities and fault slip rates of active faults in the study area were obtained acquired from simulations using the aforementioned the model. The results were then validated against independent geographic datasets. Based on the analysis of the fault kinematics in the study area, The fault kinematic characteristics indicate that the Laohushan, middle-southern Liupanshan, and Guguan-Baoji faults, as well as the locked fault zone at the junction area of the Maxianshan and Zhuanglanghe faults, represent are potential hazard areas for strong earthquakes. However, as these faults are currently in the stress accumulation stage, they are unlikely to cause a majorstrong earthquake in the short term. In contrast, it is likely that the Jinqiangshan— Maomaoshan fault will generate a -Ms7.0Ms 7.1-7.3 earthquake in the coming decades. Based on In addition, the analysis of severalvelocity profiles across the NETP, imply that the deformations at plate rotation is the primary mechanism for the deformation of the NETP are continuous ineven though the Bayan Harintrablock straining and Qaidam blocks, as well as in the block like in Qilian Block, particularly around the Haiyuan Faultfaulting are nonnegligible.

1 Introduction

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The northeastern margin of the Tibetan Plateau (NETP) is the growth front of the Tibetan Plateau (TP) system and a modern topographic). Modern geomorphology and tectonic framework that features of the NETP are inferred to be formed due to the expansion of the TP toward its periphery, which has been ongoing since the Indian and Eurasian

plates collided ((P. Zhang et al., 2013; P. Zhang et al., 2014). This region contains some of Having experienced the most easily deformed and flowing crustal matter worldwide, with extremely intense tectonic movements and seismic activities, and a complex and highly varied tectonic system characterized by strong Cenozoic deformation (Zhang, 1999). The NETP is intersected by many, crust of this area develops a complex fault system with several large and deep and large faults, such as the generalized Haiyuan, fault (F1), West Ordos fault (F2), West Qinling, Huanghe, Luoshan, Yunwushan, and Xiaoguanshan faults, which fault (F3), East Kunlun fault (F4), that divide the NETP into several active tectonic blocks. These blocks include the Alxa, Ordos, Qilian, Qaidam, and Bayan Har blocks (Zhang et al., 2003; see Figure Fig.1). The These faults have been highly active since the Holocene are characterized by extremely intense tectonic movements and have caused many large earthquakes, including 17 seismic activities (Zhang, 1999; Zheng et al., 2016b). At least 5 earthquakes with a magnitude magnitudes of ≥ 7 and several $M \geq 8.0$ earthquakes, such as the 1654 M_8.0 Tianshui, 1739 M_8.0 Pingluo, 1879 M_8.0 Wudu, 1920 M_8.0 Haiyuan, and 1927 M_8.0 Gulang earthquakes (Figure, occurred in this area and caused huge loss of life and property in history (Fig. 1). The Since the generation, occurrence, and strengthmagnitude of an earthquake areis closely related to fault activity. The segmentation of active faults and their, long-term slip rates are imperative in seismological research and important predictors of fault slip rate plays a key role in medium- and long-term seismic hazardshazard assessment (Ding et al., 1993; Xu et al., 2018). Accurate For example, combined with coseismic displacements, long-term fault slip rates can be used to calculate seismic cyclescarthquake recurrence interval (Shen et al., 2009) and assess the seismogenic magnitudes of potential earthquakes (Bai et al., 2018; Hergert et al., and Heidbach, 2010). Continuous Moreover, the spatially continuous fault slip rates, which are lack in the NETP, can also be used to reconstruct the tectonic evolution of anthis area, which may and provide important insights into the lateral expansion pattern and mechanical deformation mechanisms of the TP (Royden et al., 1997; Tapponnier et al., 1982; Zhang et al., 2004). Therefore, detailed studies must be performed on the slip rates of active faults in the NETP.

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The Although there has been extensive research on the fault slip rates of active faults-in the NETP have been extensively studied by using geologic (Chen et al., 2019; Li et al., 2009; Li et al., 2018; Matrau et al., 2019; Wang et al., 2021; X. Li et al., 2017) and or geodetic (Hao et al., 2021; Li et al., 2019; Li, Pierce, et al., 2021; X. Li et al., 20172019) approaches. However, both approaches have limitations. The fault-, a systematic mismatch is typically found between the slip rates calculated from geological records and that obtained from geological slip rates only represent the rate at each point of measurement, which does not necessarily represent the fault as a whole. Furthermore, geologic fault slip rates are generally averaged over long periods of time and therefore provide limited information regarding present day fault movements. Conversely, the geodetic approach assumes that each block is rigid with negligible internal deformation. The results activities of one fault branch that measured in a fault zone, which is always consist of several studies branches. They are usually lower than the geodetic slip rates on the fault as a whole if a rigid block assumption is adopted in the geodetic inversion process (Shen et al., 2009). However, several crustal deformation studies conducted in TP demonstrated that the internal deformations of the TP are "continuous" (Royden et al., 1997; Zhang et al., 2004). Therefore, internal block deformation in the NETP cannot be ignored. Numerical simulations are (Royden et al., 1997; Zhang et al., 2004; Y. Li et al., 2017, 2021). Numerical modeling provides a

powerful tool for systematic fault to study the large-scale crustal kinematics studies (Hergert and Heidbach, 2010; Hergert et al., 2011; Li, Hergert, et al., 2021) as they provide a well as the comprehensive 3D view of eurrent-fault activities. However, with spatially continuous distribution. High efficiency and accuracy have made the focus of previous numerical studies onmodeling a widespread technology in the NETP has been placed primarily onfield of geosciences, especially for the crustal stress environment and seismic activitystudy of kinematics and dynamics of the NETP (Pang et al., 2019b2019a, b; Sun et al., 2018, 2019) or on the analysis of factors affecting crustal movements (Pang et al., 2019a; Zhu et al., 2018). In contrast, detailed studies of the : Xiao and He, 2015). However, all these previous numerical models are either two-dimensional (2D) or three-dimensional (3D) with extremely simplified fault planes. To our knowledge, so far there is no 3D geomechanical model that take into the complex 3D fault system in the NETP. Therefore, detailed kinematics of the crust and active faults in the NETP are scarcestill remains unclear.

In this study, we constructed a 3D geomechanicsinstead of a simple conceptual model, a comprehensive 3D geomechanical model of the NETP fault system to elucidate the slip rates of the with detailed complex 3D fault geometries, heterogeneous rock properties and reasonable initial crustal stress is constructed. After calibrated by model-independent observations, the results of the geomechannical model, such as the horizontal crustal velocities, spatially continuous slip rates of major active faults, faults, are presented. Based on these results, we summarized the long-term crustal deformation characteristics, and partitioning of deformation modes (between block like and continuous deformation). The results were then used to analyze in the NETP. Finally, we assessed the seismic hazards of major faults at the NETP. Based on this numerical study, important data were obtained that provide insights into the motions and transformations of active tectonic structures at the NETP.in the study area, and suggested that the Jinqiangshan–Maomaoshan fault has the potential for a M_S 7.1—7.3 earthquake in the coming decades.

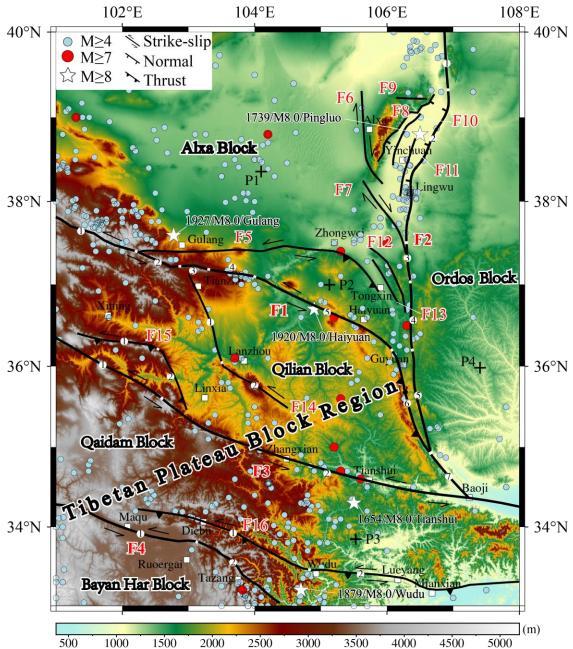


Figure 1. Map of active faults and earthquakes of the NETP. Black lines represent the active faults. Faults The light blue, red dots and the white pentagrams represent earthquakes from 1831 BC to 2017 AD from the National Earthquake Data Center (http://data.earthquake.cn). Black crosses (P1-P4) indicate the locations of four test sites for the comparison with the numerical model shown in Fig. 3b. Faults discussed in the text are labeled as followed: F1-1 = LLLF = Lenglongling fault; F1-2 = JQHF = Jinqinaghe fault; F1-3 = MMSF = Maomaoshan fault; F1-4 = LHSF = Laohushan Faultfault; F1-5 = HYF = Haiyuan Faultfault. F1-6 = LPSF = Liupanshan Faultfault; F1-7=GG-BJF=Guguan-Baoji fault; F2-1 = ZZSF = Zhuozishan Faultfault; F2-2 = HHF = Huanghe Faultfault; F2-3 = LSF = Luoshan fault; F2-4 = YWSF = Yunwushan fault; F2-5 = XGSF = Xiaoguanshan Faultfault; F3-1 = DTH-LXF = Daotanghe-Linxia fault; F3-2 = WQLF = West Qinling Faultfault. F4-1 = EKLF = Eastern Kunlun fault; F4-2 = TZF = Tazang Faultfault; F5 = TJSF = Tianjingshan fault; F6 = WHLSF = West Helanshan fault; F7 = NSSF = Niushoushan fault; F8 = EHLSF = East Helanshan fault; F9 = ZYGF = Zhengyiguan fault; F10 = LHTF = Lyhuatai fault; F11 = YCF = Yinchuan fault; F12 = YTSF = Yantongshan fault; F13 = QSHF = Qingshuihe fault; F14-1 = ZLSF = Zhuanglanghe fault; F14-2 = MXSF=Maxianshan Faultfault. F15-1 = WLJSF = West section of Lajishan fault; F15-2 = ELJSF = East section of Lajishan fault; F16-1 = DB-BLJF = Diebu-Bailongjiang fault; F16-2 = WD-KXF = Wudu-Kangxian fault.

2 Model concept and input

2.1 Model geometry

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The 3D geomechanics model of this work is a rectangular <u>euboidcartesian 3D block</u> with an E–W length of 654 km (101°E–108°E), N–S length of 777 km (33°N–40°N), and thickness of <u>~80</u> km. The <u>topographic undulationstopography</u> of the model's surface <u>were characterized using based on GTOPO30</u> elevation data, which has a resolution of 30 arcseconds, (about 900m). The model comprises four layers: the upper crust, middle crust, lower crust, and upper mantle, from top to bottom. The geometric data of the layer interfaces were derived from CRUST1.0 (Laske et al., 2013).

Based on the cuttingtheir depth, the faults of the model can be categorized into lithospheric and intracrustal faults. Lithospheric faults (i.e.g., F1, F2, F3, and F4) are plate boundaries because they cut through the Moho and reach the bottom of the model (FigureZhan et al., 2005; B. Liu et al., 2017; Zhao et al., 2015; Fig. 2a and Figure 2b, b; Table 1). All other faults are intracrustal faults because the depth data indicate they that terminate in the upper, middle, or lower crust- (Yuan et al., 2002b, 2003; Lease et al., 2012; Meng et al., 2012; B. Liu et al., 2017; Wu et al., 2020). The fault traces were obtained are modified from Xu et al. (2016) and the attitudes were derived of these faults are summarized from previously published data including surface-based fault surveys and deep seismic sounding-profiles (Table 1). The results of In the NETP, many studies indicated a geophysical investigations found that low-velocity bodybodies exist widely in the upper middle-lower crust and that the deformations in the upper crust are not coupled to those in the underlyingmiddle-lower crust (Bao et al., 2013; Wang et al., 2018; Ye et al., 2016). Therefore, we introduced a contact surface between the upper and middle crusts were decoupled in into the model to and account it as a detachment layer that make the upper crust decouple from the middle crust and allow the upper crust to slides liding freely along its bottom interface the contact surface according to the stress conditions.

The model was meshed using tetrahedron elements. The <u>elements were element size is</u> 1–2 km <u>wide at the faults</u>. The <u>largest elements outside near</u> the faults <u>were and increases to</u> ~10 km <u>wide. The at the model boundary. The model totally contained 8,463,583 elements (<u>Figure Fig. 2a</u>).</u>

2.2 Rock properties

TheIn order to obtain the time-independent contemporary background crustal stress—strain relationships of the rocks were modeled using their elastic parameters (Hergert et al., 2010, 2011; Li, Hergert, et al., 2021). NETP, we assumed that the rock rheology in the model is linear elasticity, consistent with the observations that the large-scale continental crust always exhibits elastic-brittle behavior rather than elastic-viscous behavior (Armijo et al., 2004; Hubert-Ferrari et al., 2003). The model was divided into three major tectonic elementsunits—the Alxa, block, the Ordos block, and the TP blocksblock region. The part of the TP block region that located in the study area comprises the Qilian, Qaidam, and Bayan Har blocks. Each tectonic element containedThe rock properties of each block contain the elastic parameters (i.e. the Young's modulus, density, and Poisson's ratio) of the upper, middle, and lower crust as well as those of the upper mantle, with each set of elastic parameters including the Young's modulus, density, and Poisson's ratio (Figure (Fig. 2a). The density and Poisson's ratio were derived from CRUST1.0 (Laske et al., 2013). The Young's

modulus <u>adopted in our model is static and was converted from the dynamic elastic modulus using the empirical equation of Brotons et al. (2016)</u>, <u>which</u> was calculated based on the P-wave velocities, S-wave velocities, and densities derived from CRUST1.0 <u>using the empirical equation of Brocher (2005)</u>. The Young's modulus, computed from seismic wave velocities, corresponded to the dynamic elastic modulus, which is generally greater than a rock's static Young's modulus. Therefore, the Young's modulus values were converted into static Young's moduli using the empirical equation of Brotons et al. (2016). The elastic parameters used in the model are listed in Table 2.

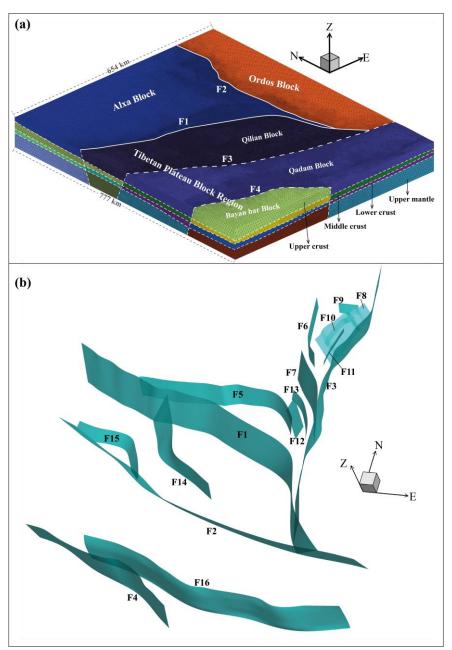


Figure 2. Model geometry and implemented fault system. (a) Distribution of the rock properties types employed for the model. Different colors represent different rock properties. (b) Cyan surfaces indicate the faults implemented in the model as frictional contact surfaces. Fault names can be found in Figure Fig. 1.

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Table 1. Geometric parameters of faults in the model

	Fault name	Strike	parameters of faults in Dip direction—(°)	Dip (°)	Reference
F1	/	NWW-SSE	SW	70	RGAFSAO, 1988
F2-1	ZZSF	N-S	W	70	Gao, 2020
F2-2	HHF	N-S	W	70	Bao et al., 2019
F2-3	LSF	N-S	W	80	Wang et al., 2013
F2-4	YWSF	N-S	W	70	NIGS, 2017
F2-5	XGSF	N-S	W	70	NIGS, 2017
F3-1	DTH-LXF	MANA GGE	NE	70	Zhou et al., 2009
F3-2	WQLF	NWW-SSE	NE	70	Li, 2005
F4-1	EKLF	NW-SE	NE	75	Z. Liu et al., 2017
F4-2	TZF			, .	J. Li et al., 2019
	East section of TJSF	NW-SE	SW	70	RGAFSAO, 1988
F5	West section of	E-W	S	70	RGAFSAO, 1988
	TJSF				T : 2015
F6	WHLSF	N-S	W	80	Lei, 2015
F7	NSSF	NW-SE	SW	70	RGAFSAO, 1988
F8	EHLSF	NE-SW	SE	60	Du, 2010
F9	ZYGF	E-W	S	60	NIGS, 2017
F10	LHTF	NNE-SSW	SE	70	NIGS, 2017
F11	YCF	NNE-SSW	NW	70	NIGS, 2017
F12	YTSF	NW-SE	SW	65	NIGS, 2017
F13	QSHF	NW-SE	SW	45	Tian et al., 2020
F14-1	ZLHF	NNW-SSE	SW	45	Xu et al., 2016
F14-2	MXSF	NW-SE	SW	80	Hou et al., 1999
F15	LJSF	NWW-SSE	SW	50	Yuan et al., 2005
F16-1	DB-BLJF	NW-SE	SW	70	Yuan et al., 2007
F16-2	WD-KXF	E-W	SW	70	Jia et al., 2012

The detailed fault names are defined in FigureFig. 1.

Table 2. Material parameters Rock properties of the finite element model

	A	lxa Block		Oı	Ordos Block			Tibetan Plateau Block		
	ρ				ρ					
	E(Gpa)	(g/cm^3)	ν	E(Gpa)	(g/cm^3)	ν	E(Gpa)	ρ (g/cm ³)	ν	
Upper crust	77.4	0.244	2.74	77.4	0.244	2.74	76.8	0.243	2.74	
Middle crust	84.2	0.247	2.78	84.2	0.247	2.78	84.5	0.246	2.78	
Lower crust	113.0	0.259	2.95	113.0	0.259	2.95	110.0	0.257	2.93	
Upper mantle	194.0	0.278	3.39	191.0	0.278	3.37	187.0	0.278	3.36	

E, ρ , and ν are Young's modulus, density, and Poison's ratio, respectively.

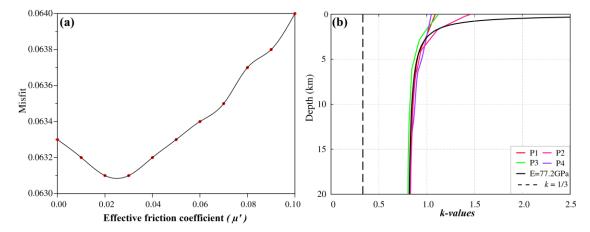


Figure 3. (a) Velocity misfit of the crustal velocity between the modeled results and GPS measurements as a function of the effective friction coefficient. The optimal friction coefficient was determined to be 0.02. (b) Depth profiles of the initial k-values at four test sites indicated in FigureFig. 1. The solid black line shows the stress state based on Equation (3), which was used as a reference stress state. For comparison, the low k-value based on the uniaxial strain state is also shown (dashed black line).

2.3 Friction coefficient

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In our model, frictional contacts between fault surfaces faults were considered obeyingto obey the Mohr-Coulomb friction law:

$$\sigma_{\rm S} = C_0 + \mu \cdot (\sigma_n - P_f) = C_0 + \mu' \cdot \sigma_n,\tag{1}$$

where σ_s is the shear forcestress on the fault surface at time of rupture, C_0 is the cohesion, μ is the coefficient of friction, σ_n is the normal stress on the fault surface, P_f is the pore pressure, and $\mu^{2'}$ is the effective coefficient of friction of the fault surface when accounting for the pore pressure. In our model, tThe cohesion C_0 of the rocks was assumed to be negligible (Jamison et al., 1980). The frictional relations friction coefficient of the fault surface are critically is important forto the kinematics of a fault,. However, these relations can be but it is complex in a fault and also varyvaries in time and space. The exact magnitude of the friction coefficient iscan be affected by various external factors including fluid-seepage, temperature-variations, stress states, and movement fault slip rate (Zhu et al., 2009). Therefore, it is challenging to obtain the precise friction coefficient of a fault. However, the results of many studies showed that large strike slip-faults generally have low effective friction coefficients. (Wang, 2021). For instance, the Haiyuan Fault has friction coefficients as low as 0.05 (He et al., 2013) and faults on the eastern margin of the TP have friction coefficients as low as 0.02 (Li et al., 2015; Li, Hergert, et al., 2021). Because of this information, simulations Simulations were performed with a series of friction coefficients (0–0.051) and the results were compared with GPS observations (Cianetti et al., 2001). The results showed that setting a friction coefficient of 0.02 for all faults yields the smallest fitting error (0.05389; FigureFig. 3a). To minimize the fitting error, localized adjustments were made for the friction coefficients of the F1 and F3 faults, which are large strike-slip faults. The final friction coefficients of F1, F3, and all other faults were 0.01, 0.1, and 0.02, respectively, with a fitting error of 0.04460536.

2.4 Initial stress state

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The <u>crustal</u> initial stress affects the <u>stress</u> state of <u>stress acting on</u> a fault, which <u>further</u> controls the kinematic <u>state</u> of the fault via the <u>Mohr–Coulomb</u> friction <u>coefficientlaw</u>. Therefore, the selection of appropriate initial <u>stressesstress</u> is important when <u>performing numerical simulations studying fault slip rates</u> based on geomechanics models. The initial stress <u>modelstate</u> that is most commonly employed in <u>previous</u> numerical <u>modeling</u> studies of the <u>TPNETP</u> is the uniaxial strain reference state (<u>Sun et al., 2019</u>; Zhu et al., 2016), which <u>predicts that all deformations due to gravitational loading occur inbased on</u> the <u>vertical direction and boundary condition</u> that no <u>expansion or contractionelongation occurs in the horizontal direction, and the strain only occurs in the <u>lateralyertical</u> direction. In this stress state, the ratio (*k*) of mean horizontal stress to vertical stress is only dependent on the Poisson's ratio:</u>

$$k = \frac{(S_H + S_h)}{2S_V} = \frac{v}{1 - v'},\tag{2}$$

where S_H , S_h , and S_V are the maximum horizontal, minimum horizontal, and vertical stress, respectively, and v is Poisson's ratio. For the typical v-value of 0.25, Equation (2) gives k = 1/3, which implies that the vertical stressesstress acting on the rock mass far exceed the horizontal stressesstress and that the crust is always in a normal faulting or extensional stress regime. However, this assumption contradicts the thrust and strike-slip stress regimes common in the crust. Furthermore, k-values obtained globally from in situ measurements always greatly exceed 1/3 even in extensional tectonic environments (Hergert and Heidbach, 2011).

Based on a spherical shell model, Sheorey (1994) proposed a method for the estimation of the initial crustal stress, which accounts for the curvature of the Earth, the properties of crustal and mantle materials, temperature fields, and other thermally dependent properties, as shown in Equation (3):

$$k = 0.25 + 7E \cdot \left(0.001 + \frac{1}{z}\right),\tag{3}$$

Where *E* is the Young's modulus of the rock (Gpa(GPa); and *z* is the depth from the surface (m). Because the *k*-values obtained predicted by this method are generally consistent with those obtained from ultra deep boreholesthe Continental Deep Drilling Program (Hergert and Heidbach, 2011), they are often Equation (3) has been widely used in numerical modeling studies performed by researchers outside Chinaworldwide (Ahlers et al., 2021; Buchmann et al., 2007; Rajabi et al., 2017; Reiter et al., 2014; Hergert and Heidbach, 2011; X. Li et al., 2022). However, In this approach is rarelystudy, we used in China. Equation (3) is used in our model to calculate the initial stresses. stress state for our model. The exact methodsprocedure for obtaining the initial stresses proposed by Sheorey (1994) have has been described previously by Hergert (2009); in detail. Figure 3b shows that the modeled initial stresses is in our model agreegood agreement with the theoretical results given by Sheorey (1994) Equation (3).

2.5 Kinematic boundary conditions

The GPS velocity field data of Wang et al. (2020) were used as lateral boundary conditions forof our model. Because of the scarcity of local vertical deformation data, the model boundaries were only were constrained in by the horizontal direction GPS velocity field data of Wang and it was Shen (2020) and were assumed that the lateral velocities of the 3D model do not vary withto be constant along depth. The vertical displacements of the model were unconstrained.

(Wang et al., 2008). The top surface of the model was configured as a free boundary, whereas the bottom surface slid freely in the horizontal direction, with a vertical velocity of 0. The detailed boundary conditions are shown in Figure 4Fig. 4. For the calculation, we used the finite-element software AbaqusTM because its powerful nonlinear processing capabilities. The model time is set as 500 ka, which is required to generate a proper contemporary state of stress and deformation until the accumulated displacements at the boundaries are propagated into the model.

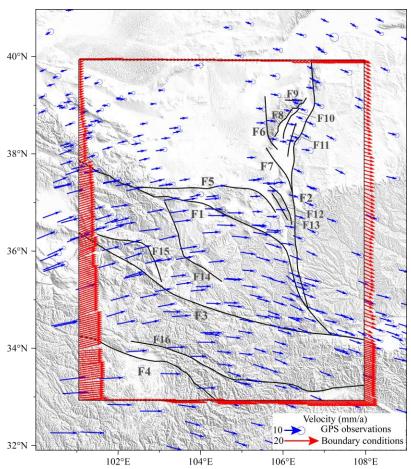


Figure 4. Boundary conditions of the model. The blue arrows represent the GPS observation velocities according to Wang et al. and Shen (2020). The red arrows at the boundary represent the boundary velocities calculated by the interpolation of the GPS observations. Fault names can be found in Fig. 1.

3 Results

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3.1 Horizontal crustal velocities

The distribution of calculated horizontal crustal velocities in the study area is are shown in Figure Fig. 5. In terms of the direction, the western and central parts of the study area are moving in the NEE and near-EW directions and the eastern part gradually changes in motion toward the SW or SEE directions. Therefore, the study area is characterized by clockwise crustal motions. In terms of erustal speed the movement rate, the model shows that the erustal speeds rates in the southwestern part of the study area are high, whereas they are low in the northeastern part. The movement rates of the Alxa Block in the north and Ordos Block in the east have crustal speeds of are as low as ~4–6 mm/a, indicating

that their internal deformation is low. Therefore, these blocks are relatively stable. The Bayan Har Block in the south has the highest crustal speed (movement rate up to 13–14 mm/a). The For the Qaidam Block exhibits crustal speeds of 11–12 mm/a on its western side and the Qilian Block, both of them exhibit a higher movement rate in the west than that in the east, decreasing from 12 to 9 mm/a on the eastern side. The western part of the Qilian Block has a crustal speed of 9 and from 10 mm/a, decreasing to 8 mm/a on the southeastern side, respectively.

Figure 5In addition, Fig. 5 also shows that large strike-slip faults control the distribution of crustal velocities: accommodate velocity gradients between adjacent blocks. For example, the modeled velocity map can be divided in several parts by the F1, F3, and F4 block boundary faults vertically cut through, across which the model and act as "separators" regarding movement rates of the crustal velocity distribution. This phenomenon is most pronounced crust change remarkably, especially at the F1 fault. The crustal speed movement rate on the southern side of the Qilian Block is 9–11 mm/a, whereas that on the northern side of the Alxa Block is 4–6 mm/a. Therefore, A different rate of ≥3 mm/a between the crustal speeds on opposing sides of two blocks is accommodated by the F1 fault can differ by ≥3 mm/a.

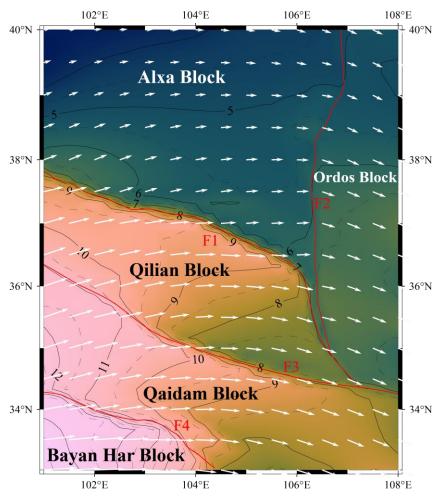


Figure 5. Distribution of modeled crustal surface velocities of the NETP with a grid interval of 0.5° both in longitude and latitude. White arrows represent the crust movement direction. The background color contours represent the magnitude of the velocity in mm/a. The red lines represent the faults implemented in the model. The names are defined in Figure Fig. 1.

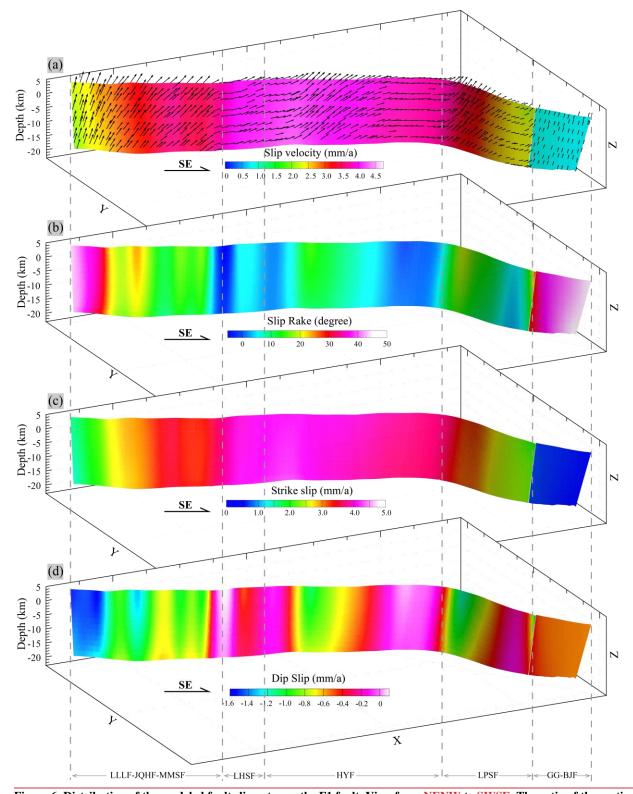


Figure 6. Distribution of the modeled fault slip rates on the F1 fault. View from NENW to SWSE. The ratio of the vertical to horizontal scale is 4:1. (a) Total slip rates with slip directions (black arrows). Parts of the fault has an oblique-slip component. (b) Slip rake. Positive values indicate that the fault's movement has a thrust component. (c) Slip rates along the fault's strike. Positive values represent sinistral strike-slip. (d) Slip rates along the fault's dip direction. Negative values represent thrust faulting.

3.2 Fault slip rates of the main faults

The dominant depth range of seismic activities in the study area is 5–15 km, with a few events at depths up to 20 km (Li et al., 2020; Y. Li et al., 2021). Therefore, we. As mentioned in the introduction, seismic activities are closely related to fault activities. In order to assess the seismic hazard reasonably on the faults in the NETP, we focused on the fault kinematics in the brittle crust and extracted the kinematic characteristics up to a depth of 20 km for the main faults of the study area using from our 3D geomechanics model. The extracted kinematic characteristics are described below.

3.2.1 Slip rate of the F1 fault

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From west to east, the F1 fault comprises the Lenglongling, Jinqianghe, Maomaoshan, Laohushan, Haiyuan, Liupanshan, and Guguan–Baoji faults (FigureFig. 1). Two earthquakes with a magnitudemagnitudes M ≥ 8.0 have occurred along this fault—the 1920 M_8.0 Haiyuan Earthquake and 1927 M_8.0 Gulang Earthquake, which formed 220 and 120 km long surface rupture zones, respectively (Guo et al., 2020; Liu-Zeng et al., 2015; Zhang et al., 1987). The 3D kinematic state of the F1 fault was extracted from the 3D geomechanics model, as shown in FigureFig. 6. On the western part of the F1 fault (Lenglongling, Jinqianghe, and Maomaoshan faults), the slip rates increase from 2.0 to 4.0 mm/a from west to east and continue to increase further east (Laohushan Fault and western part of the Haiyuan Fault. The eastern part of the Haiyuan Fault has a slip rates of the F1 fault decrease in the middle of the Haiyuan Fault. The eastern part of the Haiyuan Fault has a slip rate of ~3.5 mm/a. The slip rate of the Liupanshan Fault decreases in the SE direction and bottoms out at ~2.0 mm/a; aton the Guguan–Baoji Fault, the slip rate is lower than 1 mm/a (FigureFig. 6a). The slip rates obtained by our 3D geomechanics model for the Haiyuan Fault are much lower than olderearlier estimates (8.0–12 mm/a; Burchfiel et al., 1991; Lasserre et al., 1999; Zhang et al., 1988) but similar to more recent estimates (3.2–4.5 mm/a; Li et al., 2009; Matrau et al., 2019; Y. Li et al., 2017). The disagreements with earlier geological estimates may be related to the time scale and the extent to which faults have been studied (Li et al., 2009).

Although the F1 fault is predominantly a left-lateral strike-slip fault, it also has a thrust component (see Figure Fig. 6b). The Lenglongling, Jinqianghe, Maomaoshan, middle Haiyuan, and Liupanshan faults have the rake ranging from 10° to 20°, whereas the Guguan–Baoji Fault has the rake varying from 40° to 50°, indicating that they are oblique thrust faults. The Laohushan and western and eastern Haiyuan faults have rake below 10°, showing that left-lateral strike-slip faulting is dominant at these faults. Figures 6c and 6d show the continuous slip rates of the F1 fault along its strike and dip, respectively. The slip rates along the strike (Fig. 6c) are like the total slip rates- (Fig. 6a). The Laohushan and Haiyuan faults have the highest slip rates on the F1 fault. Conversely, the Lenglongling, Jinqianghe, Maomaoshan, and Liupanshan faults have high dip-slip rates.

3.2.2 Slip rate of the F2 fault

The F2 fault comprises the Zhuozishan, Huanghe, Luoshan, and Yunwushan—Xiaoguanshan faults (Figure Fig. 1). Figure 7 shows that right-lateral strike-slip faulting is prevalent across the entire F2 fault. However, the magnitude of the dip-slip component varies from one location to another. The Zhuozishan Fault is an oblique-slip reverse fault with

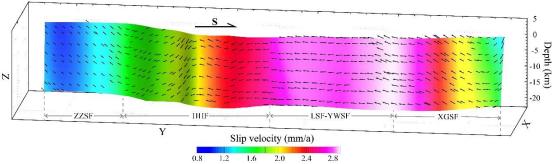


Figure 7. Distribution of the modeled fault slip rates on the F2 fault. View from west to east. The black arrows represent the slip directions. The ratio of the vertical to horizontal scale is 4:1.

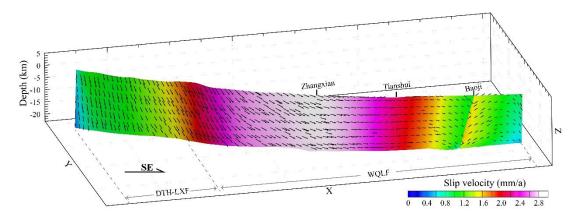


Figure 8. Distribution of the modeled fault slip rates on the F3 fault. View from SW to NE. The black arrows represent the slip directions. The ratio of the vertical to horizontal scale is 4:1.

slip rates ranging from 0.8 to 1.6 mm/a. The Huanghe Fault has a slip rate of 1.6–2.6 mm/a. Its northern segment is an oblique-slip normal fault, whereas its southern segment has <u>almost</u> no dip-slip component. The Luoshan and Yunwushan faults have slip rates ranging from 2.6 to 3.0 mm/a and are dominated by right-lateral strike-slip faulting. The Xiaoguanshan Fault is an oblique-slip reverse fault with slip rates ranging from 3.0 mm/a (northern end) to 1.4 mm/a (southern end).

3.2.3 Slip rate of the F3 fault

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The F3 fault includes the Daotanghe–Linxia and West Qinling faults (FigureFig. 1) and is mainly a uniform left-lateral strike-slip fault, as shown in FigureFig. 8. The western Daotanghe–Linxia Fault is an oblique-slip reverse fault, which has slip rates ranging from 0.8 to 1.8 mm/a. The West Qinling Fault has slip rates varying from 1.8 to 2.8 mm/a, but each partsegment of this fault has slightly different kinematics. The West Qinling Fault is an oblique-slip reverse fault west of Zhangxian, but is dominated by left-lateral strike-slip faulting with a small thrust component in the Zhangxian–Tianshui–Baoji region. The West Qinling Fault is becomes an oblique-slip normal fault only in the vicinity of Baoji.

<u>The</u> kinematics of other faults in the study area are not described in this study. Their horizontal velocities are listed in <u>Figure 10Fig. 9</u>.

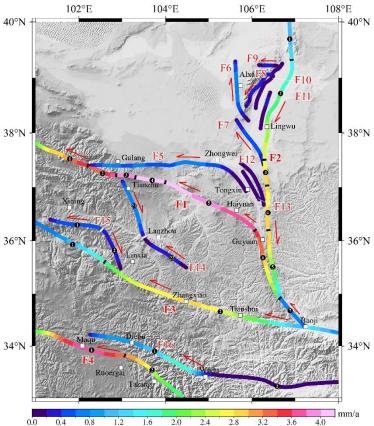


Figure 9. Modeled horizontal fault slip rates and slip senses. The fault names are defined in Fig. 1.

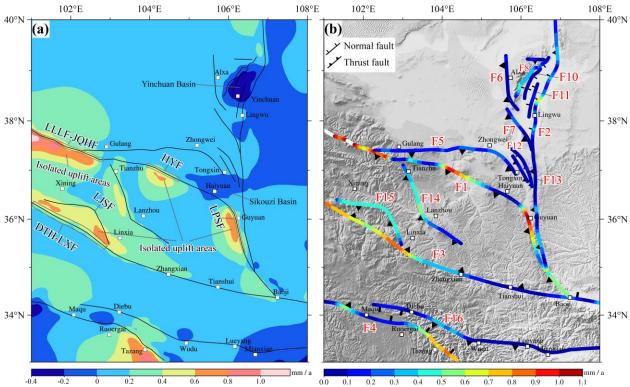


Figure 10. (a) Modeled vertical velocity at the surface. Negative values indicate subsidence, whereas positive values represent uplift. (b) Modeled vertical slip rates on faults at the surface. The fault names are defined in Fig. 1.

3.3 Vertical velocities

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Figure 11a10a shows the distribution of vertical velocities in the study area. In the study areaour model, surface subsidence can be observed only in the Yinchuan Basin west of Huanghe Fault, in the Ordos basin in the east, and in the Sikouzi Basin in the southern Ningxia arc tectonic belt. Most of the subsidence rates range between 0 and 0.2 mm/a, except in the center of the Yinchuan Basin, which exhibits subsidence rates varying from 0.2 to 0.4 mm/a. Based on paleomagnetic studies, the Sikouzi Basin had a subsidence rate of 0.22 mm/a during the Pliocene (Wang et al., 2011), whereas the subsidence rate of the Yinchuan Basin has been 0.32 mm/a since the Middle Pleistocene (Ma et al., 2021). Both values are consistent with those derived from our simulation.

Most other parts of the study area exhibit uplifting, albeit at low rates (generally less than 0.2 mm/a). Most areas with high uplift rates (0.8–1.0 mm/a) are in the Qilian Block such as the Lenglinglong Fault and Jinqianghe Fault, the southern side of the middle Haiyuan Fault, the western side of the Liupanshan segment, and the southern side of the Lajishan Fault (Figure 11a). Areas with highFig. 10a). High vertical fault velocities areslip rates also appear on the F1 and F3 thrust faults that form the NS boundarynorth and south boundaries of the Qilian Block (Figure 11b). TheFig. 10b). These high vertical velocities of the Qilian Blockfault slip rates are inferred to be caused by the tectonic setting. Because of compression from the NE expansion of the TP and SW subducting of the Alxa Block under thrusting the tectonic transition zone of the NETP, the Qilian Block is compressed from two directions (Ye et al., 2015). Therefore, outward thrust stacking occurs on the southern and northern boundaries (F1 and F3 faults) of the Qilian Block.

4 Discussion

4.1 Comparison with previous results

The boundary conditions of our model were derived from the GPS data of Wang and Shen (2020). Figure 11 shows a comparison of the results of our model with the GPS data. The modeled velocity field is consistent in both direction and magnitude with GPS-derived velocity field. In order to further examine the fit between the model results and GPS data, we selected a NE–SW profile that crosses through the study area (Fig. 11, C–C') and projected all GPS-observed values within 50 km of both sides of the profile. Figure 12 shows that the modeled and observed values on either end of the profile (i.e., locations close to the model's boundaries) are almost identical. Although there were differences between the modeled and GPS-observed values, the differences were within the margin of error for the GPS data. Therefore, based on comparisons between the modeled and GPS-observed values in the map and profile, our modeled kinematics agrees well with the GPS data.

Table 3 is a comparison of the modeled slip rates and model-independent geological slip rates compiled from previous studies. From the comparison, we can see that our modeled results are generally consistent with the slip rates obtained by geologic approaches. For example, the modeled horizontal slip rates on the F1 fault (e.g., the Laohushan, Haiyuan, and Liupanshan faults) are similar to the geological slip rates obtained by previous pointwise measurements (Table 3). The modeled slip rates on the F2-3 Luoshan Fault (2.6–3.0 mm/a) are in line with the geological slip rate

(2.2 mm/a). A good agreement between these two kinds of slip rates also exists on the West Qinling Fault in the Zhangxian and Tianshui region (Table 3).

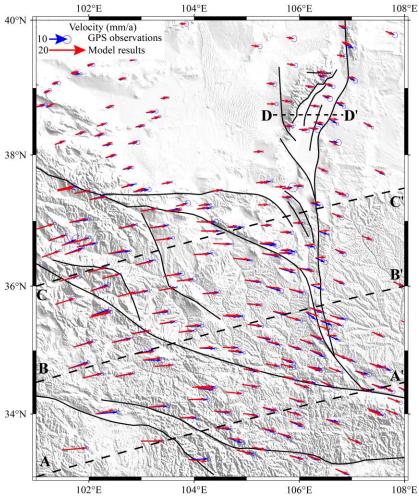


Figure 1211. Comparison of the modeled horizontal velocities and GPS velocities. The red arrows represent the modeled results and the blue arrows are the GPS measurements (Wang et al., and Shen, 2020). The dashed line is the location of the profile in Figure Fig. 123 and Figure Fig. 145.

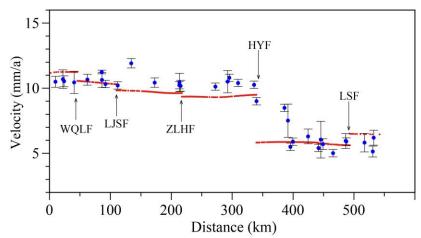


Figure <u>1312</u>. Comparison of the modeled horizontal velocities and GPS velocities along the C-C' profile in <u>FigureFig.</u> <u>112</u>. The red points are model data and blue circles indicate GPS measurements. The fault names are defined in <u>FigureFig.</u> 1.

Table 3. Comparison of model slip rates with geological slip rates

					ical slip rates		
Fault name					References		
LLLE					He et al., 2000, 2010		
					He et al., 2000		
_		0.7-1.0					
		/			He et al., 2000		
LHSF		/	4.0	/	Liu et al., 2018		
HYF	3.6–4.2	0.2-1.0	3.2–4.5	/	Li et al., 2009; Matrau et al., 2019		
LPSF	2.0 - 3.6	0.2 - 1.1	0.7 - 3.0	0.2 – 0.9	Wang, 2018; Wang et al., 2021;		
GG-BJF	0.6 – 0.8	0.5 – 0.6	/	/	/		
ZZSF	- (1.2–1.4)	0.2 - 0.3	/	/	/		
HHF	- (1.6–2.6)	0-0.7	/	0.04-0.24	Lei et al., 2014		
LSF	- (2.6–3.0)	/	- 2.2	/	Min et al., 2003		
YWSF	- (2.6–3.0)	/	/	/	/		
XGSF	- (1.4–3.0)	0-0.4	/	/	/		
DTH-LXF	0.8-1.8	0.5 – 0.8	/	/	/		
WQLF	1 2.0–3.0	0.1-0.9	2.5-2.9	/	Chen et al., 2019		
EKLF	3.2-3.8	0-0.5	4.9	0.25	Li, 2009		
TZF	2.2 - 3.2	0.3 – 0.7	1.4-3.2	0.1-0.3	Ren et al., 2013		
TJSF	0-0.8	0.1-0.3	0.77-0.96	0.1-0.2	X. Li et al., 2017, 2019; X. Li et al., 2017; Zhang et al., 2015		
WHLSF	- (0.6–0.8)	0-0.2	- 0.28	0.11	Lei, 2016		
NSSF	- (0.4–0.6)	0-0.3	- 0.35	0.10	Lei, 2016		
EHLSF	0.2-0.4	0.1 – 0.5	/	0.88	Lei et al., 2016		
	0.2–0.4		/	/	/		
	/		/		Lei et al., 2011		
	/		/		Lei et al., 2008		
	/		/		/		
	(0.6.0.0)		•				
				0.12–0.51	Hou et al., 1999		
			0.5–1.72	/	Song et al., 2006		
			/	/	/		
	, ,		13	0.39	/ Liu et al., 2015		
WD-KXF	0-0.2	0-0.1	1.0	/	Zheng et al., 2016 <u>a</u>		
	LLLF JQHF MMSF LHSF HYF LPSF GG-BJF ZZSF HHF LSF YWSF XGSF DTH-LXF WQLF EKLF TZF TJSF WHLSF NSSF EHLSF ZYGF LHTF YCF QSHF YTSF ZLHF MXSF WLJSF ELJSF ELJSF DB-BLJF	Lateral a	Lateral a Vertical b LLLF 2.8–3.6 0.6–1.3 JQHF 3.2–3.8 0.7–1.0 MMSF 3.8–4.0 / LHSF 4.0–4.2 / HYF 3.6–4.2 0.2–1.0 LPSF 2.0–3.6 0.2–1.1 GG-BJF 0.6–0.8 0.5–0.6 ZZSF -(1.2–1.4) 0.2–0.3 HHF -(1.6–2.6) 0–0.7 LSF -(2.6–3.0) / YWSF -(2.6–3.0) / XGSF -(1.4–3.0) 0–0.4 DTH-LXF 0.8–1.8 0.5–0.8 WQLF 42.0–3.0 0.1–0.9 EKLF 3.2–3.8 0–0.5 TZF 2.2–3.2 0.3–0.7 TJSF 0–0.8 0.1–0.3 WHLSF -(0.6–0.8) 0–0.2 NSSF -(0.4–0.6) 0–0.3 EHLSF 0.2–0.4 0.1–0.5 ZYGF 0.2–0.4 0–0.2 LHTF / 0–0.1 YCF / 0–0.2 YTSF / 0–0.2 ZLHF -(0.6–0.8) 0.2–0.6 MXSF 0.2–0.4 0.1–0.4 WLJSF 0.4–0.6 0.4–0.5 ELJSF / 0–0.2 ZLHF -(0.6–0.8) 0.2–0.6 MXSF 0.2–0.4 0.1–0.4 WLJSF 0.4–0.6 0.4–0.5 ELJSF 0.2–0.4 0.1–0.4	Lateral a Vertical b Lateral a	Lateral a Vertical b Lateral a Vertical b LLLF 2.8-3.6 0.6-1.3 3.9 0.38 JQHF 3.2-3.8 0.7-1.0 4.4 / MMSF 3.8-4.0 / 3.7 / LHSF 4.0-4.2 / 4.0 / HYF 3.6-4.2 0.2-1.0 3.2-4.5 / LPSF 2.0-3.6 0.2-1.1 0.7-3.0 0.2-0.9 GG-BJF 0.6-0.8 0.5-0.6 / / ZZSF -(1.2-1.4) 0.2-0.3 / / LSF -(2.6-3.0) / -2.2 / YWSF -(2.6-3.0) / / / XGSF -(1.4-3.0) 0-0.4 / / DTH-LXF 0.8-1.8 0.5-0.8 / / WQLF 42.0-3.0 0.1-0.9 2.5-2.9 / EKLF 3.2-3.8 0-0.5 4.9 0.25 TZF 2.2-3.2 0.3-0.7 1.4-3.2 0.1-0.3 TJSF 0-0.8 0.1-0.3 0.77-0.96 0.1-0.2 WHLSF -(0.6-0.8) 0-0.2 -0.28 0.11 NSSF -(0.4-0.6) 0-0.3 -0.35 0.10 EHLSF 0.2-0.4 0.1-0.5 / 0.88 ZYGF 0.2-0.4 0.1-0.5 / 0.88 ZYGF 0.2-0.4 0-0.2 / / LHTF / 0-0.1 / 0.18 YCF / 0-0.2 / / YTSF / 0-0.2 / / ZLHF -(0.6-0.8) 0.2-0.6 / 0.12-0.51 MXSF 0.2-0.4 0.1-0.4 0.5-1.72 / WLJSF 0.4-0.6 0.4-0.5 / / DB-BLJF 0.8-1.8 0.1-0.4 1.3 0.39		

^a Positive value indicates left-lateral slip rate. ^b Fault attributes are shown in Figure 11bFig. 10b

4.2 Fault slip rates and seismic hazards

4.2.1 Tianzhu Seismic Gap

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The M_{8.0} Gulang earthquake occurred in 1927 in the northwestern part of the F1 fault, whereas the M_{8.0} Haiyuan earthquake occurred in 1920 on the Haiyuan Fault, (Fig. 1). The Jinqianghe, Maomaoshan, and Laohushan faults, which are in the region between these earthquake zones, participated the locations of these two strong earthquakes, unruptured in neitherthe two earthquakes, are collectively known as the Tianzhu Seismic Gap (TSG, Guo et al., 2019; Y. Li et al., 2016; Figure 14aFig. 13a). Based on the model simulation, the left-lateral strike-slip rates of the Jinqianghe, Maomaoshan, and Laohushan faults were 3.2–3.8, 3.8–4.0, and 4.0–4.2 mm/a, respectively (Table 2, Fig. 13a). Therefore, all three faults have relatively high slip rates compared with the rest of the study area. Based on the slip rates and other fault data, we estimated the earthquake magnitude based on the energy accumulated during the time elapsed time-from the previous event (Purcaru et al., 1978) and recurrence intervals (Shen et al., 2009), as shown in Table 4. The Jinqianghe, Maomaoshan, and Laohushan faults can generate Ms6.9, Ms 7.21, Ms 7.3, and Ms 6.86 earthquakes, with recurrence intervals of 707, 890424, 571, and 11321910 years, respectively. These intervals are like the 1000 year recurrence interval estimated based on geological evidence (Liu Zeng et al., 2007). It has been reported that 675 and 952 years have elapsed since the last time Jingianghe and Maomaoshan faults were last activated ruptured (Gan et al., 2002; Table 4). Therefore, the likelihood these two faults will reactivate in the next few decades is high. For the Laohushan Fault, it is believed that the most recent seismic event inducing earthquake with surface ruptures was the 1888 M6.25 Jingtai earthquake. Because only 133 years have elapsed since this event, the near term-seismic hazard of this fault in the near future is low. However, Although several researchers believe suggested that the TSG experienced could be ruptured thoroughly by a $M \ge 8.0$ earthquake with a recurrence interval of 1000 years, which would involve the simultaneous activation of the Lenglinglong, Jingianghe, Maomaoshan, (Chen, 2014) and Laohushan faults (Chen, 2014). Based on historical seismic records, 925 years have the elapsed sincetime from the most recent M \ge 8\lambda simultaneous rupture event in the TSG (Liu et al., 2018). Therefore, the likelihood that a major earthquake will occur inmay be closed to the recurrence interval (Liu et al., 2018), further work is needed to verify this region assumption, especially on the stress state of the faults. Nevertheless, our results together with the previous studies suggest that the seismic hazard caused by a large earthquake in the TSG is high in the next few decades is high, careful earthquake monitoring should be conducted in this area.

4.2.2 Seismic gap at the southern Liupanshan and Guguan-Baoji faults

Because of the unique tectonic setting of the The Liupanshan and Guguan–Baoji faults, this region is simultaneously are jointly affected by three sources of tectonic stress (Figure 14binteracting blocks with contrasting velocity fields (Fig. 13b). First, the SE movement of the Qilian Block horizontally compresses this region against the stable Ordos Block to the east and causes strong thrusting activity (Figure motion (Fig. 6a). Second, the Liupanshan Fault zone—at, which is adjacent to the SE end of the Haiyuan Fault—and, accommodates the displacements shortening caused by the shortening of the Liupanshan Fault zone. Third, our simulations modeled results show that the Yunwushan–Xiaoguanshan Fault has a significant right-lateral strike-slip component (Figure Fig. 7), which contributes to the

accumulation of right-lateral shear strain in the Liupanshan and Guguan–Baoji fault zones (Du et al., 2018). Based on these three sourcesthe analysis of tectonic stressthe velocity field in the region, the Liupanshan and Guguan–Baoji faults are prime locationslocation for stresselastic strain accumulation. The distribution of the velocities of the faults are also indicative of stress accumulation in this region (FigureFig. 7). The northern segment of the Liupanshan Fault has slip rates of 3.2–3.6 mm/a, which suddenlydramatically decrease to 2.5 mm/a in the middle and southern segments of the fault. In addition, the slip rate of the Guguan–Baoji Fault is only 0.7 mm/a. The northern part of the Yunwushan–Xiaoguanshan Fault has slip rates of 2.8–3.0 mm/a, which decrease to 1.5 mm/a in the southern part (Figure 14bFig. 13b). These changes in the slip rate indicate that the middle–southern segments of the Liupanshan and Guguan–Baoji

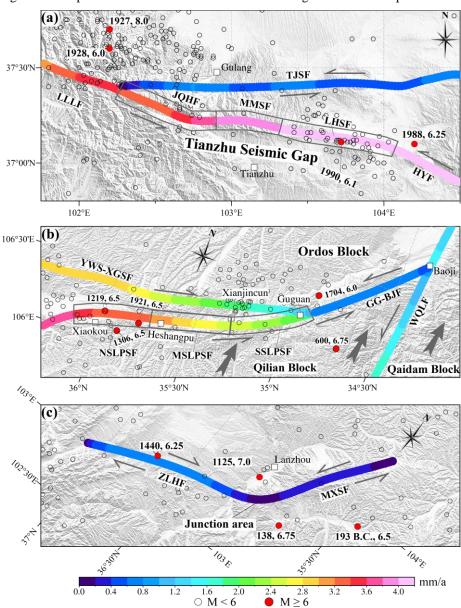


Figure 13. Modeled horizontal fault slip rates and distribution of historical earthquakes in (a) the Tianzhu Seismic Gap, (b) the intersection area of the Liupanshan, Guguan-Baoji, and Yunwushan-Xiaoguanshan faults and (c) the junction area of the Maxianshan and Zhuanglanghe faults. The gray arrows in (b) represent the movements of the Qilian and Qaidam blocks and NSLPSF, MSLPSF, and SSLPSF are the northern, middle, and southern segments of the Liupanshan Fault, respectively.

Table 4. Earthquake magnitude and recurrence interval of each fault based on the energy accumulated during the elapsed time since the last remarkable earthquake

	1								
Fault name	$V_1(mm/a)$	$V_2(mm/a)$	L_1 (km)	$L_2(km)$	μ (Gpa)	t	S (m)	$M_{\rm S}$	T (a)
JQHF	3.5	/	34	20	34.5	675	1.5	7.1	424
MMSF	3.9	/	51	20	34.5	952	2.2	7.3	571
LHSF	4.1	2.5	70	20	34.5	133	3.1	6.6	1910
MSLPSF, SSLPSF	2.5	/	80	23	34.5	570	3.5	7.2	1397
GG-BJF	0.7	/	70	23	34.5	1400	3.1	7.1	4365

 V_1 is the modeled average slip rate of the fault in this study; V_2 is the aseismic creep rate of the fault (Y. Li, et al., 2021); L_1 is the length of the fault (Xu et al., 2016); L_2 is the depth of the seismogenic, which refers to the locking depth (Y. Li, et al., 2017, 2021); μ is the shear modulus of the rocks (Aki et al., 2002); t is the time that has elapsed since the most recent remarkable earthquake (Gan et al., 2002; Shi et al., 2013, 2014; Wang et al., 2001); S is the largest maximum coseismic displacement, calculated using the method of Gan et al. (2002); M_S is the earthquake magnitude corresponding to the energy accumulated by the fault between recurrences (Purcaru et al., 1978); T is the recurrence interval of the fault, where $T = S/(V_1-V_2)$ (Shen et al., 2009). The fault names are defined in Fig.ure 1 and Fig.ure 134.

faults have high slip rate deficits, implying this region accumulates strain—very rapidly. However, in terms of seismic activity, only the northern part of the Liupanshan Fault has a history of major earthquakes including an M_2 earthquake in 1219, M_2 6.5 earthquake in 1306, and M_2 6.5 earthquake in 1921 (Figure 14bFig. 13b). Earthquakes stronger than M_2 6.0 have not been recorded in the middle—southern parts of Liupanshan Fault. Their seismic activity mainly manifests as small and sparse earthquakes and the most recent remarkable activation was recorded $500\sim570$ years ago (Shi et al., 2014). Minor earthquakes related to the Guguan—Baoji Fault are scarce and the only notable earthquakes that have occurred near this fault are an M_2 6.0 earthquake in 1704 and the 600 AD Qinlong M_2 6.75 earthquake (Shi et al., 2013). It has been estimated that ~1400 years have elapsed since its the last activation (Xue, 2014). M_2 7 earthquake.

Base on the above analysis, we suggest that the southern segments of the Liupanshan and Guguan–Baoji faults are in prime locations for stress/strain accumulation and constitute a seismic gap on a majorat the end of the large-scale Haiyuan strike-slip fault. Furthermore, zone. Since this region has a history of strong earthquakes. Hence, it is anecessary to assess the seismic hazard zone for strong earthquakesand its urgency in this region. Based on the fault slip rates obtained from our model and fault data in the literature, we estimated that the energy accumulated byon the middle–southern Liupanshan and Guguan–Baoji faults during the elapsed time is sufficient to generate Ms.7.2 and Ms 7.1 earthquakes, with recurrence intervals of 14001397 and 44294365 years, respectively (Table 4). Because the next event is not likely to occur for a long time Obviously, the elapsed time on the middle–southern Liupanshan (570 years) and Guguan–Baoji faults (1400 years) (see the column "t" in Table 4) are much shorter than their typical recurrence intervals. Therefore, we infer that the middle-southern Liupanshan fault and the Guguan-Baoji fault are most likely in a state of stress accumulation. Therefore, and the likelihood of a majorlarge earthquake on these fault segments in the next few decades is thought to be low in this region.

4.2.3 Maxianshan-Zhanglanghe fault zone

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The Maxianshan Fault <u>innear</u> Lanzhou <u>city</u> is a large Holocene <u>reverse</u> strike-slip fault. <u>It is with a component of thrusting and acts as</u> an important earthquake-controlling fault that affects and constrains the seismicity of this region

(Yuan et al., 2003). Different left-lateral strike-slip rates have been reported for this fault—3.73 mm/a (Yuan et al., 20022002a), 0.5–1.72 mm/a (Song et al., 2006), and 0.93 mm/a (Liang et al., 2008). These discrepancies in fault slip rate may be attributed to the loess that covers the extension of the fault, which obscures the fault traces in many segments and makes it difficult to track its activity. The simulations performed modeled results in this study indicate that the left-lateral strike-slip rates of the Maxianshan Fault range from 0.2 to 0.4 mm/a and that the vertical slip rates vary from 0.1 to 0.4 mm/a (Figure 14cFig. 13c, Table 3). Therefore, the left-lateral strike-slip motionsrates of the Maxianshan Fault may not be as intenselarge as previously thought, but they have a relatively large thrust component. The Zhanglanghe Fault is predominantly a right-lateral strike-slip fault with slip rates ranging from 0.6 to 0.8 mm/a (Figure 14eFig. 13c, Table 3). These slip rates are significantly greater than the left-lateral strike-slip rates of the Maxianshan Fault. Note that the slip rate on the junction between the Maxianshan fault and Zhuanglanghe faultsfault is a locked fault zone with a slip rate of almost zero. Locked fault zones It can be inferred that the junction area would accumulate high concentrations of stress. An earthquake will occur when this stress exceeds the ultimate strength of the rocks in this segment under the continuous eastward movement of the Qilian Block. Some have suggested that the 1125 Lanzhou M_7.0 earthquake occurred in such a tectonic setting (He et al., 1997; FigureFig. 13c). Given that the recurrence interval of this region is 2250-3590 years and the last event was only 896 years ago (Liang et al., 2008), the near-term risk of a majorlarge earthquake in this region is low-because. Therefore, we speculate that the next event is not expected to occur for a long time. The locked fault zone jointly controlled by junction area of the Maxianshan fault and Zhuanglanghe faults represents a tectonic setting conducive for strong quakes and fault is currently in a state of stress accumulation.

4.2.4 Isolated uplift areas and earthquakes

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As mentioned above, we considered that earthquakes are less likely to occur on the Laohushan, Liupanshan and Haiyuan faults in the short term from the perspective of the earthquake recurrence cycle and the elapsed from the previous earthquake. However, the Haiyuan, Liupanshan, Lajishan and Daotanghe-Linxia faults are all located near the isolated rapid uplift areas of Qilian block (Fig. 10a). Many studies have also found that low-velocity bodies are widely distributed in the middle-lower crust of the Qilian block (Bao et al., 2013; Wang et al., 2018; Ye et al., 2016). The spatial coupling of active faults, isolated uplift areas and low-velocity bodies is highly similar to the seismogenic conditions elaborated by the "seismic source cavity" model recently proposed by Zeng et al. (2021). That is, during the rapid uplift of the isolated areas (Fig. 10a), the low-velocity bodies in the middle-lower crust easily intruded into the weak space of the crust under the action of differential pressure to form a "seismic source cavity". If the isolated uplift areas keep to rise, the "seismic source cavity" may rise to the shallow part of the crust to intersect with brittle faults, causing strong earthquakes (Yang et al., 2009; Zeng et al., 2021). Therefore, in addition to the Jinqianghe and Maomaoshan faults mentioned above, the Haiyuan fault, Liupanshan fault, Lajishan fault and the Daotanghe-Linxia fault also have favorable structural conditions for strong earthquakes although some areas have not experienced in history.

4.3 Implication for deformation block models mechanism of NETP

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The deformation of NETP is the result of the combined action of block rotation, faulting, and the intrablock straining (Meade and Loveless, 2009). We analyzed four velocity profiles to compare the contributions of block rotation, faulting, and intrablock straining to the total deformation of NETP (Fig. 14). It is noted that the rigid displacements caused by block rotation were calculated according to the Euler pole locations and rotation rates with respect to the Eurasia plate (Wang et al., 2017; Y. Li et al., 2022), as shown in Fig. 14 a–d. The velocity gradient caused by block rotation accounts for more than 80% of that on the profiles. Obviously, the block rotation should be the primary mechanism for the deformation of the NETP, which is similar to the southeastern Tibet (Z. Zhang et al., 2013). However, the intrablock straining of Bayan Har and Qaidam blocks contribute approximately 4 mm/a and 3 mm/a shortening in profiles of AA', BB' (Fig. 14a–b). The Qilian block also has a contribution of 2 mm/a shortening in profile BB' but decreases to about 1mm/a in profile CC' (Fig. 14b–c). Therefore, the intrablock straining is still significant for regional deformation. The boundary faults of the blocks, such as the East Kunlun fault, Haiyuan fault, West Qinling fault, also play an important role in regulating the deformation differences between blocks.

The D–D' profile shows that the tectonic deformations of the Yinchuan Basin structural belt slightly differ from those in other profiles. The NE expansion of the TP leads to near-N–S compression on the Helanshan–Yinchuan Basin structural belt (Yang, 2018), (Yang, 2018), which causes the Yinchuan Basinit to move eastwards faster than the Helanshan structural belt and Alxa Block. This manifests as an eastward extension in the Yinchuan Basin. The crustal deformations caused by this process are accommodated by the right-lateral strike-slip of Huanghe Fault (FigureFig. 14d).

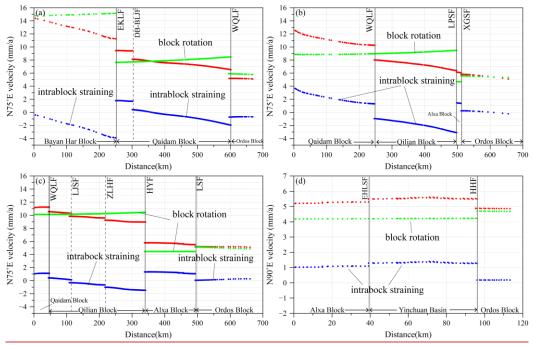


Figure 14. Modeled velocity profiles across the study area with orientation of profiles. The profiles in (a)–(d) correspond to the AA', BB', CC', and DD' in Fig. 11, respectively. The red dots indicate the components along the profiles of the node motion velocity within 2 km on both sides of the profile. The green dots represent the velocity component along the profiles due to plate rotation. The blue dots indicate the differences between the red and green dots. Fault names are defined in Fig. 1.

5 Conclusions

In this study, a detailed 3D geomechanical—numerical model of the NETP was constructed based on geophysical, geodetic, and geological data. This model accounts for physical D fault geometries, variational rock properties, gravity fields, fault friction coefficients, a reasonable initial crustal stressesstress, and boundary conditions gravity. Special attention has been paid to the evaluation of fault friction coefficients and initial stress field parameters, which are important for kinematics simulations. To obtain the fault friction coefficients, simulations were performed using a series of friction coefficients. The results of these simulations were then compared to GPS observations. Friction coefficients with the lowest global fitting error were used in the final model. The initial stress field was characterized using the crustal model of Sheorey (1994) and the procedures of Hergert (2009). The initial stresses obtained based on this procedure agree well with the stress fields measured across the globe. Based on the numerical analysis of our model, weto ensure that the model is consistent with the real geological conditions as much as possible. After that, we extracted particular data from the model and obtained the horizontal and vertical crustal velocities of the study area as well as the horizontal and vertical velocitiesslip rates of the major faults. The results were then validated against independent geodetic, geological, and paleomagnetic datacan be mutually confirmed with the conclusions obtained by geodesy, geology, paleomagnetism, etc.

Based on the analysis of the kinematics of the study area's major faults, the we suggest that the Jinqianghe—Maomaoshan Fault will probably cause a Ms 7.1 ~ 7.3 earthquake in the following decades due to its relatively high slip rates with an elapsed time close to the recurrence interval. In contrast, the Laohushan and middle—southern Liupanshan faults as well as the Guguan—Baoji and loeked fault zones at the junction area of the Maxianshan and Zhuanglanghe faults are inferred to have a low seismic hazard zones for strong earthquakes. However, the likelihoodin the near future on account of a major earthquake at these faults is low in thetheir very short term because they are eurrently in the elapsed time, although stress accumulation state. In contrast, the Jinqianghe Maomaoshan Fault will probably cause a M7.0 earthquake in the following decades is easily accumulated in these areas. The simulation model also provided information on the deformation modes mechanism of the NETP. Because of velocity differences between the opposing sides of the Haiyuan, West Qinling, and East Kunlun faults, as well as the relative stability of the Alxa and Ordos blocks, the NE expansion of the TP has caused the fault-separated Qilian, Qaidam, and Bayan Har blocks to extrude in the SEE direction and rotate in the clockwise direction. The crustal deformations at the NETP are predominantly continuous in the Bayan Har and Qaidam blocks and predominantly block like in the Qilian BlockThe block rotation is the primary mechanism for the deformation of the NETP even though the intrablock straining and faulting are non-negligible.

Data Availability

The GPS data displayed in Figure Fig. 4 and Figure 12 Fig. 11 are available through Wang and Shen (2020). The fault traces were obtained from Xu et al. (2016). The CRUST1.0 was obtained from Laske et al. (2013).

Author contribution

LL and XL contributed to the model building. LL carried out the analysis, wrote the paper, and prepared the figures. FY, LP and JT reviewed and edited the paper.

Competing interests

The authors have no competing interests to declare.

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Acknowledgments

This research was funded by the Ningxia Natural Science Foundation of Ningxia Province (gGrant numbers: 2020AAC03445, 2021AAC05022 and 2021AAC03441). Some figures were plotted using The Generic Mapping Tools (https://www.generic-mapping-tools.org/). Slip rates on fault surfaces were calculated by the software GeoStress (Stromeyer et al., 2020).

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