Numerical Simulation of Contemporary Kinematics at the Northeastern Tibetan Plateau and its implications for seismic hazard assessment

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Abstract. The slip rates of active faults <u>atin</u> the northeastern Tibetan Plateau (NETP) <u>should be clarifiedrequire</u> <u>clarification</u> to understand the lateral expansion of the Tibetan Plateau and assess the seismic hazards in this region. To obtain the continuous slip rates of active faults at the NETP, we constructed a three-dimensional (<u>3D</u>) geomechanics-numerical model which includes a complex 3D fault system. The model also accounts for the physical rock properties, gravity fields, fault friction coefficients, initial stress, and boundary conditions. Then, we

15 rock properties, gravity fields, fault friction coefficients, initial stress, and boundary conditions. Then, we presentedpresent the long-term kinematics of NETP according tobased on the horizontal and vertical velocities and fault slip rates acquired from the model. The fault kinematic characteristics indicate that the Laohushan, middle– southern Liupanshan, and Guguan–Baoji faults, as well as the junction area of the Maxianshan and Zhuanglanghe faults, are potential hazard areas for strong earthquakes. However, as these faults are currently in the stress accumulation stage, they are unlikely to cause a strong earthquake in the short term. In contrast, it is likely that the Jinqiangshan–Maomaoshan fault will generate a M_s 7.1–7.3 earthquake in the coming decades. In addition, the velocity profiles across the NETP imply that the plate rotation is the primary mechanism for the deformation mechanism of the NETP even though the intrablock straining and faulting are non-negligible.

1 Introduction

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The northeastern Tibetan Plateau (NETP) is the growth front of the Tibetan Plateau (TP). Modern geomorphology and tectonic features of the NETP are inferredthought to be formed due toby the expansion of the TP toward its periphery, which has been ongoing since the initial collision of the Indian and Eurasian plates collided ((Achache et al., 1984; Patriat and Achache 1984; P. Zhang et al., 2013, 2014). Having experienced the strong Cenozoic deformation, crust ofin this area developshas developed a complex fault system with several large and deep faults, such as the generalized Haiyuan fault (F1), West Ordos fault (F2), West Qinling fault (F3), and East Kunlun fault (F4), that divide the NETP into the Alxa, Ordos, Qilian, Qaidam, and Bayan Har blocks (Zhang et al., 2003; Fig.1). These faults are characterized by extremely intense tectonic movements and seismic activitiesactivity (Zhang, 1999; Zheng et al., 2016b). At least 5 earthquakes with magnitudes of ≥ 8, such as the 1654 M 8.0 Tianshui, 1739 M 8.0 Pingluo,

1879 M 8.0 Wudu, 1920 M 8.0 Haiyuan, and 1927 M 8.0 Gulang earthquakes, <u>have_occurred in this area and caused</u> huge <u>losslosses</u> of life and property <u>in history-(Fig. 1)</u>. <u>SinceBecause</u> the generation and magnitude of an earthquake <u>isare</u> closely related to fault activity, long-term fault slip rate plays a key role in medium- and long-term seismic hazard assessment (Ding et al., 1993; Xu et al., 2018). For example, combined with coseismic displacements, long-term fault slip rates can be used to calculate <u>the</u> earthquake recurrence interval (Shen et al., 2009) and assess the magnitudes of potential earthquakes (Bai et al., 2018; Hergert and Heidbach, 2010). Moreover, the spatially continuous fault slip

40 rates, which are lack in the that NETP, lacks can also be used to reconstruct the tectonic evolution of this area and provide important insights into the lateral expansion pattern and deformation mechanisms of the TP (Royden et al., 1997; Tapponnier et al., 1982; Zhang et al., 2004).

Although there has been extensive research on the fault slip rates in the NETP-by using geologic (Chen et al., 2019; Li et al., 2009; Li et al., 2018; Matrau et al., 2019; Wang et al., 2021;X. Li et al., 2017) or geodetic (Hao et al., 2021; Li, Pierce, et al., 2021; X. Li et al., 2019) approaches, a systematic mismatch is typically found between the slip rates

- calculated from geological records and <u>thatthose</u> obtained from geodetic inversion, <u>dueowing</u> to the limited assumptions behind these two methods. For example, the geological slip rates only represent the activities of one fault branch <u>that</u> measured in a fault zone, which <u>is</u>-always <u>consist</u> of several branches. They are usually lower than the geodetic slip rates <u>on the fault</u> as a whole if a rigid block assumption is adopted in the geodetic inversion process
- 50 (Shen et al., 2009). However, several crustal deformation studies conducted in TP <u>have</u> demonstrated that the internal block deformation in the NETP cannot be ignored (Royden et al., 1997; Zhang et al., 2004; Y. Li et al., 2017, 2021). Numerical modeling provides a powerful tool to study thefor studying large-scale crustal kinematics (Hergert and Heidbach, 2010; Hergert et al., 2011) as well as thea comprehensive three-dimensional (3D) view of fault activities with a spatially continuous distribution. High efficiency and accuracy have made the numerical modeling a widespread
- 55 technology in the field of geosciences, especially for the study of kinematics and dynamics of the NETP (Pang et al., 2019a, b; Sun et al., 2018, 2019; Zhu et al., 2018; Xiao and He, 2015). However, all-these previous numerical models arehave been either two-dimensional (2D) or three dimensional (3D) with extremely simplified fault planes. To our knowledge, so far-there is nonot currently a 3D geomechanical model that take intoconsiders the complex 3D fault system in the NETP. Therefore, detailed kinematics of the crust and faults in the NETP still remainsremain unclear.
- In this study, instead of a simple conceptual model, a comprehensive 3D geomechanical model of the NETP was constructed with detailed complex 3D fault geometries, heterogeneous rock properties, and reasonable initial crustal stress-is constructed. After calibrated bycalibration with model-independent observations, the results of the geomechannicalgeomechanical model, such as the horizontal crustal velocities, and spatially continuous slip rates of major faults, arewere presented. Based on these results, we summarized the long-term crustal deformation characteristics in the NETP. Finally, we assessed the seismic hazards of major faults in the study area, and suggested that the Jinqiangshan–Maomaoshan fault has the potential for an M_s 7.1–7.3 earthquake in the coming decades.

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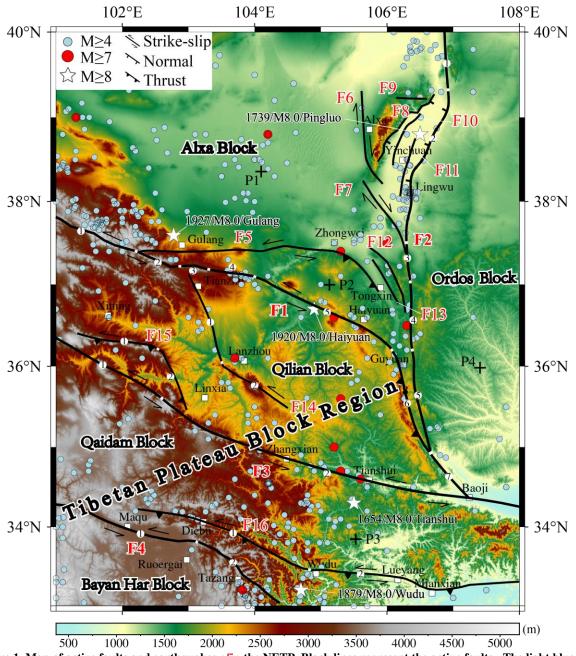


Figure 1. Map of active faults and earthquakes ofin the NETP. Black lines represent the active faults. The light blue, and red dots and the white pentagramsstars represent earthquakes from 1831 BC to 2017 AD from the National Earthquake Data Center (http://data.earthquake.cn). Black crosses (P1-P4) indicate the locations of four test sites for the comparison with the numerical model shown in Fig. 3b. Faults discussed in the text are labeled as followed: F1-1 = LLLF = Lenglongling fault; F1-2 = JQHF = Jinqinaghe fault; F1-3 = MMSF = Maomaoshan fault; F1-4 = LHSF = Laohushan fault; F1-5 = HYF = Haiyuan fault. F1-6 = LPSF = Liupanshan fault; F1-7=GG-BJF=Guguan-Baoji fault; F2-1 = ZZSF = Zhuozishan fault; F2-2 = HHF = Huanghe fault; F2-3 = LSF = Luoshan fault; F2-4 = YWSF = Yunwushan fault; F2-5 = XGSF = Xiaoguanshan fault; F3-1 = DTH-LXF = Daotanghe–Linxia fault; F3-2 = WQLF = West Qinling fault. F4-1 = EKLF = Eastern Kunlun fault; F4-2 = TZF = Tazang fault; F5 = TJSF = Tianjingshan fault; F6 = WHLSF = West Helanshan fault; F7 = NSSF = Niushoushan fault; F12 = YTSF = Yantongshan fault; F13 = QSHF = Qingshuihe fault; F14-1 = ZLSF = Zhuanglanghe fault; F14-2 = MXSF=Maxianshan fault. F15-1 = WLJSF = West Lajishan fault; F15-2 = ELJSF = East Lajishan fault; F16-1 = DB-BLJF = Diebu–Bailongjiang fault; and F16-2 = WD-KXF = Wudu–Kangxian fault.

2 Model concept and input

2.1 Model geometry

85 The proposed 3D geomechanicsgeomechanical model of this work is a rectangular cartesian 3D block with an E–W length of 654 km (101°E–108°E), N–S length of 777 km (33°N–40°N), and thickness of ~80 km. The topography of the model's surface is based on GTOPO30 elevation data, which hashave a resolution of 30 arcseconds (about 900m), approximately 900 m). The model comprises consists of four layers: the upper crust, middle crust, lower crust, and upper mantle, from top to bottom. The geometric data of the layer interfaces were derived from CRUST1.0 (Laske et al., 2013).

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Based on their depth, the faults of the model can be categorized into lithospheric and crustal faults. Lithospheric faults (i.e., F1, F2, F3, and F4) cut through the Moho and reach the bottom of the model (Zhan et al., 2005; B. Liu et al., 2017; Zhao et al., 2015; Fig. 2a, b; Table 1). All other faults are crustal faults that terminate in the upper, middle, or lower crust (Yuan et al., 2002b, 2003; Lease et al., 2012; Meng et al., 2012; B. Liu et al., 2017; Wu et al., 2020).

95 The fault traces arewere modified from Xu et al. (2016), and the attitudes of these faults arewere summarized from previously published data, including surface fault surveys and deep seismic profiles (Table 1). In the NETP, many geophysical investigations found that low-velocity bodies exist widely-in the middle-lower crust and deformations in the upper crust are not coupled to those in the middle-lower crust (Bao et al., 2013; Wang et al., 2018; Ye et al., 2016). Therefore, we introduced a contact surface between the upper and middle crusts into the model and account treat it as 100 a detachmentdecollement layer that makemakes the upper crust decouple from the middle crust and allowallows the upper crust slidingto slide freely along the contact surface according tobased on the stress conditions.

The model was meshed using tetrahedron elements. The element size iswas 1-2 km near the faults and increases increased to ~10 km at the model boundary. The model totally contained a total of 8,463,583 elements (Fig. 2a).

105 2.2 Rock properties

In order to To obtain the time-independent contemporary background crustal stress of the NETP, we assumed that the rock rheology in the model iswas linear elasticity, consistent with the observations that the large-scale continental crust always exhibits elastic-brittle behavior rather than elastic-viscous behavior (Armijo et al., 2004: Hubert-Ferrari et al., 2003). The model was divided into three major tectonic units—the Alxa-block, the Ordos-block, and the-TP

- 110 block region regions. The partportion of the TP block region that located in the study area comprises consisted of the Qilian, Qaidam, and Bayan Har blocks. The rock properties of each block containincluded the elastic parameters (i.e. the Young's modulus, density, and Poisson's ratio) of the upper, middle, and lower crust, as well as those of the upper mantle (Fig. 2a). The density and Poisson's ratio were derived from CRUST1.0 (Laske et al., 2013). The adopted Young's modulus adopted in our model is was static and was converted from the dynamic elastic modulus using the
- empirical equation of Brotons et al. (2016), which was calculated based on the P-wave velocities, S-wave velocities, 115 and densities derived from CRUST1.0. The elastic parameters used in the model are listed in Table 2.

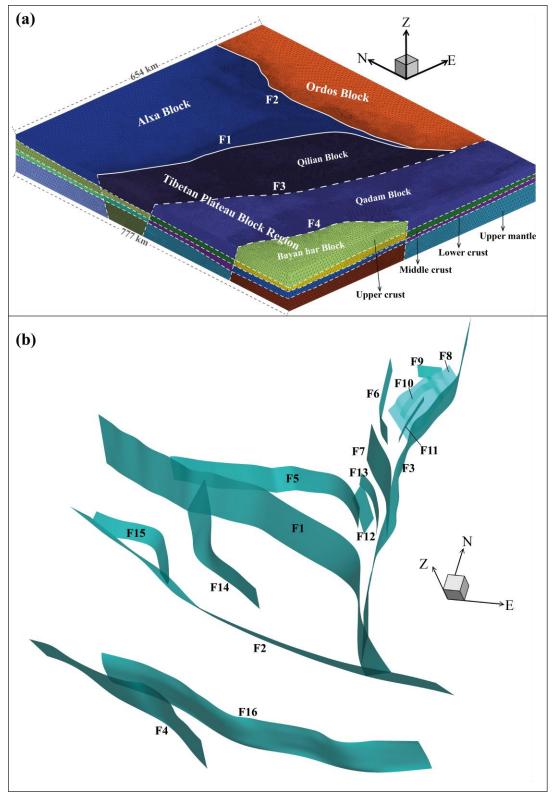


Figure 2. Model geometry and fault system. (a) Distribution of the rock types employed <u>forin</u> the model. (b) Cyan surfaces indicate the faults implemented in the model as frictional contact surfaces. Fault names can be found in Fig. 1.

	Fault name	Strike	Dip direction	Dip (°)	Reference
F1	/	NWW-SSE	SW	70	RGAFSAO, 1988
F2-1	ZZSF	N-S	W	70	Gao, 2020
F2-2	HHF	N-S	W	70	Bao et al., 2019
F2-3	LSF	N-S	W	80	Wang et al., 2013
F2-4	YWSF	N-S	W	70	NIGS, 2017
F2-5	XGSF	N-S	W	70	NIGS, 2017
F3-1	DTH-LXF		NIE	-	Zhou et al., 2009
F3-2	WQLF	NWW-SSE	NE	70	Li, 2005
F4-1 F4-2	EKLF TZF	NW-SE	NE	75	Z. Liu et al., 2017 J. Li et al., 2019
D 5	East TJSF	NW-SE	SW	70	RGAFSAO, 1988
F5	West TJSF	E-W	S	70	RGAFSAO, 1988
F6	WHLSF	N-S	W	80	Lei, 2015
F7	NSSF	NW-SE	SW	70	RGAFSAO, 1988
F8	EHLSF	NE-SW	SE	60	Du, 2010
F9	ZYGF	E-W	S	60	NIGS, 2017
F10	LHTF	NNE-SSW	SE	70	NIGS, 2017
F11	YCF	NNE-SSW	NW	70	NIGS, 2017
F12	YTSF	NW-SE	SW	65	NIGS, 2017
F13	QSHF	NW-SE	SW	45	Tian et al., 2020
F14-1	ZLHF	NNW-SSE	SW	45	Xu et al., 2016
F14-2	MXSF	NW-SE	SW	80	Hou et al., 1999
F15	LJSF	NWW-SSE	SW	50	Yuan et al., 2005
F16-1	DB-BLJF	NW-SE	SW	70	Yuan et al., 2007
F16-2	WD-KXF	E-W	SW	70	Jia et al., 2012

Table 1. Geometric parameters of faults in the model

The detailed fault names are defined in Fig. 1.

Table 2. Rock properties of the finite element model

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	Alxa Block			O	Ordos Block			Tibetan Plateau Block			
	E (Gpa)	ρ (g/cm ³)	ν	E (Gpa)	ρ (g/cm ³)	ν	E (Gpa)	ρ (g/cm ³)	ν		
Upper crust	77.4	0.244	2.74	77.4	0.244	2.74	76.8	0.243	2.74		
Middle crust	84.2	0.247	2.78	84.2	0.247	2.78	84.5	0.246	2.78		
Lower crust	113.0	0.259	2.95	113.0	0.259	2.95	110.0	0.257	2.93		
Upper mantle	194.0	0.278	3.39	191.0	0.278	3.37	187.0	0.278	3.36		

E, ρ , and v are <u>the Young's modulus</u>, density, and Poison's ratio, respectively.

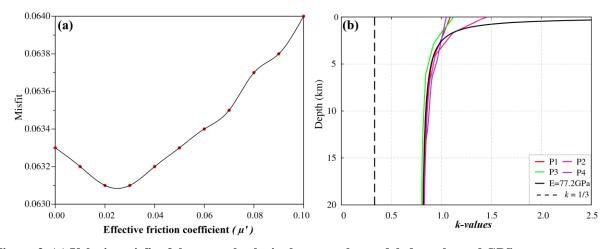


Figure 3. (a) Velocity misfit of the crustal velocity between the modeled results and GPS measurements as
a function of the effective friction coefficient. The optimal friction coefficient was determined to be 0.02.
(b) Depth profiles of the initial k-values at four test sites indicated in Fig. 1. The solid black line shows the stress state based on Equation (3), which was used as a reference stress state. For comparison, the low k-value based on the uniaxial strain state is also shown (dashed black line).

2.3 Friction coefficient

130 In our model, frictional faults were considered to obeyobeyed the Mohr–Coulomb friction law:

$$\sigma_s = C_0 + \mu \cdot (\sigma_n - P_f) = C_0 + \mu' \cdot \sigma_n, \tag{1}$$

where σ_s is the shear stress on the fault surface at time of rupture, C_0 is the cohesion, μ is the coefficient of friction, σ_n is the normal stress on the fault surface, P_f is the pore pressure, and μ' is the effective coefficient of friction of the fault surface when accounting for the pore pressure. The cohesion C_0 of the rocks was assumed to be negligible (Jamison 135 et al., 1980). The friction coefficient of the fault surface is important to the kinematics of a fault, but it is complex in a fault and varies in time and space. The exact magnitude of the friction coefficient can be affected by various external factors including fluid, temperature, stress states, and fault slip rate (Zhu et al., 2009). Therefore, it is challenging to obtain the precise friction coefficient of a fault. However, the results of many studies showed that large faults generally have low effective friction coefficients (Wang, 2021). For instance, the Haiyuan Fault has friction coefficients as low 140 as 0.05 (He et al., 2013), and faults on the eastern margin of the TP have friction coefficients as low as 0.02 (Li et al., 2015; Li, Hergert, et al., 2021). Simulations were performed with a series of friction coefficients (0-0.1), and the results were compared with GPS observations (Cianetti et al., 2001). The results showed that setting a friction coefficient of 0.02 for all faults yields the smallest fitting error (Fig. 3a). To minimize the fitting error, localized adjustments were made for the friction coefficients of thefaults F1 and F3-faults, which are large strike-slip faults. The 145 final friction coefficients of F1, F3, and all other faults were 0.01, 0.1, and 0.02, respectively, with a fitting error of

2.4 Initial stress state

0.0536.

The <u>initial</u> crustal<u>initial</u> stress affects the state of stress acting on a fault, which further controls the <u>kinematickinematics</u> of the fault via the Mohr–Coulomb friction law. Therefore, the selection of appropriate initial

150 stress is important when studying fault slip rates based on geomechanicsgeomechanical models. The initial stress state that is most commonly employed in previous numerical modeling studies of the NETP is the uniaxial strain reference state (Zhu et al., 2016), which is based on the boundary condition that no elongation occurs in the horizontal direction, and the strain only occurs in the vertical direction. In this stress state, the ratio (k) of mean horizontal stress to vertical stress is only dependent on the Poisson's ratio:

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$$k = \frac{(S_H + S_h)}{2S_V} = \frac{v}{1 - v},$$
 (2)

where S_H , S_h , and S_V are the maximum horizontal, minimum horizontal, and vertical stress, respectively, and v is Poisson's ratio. For the typical v-value of 0.25, Equation (2) gives k = 1/3, which implies that the vertical stress acting on the rock mass far <u>exceedexceeds</u> the horizontal stress, and that the crust is always in a normal faulting or extensional stress regime. However, this assumption contradicts the thrust and strike-slip stress regimes common in the crust. Furthermore, *k*-values obtained globally from *in situ* measurements always-greatly exceed 1/3, even in extensional tectonic environments (Hergert and Heidbach, 2011).

Based on a spherical shell model, Sheorey (1994) proposed a method for the estimation of estimating the initial crustal stress, which accounts for the curvature of the Earth, the properties of crustal and mantle materials, temperature fields, and other thermally dependent properties, as shown in Equation (3):

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$$k = 0.25 + 7E \cdot \left(0.001 + \frac{1}{z}\right),\tag{3}$$

Where where *E* is the Young's modulus (GPa); and *z* is the depth (m). Because the *k*-values predicted by this method are-generally consistent with those obtained from the Continental Deep Drilling Program (Hergert and Heidbach, 2011), Equation (3) has been widely used in numerical modeling studies worldwide (Ahlers et al., 2021; Buchmann et al., 2007; Rajabi et al., 2017; Reiter et al., 2014; Hergert and Heidbach, 2011; X. Li et al., 2022). In this study, we used Equation (3) to calculate the initial stress state for our model. The exact procedure for obtaining the initial stress proposed by Sheorey (1994) has been described previously by Hergert (2009) in detail. Figure 3b shows that the modeled initial stress is in-good agreement with the theoretical result given by Equation (3).

2.5 Kinematic boundary conditions

The lateral boundary conditions of our model were constrained by the GPS velocity field data of Wang and Shen
(2020) and were-assumed to be constant along depth (Wang et al., 2008). The top surface of the model was configured as a free boundary, whereas the bottom surface slid freely in the horizontal direction, with a vertical velocity of 0. The detailed boundary conditions are shown in Fig. 4. For the calculation, we used the finite-element software AbaqusTM because <u>of</u> its powerful nonlinear processing capabilities. The model time <u>iswas</u> set as 500 ka, <u>which isas</u> required to generate a proper contemporary state of stress₁ and deformation until the accumulated displacements at the boundaries arewere propagated into the model.

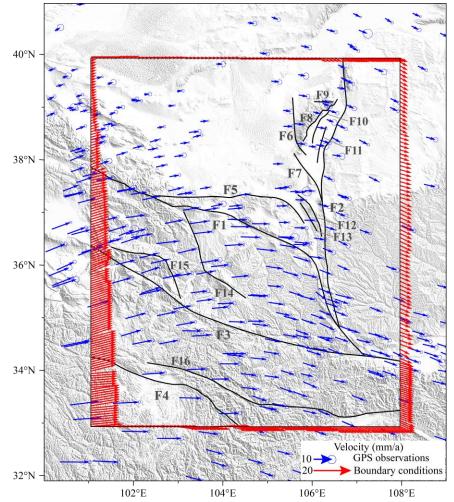


Figure 4. <u>BoundaryModel boundary</u> conditions of the model.. The blue arrows represent the GPS observation velocities according to from Wang and Shen (2020). The red arrows at the boundary represent the boundary velocities calculated by the interpolation of the GPS observations. Fault names can be found in Fig. 1.

185 **3 Results**

3.1 Horizontal crustal velocities

The calculated horizontal crustal velocities in the study area are shown in Fig. 5. In terms of the direction, the <u>The</u> western and central parts of the study area <u>are movingmoved</u> in the NEE and near-EW directions, and the eastern part gradually <u>changeschanged</u> in motion toward the SW or SEE directions. Therefore, the study area <u>iswas</u> characterized by clockwise crustal motions. In terms of the movement rate, the <u>The</u> model <u>showsshowed</u> that the rates in the southwestern part of the study area <u>arewere</u> high, whereas they <u>arewere</u> low in the <u>northeastern part.northeast.</u> The movement rates of the Alxa Block in the north and Ordos Block in the east <u>arewere</u> as low as ~4–6 mm/a. The Bayan Har Block in the south <u>hashad</u> the highest movement rate <u>up toat</u> 13–14 mm/a. For<u>Both</u> the Qaidam Block and the Qilian Block, both of them exhibit <u>exhibited</u> a higher movement rate in the west than that in the east, decreasing from

195 12 to 9 and from 10 to 8, respectively.

In addition, Fig. 5 also shows that large strike-slip faults accommodate velocity gradients between adjacent blocks. For example, the modeled velocity map can be divided in several parts by the F1, F3, and F4 block boundary faults, across which the movement rates of the crust change remarkably, especially at the F1-fault F1. The movement rate on the southern side of the Qilian Block iswas 9–11 mm/a, whereas that on the northern side of the Alxa Block iswas 4–6 mm/a. A different rate of \geq 3 mm/a between the two blocks iswas accommodated by the F1-fault.

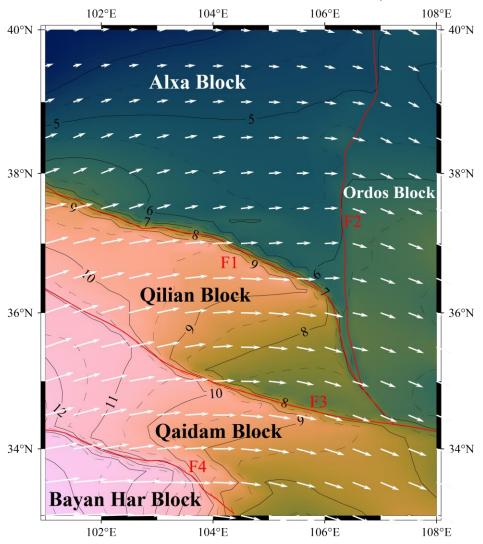


Figure 5. Distribution of modeled crustal surface velocities of the NETP with a grid interval of 0.5° both in longitude and latitude. White arrows represent the crust movement direction. The background color contours represent the magnitude of the velocity in mm/a. The red lines represent the faults implemented in the model. The names are defined in Fig. 1.

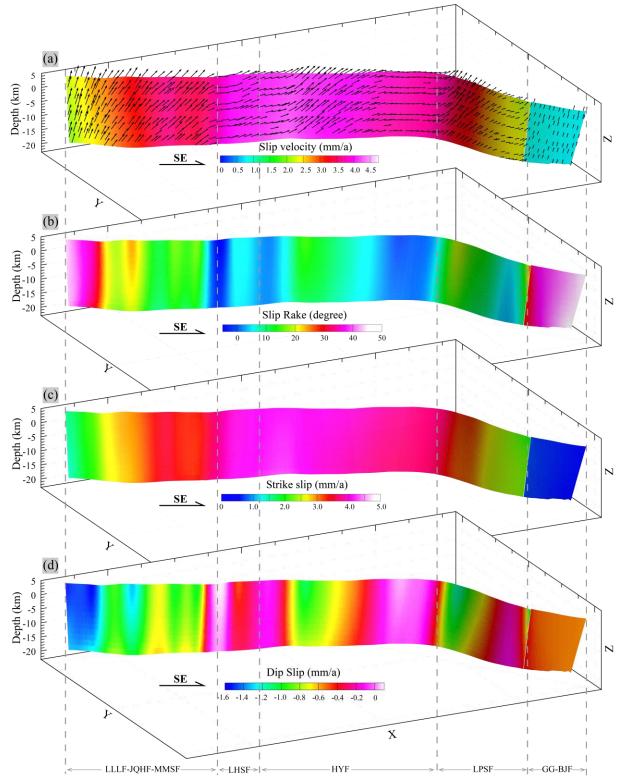


Figure 6. Distribution of the modeled fault slip rates on the F1-fault F1. View from NW to SE. The ratio of the vertical to horizontal scale is 4:1. (a) Total slip rates with slip directions (black arrows). Parts of the fault hashave an oblique-slip component. (b) Slip rake. Positive values indicate that the fault'sfault movement has a thrust component. (c) Slip rates along the fault's strike. Positive values represent sinistral strike-slip. (d) Slip rates along the fault's dip direction. Negative values represent thrust faulting.

3.2 Fault slip rates of the main faults

The dominant depth range of seismic activities in the study area is 5–15 km, with a few events at depths up to 20 km (Li et al., 2020; Y. Li et al., 2021). As mentioned in the introduction, seismic activities are closely related to fault activities. In order toTo assess the seismic hazard reasonably on the faults in the NETP, we focused on the fault kinematics in the brittle crust and extracted the kinematic characteristics up to a depth of 20 km for the main faults from our 3D geomechanicsgeomechanical model. The extracted kinematic characteristics are described below.

3.2.1 Slip rate of the F1 fault

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From west to east, the F1 fault comprises consists of the Lenglongling, Jingianghe, Maomaoshan, Laohushan, Haiyuan, Liupanshan, and Guguan–Baoji faults (Fig. 1). Two earthquakes with magnitudes $M \ge 8.0$ have occurred along this 220 fault-the 1920 M 8.0 Haiyuan Earthquake and 1927 M 8.0 Gulang Earthquake, which formed 220 and 120 km long surface rupture zones, respectively (Guo et al., 2020; Liu-Zeng et al., 2015; Zhang et al., 1987). The kinematic state of the F1 fault-was extracted from the 3D geomechanicsgeomechanical model, as shown in Fig. 6. On the western partsegment of the F1 fault (Lenglongling, Jingianghe, and Maomaoshan faults), the slip rates increased from 2.0 to 4.0 mm/a from west to east and continuecontinued to increase further east (Laohushan Fault and western 225 partsegment of the Haiyuan Fault) up toreaching a maximum of 4.5 mm/a. The slip rates of the F1 fault decreased in the middle of the Haiyuan Fault. The eastern partsegment of the Haiyuan Fault hashad a slip rate of ~3.5 mm/a. The slip rate of the Liupanshan Fault decreases decreased in the SE direction and bottoms out at, with a minimum of ~2.0 mm/a; on the Guguan–Baoji Fault, the slip rate iswas lower than 1 mm/a (Fig. 6a). The slip rates obtained by our 3D geomechanicsgeomechanical model for the Haiyuan Fault arewere much lower than earlier 230 estimates (8.0–12 mm/a; Burchfiel et al., 1991; Lasserre et al., 1999; Zhang et al., 1988) but similar to more recent estimates (3.2-4.5 mm/a; Li et al., 2009; Matrau et al., 2019; Y. Li et al., 2017). The disagreements with earlier

Although the F1-fault is predominantly a left-lateral strike-slip fault, it also has a thrust component (Fig. 6b). The Lenglongling, Jinqianghe, Maomaoshan, middle Haiyuan, and Liupanshan faults have the rakedisplayed rakes ranging
from 10° to 20°, whereas the Guguan–Baoji Fault has thehad a rake varying from 40° to 50°, indicating that they are oblique thrust faults. The Laohushan and western and eastern Haiyuan faults have rakehad rakes below 10°, showing that left-lateral strike-slip faulting is dominant at these faults. Figures 6c and 6d show the continuous slip rates of the F1-fault along its strike and dip, respectively. The slip rates along the strike (Fig. 6c) are likewere similar to the total slip rates (Fig. 6a). The Laohushan and Haiyuan faults havehad the highest slip rates on the F1-fault. Conversely, the Lenglongling, Jinqianghe, Maomaoshan, and Liupanshan faults havehad high dip-slip rates.

geological estimates may be related to the time scale and the extent to which faults have been studied (Li et al., 2009).

3.2.2 Slip rate of the F2-fault

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The F2 fault <u>comprises_consists of</u> the Zhuozishan, Huanghe, Luoshan, and Yunwushan–Xiaoguanshan faults (Fig. 1). Figure 7 shows that right-lateral strike-slip faulting is prevalent across the entire F2 fault. However, the magnitude of the dip-slip component <u>varies_varied</u> from one location to another. The Zhuozishan Fault is an oblique-slip reverse fault with slip rates ranging from 0.8 to 1.6 mm/a. The Huanghe Fault <u>hashad</u> a slip rate of 1.6–2.6 mm/a. Its northern

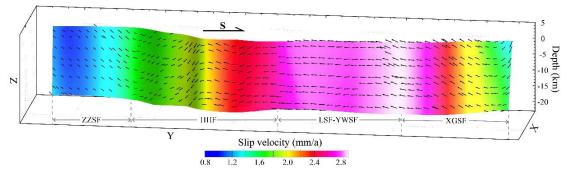
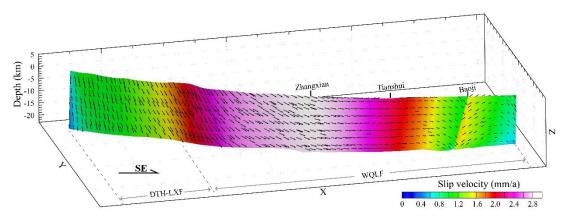


Figure 7. Distribution of the modeled fault slip rates on the F2-fault. View from west to east. The black arrows represent the slip directions. The ratio of the vertical to horizontal scale is 4:1.



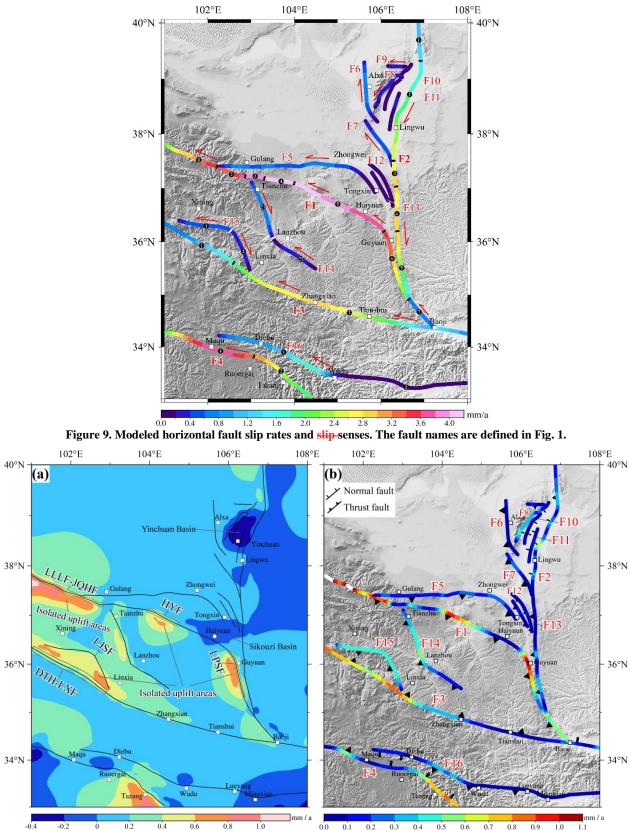
250 Figure 8. Distribution of the modeled fault slip rates on the F3-fault. View from SW to NE. The black arrows represent the slip directions. The ratio of the vertical to horizontal scale is 4:1.

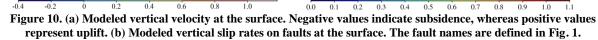
segment is an oblique-slip normal fault, whereas its southern segment hasdisplayed almost no dip-slip component. The Luoshan and Yunwushan faults havehad slip rates ranging from 2.6 to 3.0 mm/a and are dominated by right-lateral strike-slip faulting. The Xiaoguanshan Fault is an oblique-slip reverse fault with slip rates ranging from 3.0 mm/a (northern end) to 1.4 mm/a (southern end).

3.2.3 Slip rate of the F3-fault

The F3-fault includes the Daotanghe–Linxia and West Qinling faults (Fig. 1) and is mainlyprimarily a left-lateral strike-slip fault, as shown in Fig. 8. The western Daotanghe–Linxia Fault is an oblique-slip reverse fault, which
 haswith slip rates ranging from 0.8 to 1.8 mm/a. The West Qinling Fault hashad slip rates varying from 1.8 to 2.8 mm/a, but each segment of this fault hasexhibited slightly different kinematics. The West Qinling Fault is an oblique-slip reverse fault west of Zhangxian, but is dominated by left-lateral strike-slip faulting in the Zhangxian–Tianshui–Baoji region. The West Qinling Fault becomes an oblique-slip normal fault only in the vicinity of near Baoji.

The kinematics of other faults in the study area are not described in this study. Their horizontal velocities are listed in Fig. 9.





3.3 Vertical velocities

275

Figure 10a shows the distribution of vertical velocities in the study area. In our model, surface subsidence can bewas observed only in the Yinchuan Basin west of Huanghe Fault, in the Ordos basin in the east, and in the Sikouzi Basin in the southern Ningxia arc tectonic belt. Most of the subsidence rates rangeranged between 0 and 0.2 mm/a, except in the center of the Yinchuan Basin, which exhibits exhibited subsidence rates varying from 0.2 to 0.4 mm/a. Based on paleomagnetic studies, the Sikouzi Basin had a subsidence rate of 0.22 mm/a during the Pliocene (Wang et al., 2011), whereas the subsidence rate of the Yinchuan Basin has been 0.32 mm/a since the Middle Pleistocene (Ma et al., 2021). Both values are consistent with those derived from our simulation.

Most other parts of the study area exhibit upliftingexhibited uplift, albeit at low rates (generally less than 0.2 mm/a). 280 Most areas with high uplift rates (0.8–1.0 mm/a) arewere in the Qilian Block, such as the Lenglinglong Fault and Jinqianghe FaultFaults, the southern side of the middle Haiyuan Fault, the western side of the Liupanshan segment, and the southern side of the Lajishan Fault (Fig. 10a). High vertical fault slip rates also appearappeared on the F1 and F3 thrust faults that form the north and south boundaries of the Qilian Block (Fig. 10b). These high vertical fault slip rates are inferredwere thought to be caused by the compression from the NE expansion of the TP and SW 285 subducting subduction of the Alxa Block (Ye et al., 2015). Therefore, outward thrust stacking occurs on the southern and northern boundaries (F1 and F3-faults) of the Qilian Block.

4 Discussion

4.1 Comparison with previous results

290

The boundary conditions of our model were derived from the GPS data of Wang and Shen (2020). Figure 11 shows a comparison of the results of our model with the GPS data. The modeled velocity field is consistent in both direction and magnitude with the GPS-derived velocity field. In order to To further examine the fit between the model results and GPS data, we selected a NE-SW profile that crosses through the study area (Fig. 11, C-C') and projected all GPSobserved values within 50 km of both sides of the profile. Figure 12 shows that the modeled and observed values on either end of the profile (i.e., locations close to the model's boundaries) are almost identical. Although there were 295 differences between the modeled and GPS-observed values, the differences were within the margin of error for the GPS data. Therefore, based on comparisons between the modeled and GPS-observed values in the map and profile, our modeled kinematics agreesagree well with the GPS data.

300

Table 3 is a comparison of the modeled slip rates and model-independent geological slip rates compiled from previous studies. From the comparison, we can see that our modeled results are generally were consistent with the slip rates obtained by geologic approaches. For example, the modeled horizontal slip rates on the F1-fault (e.g., the Laohushan, Haiyuan, and Liupanshan faults) arewere similar to the geological slip rates obtained by previous pointwise measurements (Table 3). The modeled slip rates on the F2-3 Luoshan Fault (2.6–3.0 mm/a) are in lineagreed with the geological slip rate (2.2 mm/a). A good agreement between these two kinds of slip rates also exists existed on the West Qinling Fault in the Zhangxian and Tianshui region (Table 3).

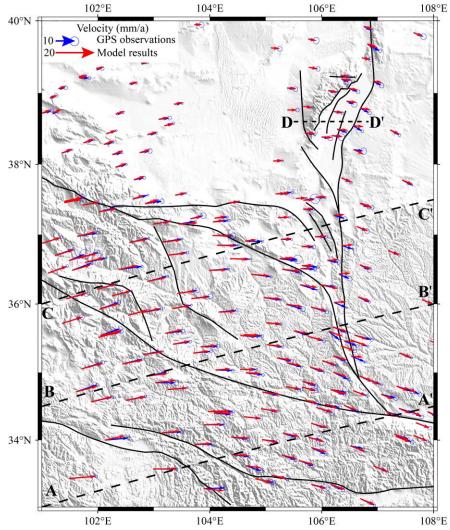


Figure 11. Comparison of the modeled horizontal velocities and GPS velocities. The red arrows represent the modeled results_a and the blue arrows are the GPS measurements (Wang and Shen, 2020). The dashed line is the location of the profile in Fig. 12 and Fig. 14.

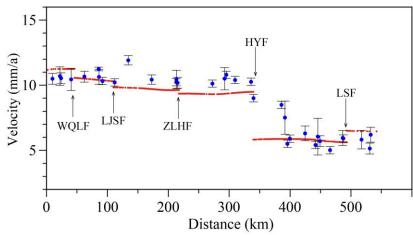


Figure 12. Comparison of the modeled horizontal velocities and GPS velocities along the C-C' profile in Fig. 11. The red points are model data, and blue circles indicate GPS measurements. The fault names are defined in Fig. 1.

Fault name		Modeled ra	te (mm/a)	Geological	rate (mm/a)	- References
		Lateral ^a	Vertical ^b	Lateral ^a	Vertical ^b	- References
F1-1	LLLF	2.8-3.6	0.6–1.3	3.9	0.38	He et al., 2000, 2010
F1-2	JQHF	3.2–3.8	0.7 - 1.0	4.4	/	He et al., 2000
F1-3	MMSF	3.8–4.0	/	3.7	/	He et al., 2000
F1-4	LHSF	4.0-4.2	/	4.0	/	Liu et al., 2018
F1-5	HYF	3.6–4.2	0.2 - 1.0	3.2–4.5	/	Li et al., 2009; Matrau et al., 2019
F1-6	LPSF	2.0-3.6	0.2–1.1	0.7–3.0	0.2–0.9	Wang, 2018; Wang et al., 2021;
F1-7	GG-BJF	0.6–0.8	0.5–0.6	/	/	/
F2-1	ZZSF	- (1.2–1.4)	0.2–0.3	/	/	/
F2-2	HHF	- (1.6–2.6)	0–0.7	/	0.04–0.24	Lei et al., 2014
F2-3	LSF	- (2.6–3.0)	/	- 2.2	/	Min et al., 2003
F2-4	YWSF	- (2.6–3.0)	/	/	/	/
F2-5	XGSF	- (1.4–3.0)	0-0.4	/	/	/
F3-1	DTH-LXF	0.8–1.8	0.5–0.8	/	/	/
F3-2	WQLF	2.0-3.0	0.1–0.9	2.5-2.9	/	Chen et al., 2019
F4-1	EKLF	3.2–3.8	0–0.5	4.9	0.25	Li, 2009
F4-2	TZF	2.2-3.2	0.3–0.7	1.4–3.2	0.1–0.3	Ren et al., 2013
F5	TJSF	0–0.8	0.1–0.3	0.77–0.96	0.1–0.2	X. Li et al., 2017, 2019; Zhang et al., 2015
F6	WHLSF	- (0.6–0.8)	0-0.2	- 0.28	0.11	Lei, 2016
F7	NSSF	- (0.4–0.6)	0–0.3	- 0.35	0.10	Lei, 2016
F8	EHLSF	0.2–0.4	0.1–0.5	/	0.88	Lei et al., 2016
F9	ZYGF	0.2–0.4	0-0.2	/	/	/
F10	LHTF	/	0-0.1	/	0.18	Lei et al., 2011
F11	YCF	/	0-0.2	/	0.14	Lei et al., 2008
F12	QSHF	/	0–0.2	/	/	/
F13	YTSF	/	0–0.2	/	/	/
F14-1	ZLHF	- (0.6–0.8)	0.2–0.6	/	0.12-0.51	Hou et al., 1999
F14-2	MXSF	0.2–0.4	0.1–0.4	0.5-1.72	/	Song et al., 2006
F15-1	WLJSF	0.4–0.6	0.4–0.5	/	/	/
F15-2	ELJSF	- (0.2–0.4)	0.3–0.5	/	/	/
F16-1 F16-2	DB-BLJF WD-KXF	0.8–1.8 0–0.2	0.1–0.4 0-0.1	1.3 1.0	0.39	Liu et al., 2015 Zheng et al., 2016a

Table 3. Comparison of model slip rates with geological slip rates

^a Positive value indicates left-lateral slip rate. ^b Fault attributes are shown in Fig. 10b

4.2 Fault slip rates and seismic hazards

315 4.2.1 Tianzhu Seismic Gap

The M 8.0 Gulang earthquake occurred in 1927 inalong the northwestern partsegment of the F1-fault, whereas the M 8.0 Haiyuan earthquake occurred in 1920 on the Haiyuan Fault (Fig. 1). The Jinqianghe, Maomaoshan, and Laohushan faults, which are in the region between the locations of these two strong earthquakes, unruptured in the two earthquakes, are collectively known as the Tianzhu Seismic Gap (TSG, Guo et al., 2019; Li et al., 2016; Fig. 13a). 320 Based on the simulation, the left-lateral strike-slip rates of the Jingianghe, Maomaoshan, and Laohushan faults were 3.2–3.8, 3.8–4.0, and 4.0–4.2 mm/a, respectively (Table 2, Fig. 13a). Therefore, all three faults have relatively high slip rates compared with the rest of the study area. Based on the slip rates and other fault data, we estimated the earthquake magnitude based on the energy accumulated during the time elapsed from the previous event (Purcaru et al., 1978) and recurrence intervals (Shen et al., 2009), as shown in Table 4. The Jinqianghe, Maomaoshan, and 325 Laohushan faults can generate $M_87.1$, $M_87.3$, and $M_86.6$ earthquakes, with recurrence intervals of 424, 571, and 1910 years, respectively. It has been reported that A total of 675 and 952 years have elapsed since the last timerupture along the Jingianghe and Maomaoshan faults-ruptured (Gan et al., 2002; Table 4). Therefore, the likelihood of reactivation along these two faults will reactivate is high. For the Laohushan Fault, it is believed that the most recent earthquake with surface ruptures wasis thought to be the 1888 M 6.25 Jingtai earthquake. Because only 133 years have elapsed 330 since this event, the seismic hazard of this fault in the near future is low. Although several researchers suggested that the TSG could be ruptured thoroughly by a $M \ge 8.0$ earthquake with a recurrence interval of 1000 years (Chen, 2014) and the elapsed time from the last M 8.0 earthquake may be elosedclose to the recurrence interval (Liu et al., 2018), further work is needed to verify this assumption, especially on the stress state of the faults. Nevertheless, our results together with the previous studies suggest that the seismic hazard caused by a large earthquake in the TSG is high in 335 the next few decades, and careful earthquake monitoring should be conducted in this area.

4.2.2 Seismic gap at the southern Liupanshan and Guguan-Baoji faults

The Liupanshan and Guguan–Baoji faults are jointly affected by three interacting blocks with contrasting velocity fields (Fig. 13b). First, the SE movement of the Qilian Block horizontally compresses this region against the stable Ordos Block to the east and causes strong thrusting motion (Fig. 6a). Second, the Liupanshan Fault zone, which is adjacent to the SE end of the Haiyuan Fault, accommodates the shortening caused by the left-lateral strike-slip motion of the Haiyuan Fault. Third, our modeled results showshowed that the Yunwushan–Xiaoguanshan Fault has a significant right-lateral strike-slip component (Fig. 7), which contributes to the accumulation of right-lateral shear strain in the Liupanshan and Guguan–Baoji fault zones (Du et al., 2018). Based on the analysis of the velocity field in the region, the Liupanshan and Guguan–Baoji faults are <u>a</u> prime location for elastic strain accumulation. The distribution of the velocities of the faults are also indicative of stress accumulation in this region (Fig. 7). The northern segment of the Liupanshan Fault hashad slip rates of 3.2–3.6 mm/a, which dramatically decreased to 2.5 mm/a in the middle and southern segments of the fault. In addition, the slip rate of the Guguan–Baoji Fault iswas only 0.7 mm/a. The northern part of the Yunwushan-Xiaoguanshan Fault hashad slip rates of 2.8–3.0 mm/a, which decreased to 1.5 mm/a in the southern partsegment (Fig. 13b). These changes in the slip rate indicate that the

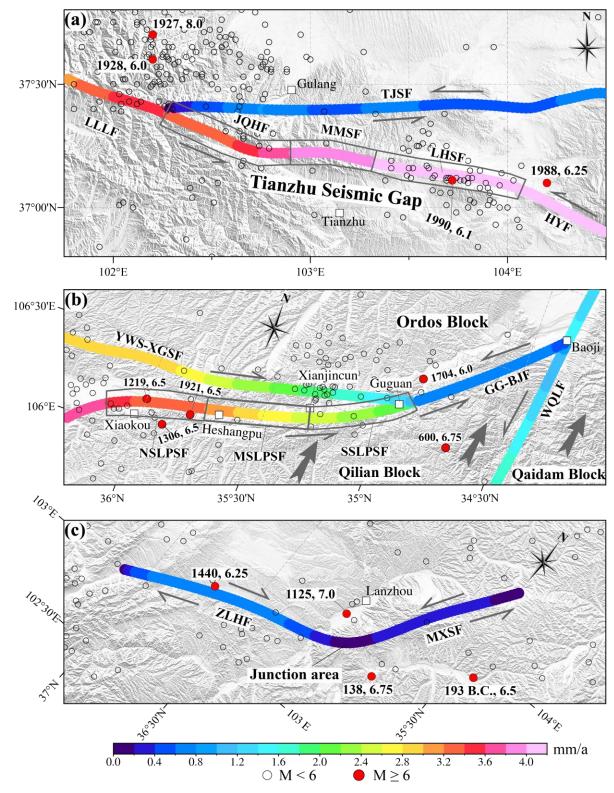


Figure 13. Modeled horizontal fault slip rates and distribution of historical earthquakes in (a) the Tianzhu Seismic Gap, (b) the intersection area of the Liupanshan, Guguan–Baoji, and Yunwushan–Xiaoguanshan faults and (c) the junction area of the Maxianshan and Zhuanglanghe faults. The gray arrows in (b) represent the movements of the Qilian and Qaidam blocks and NSLPSF, MSLPSF, and SSLPSF are the northern, middle, and southern segments of the Liupanshan Fault, respectively.

_during the elapsed time since the last remarkablesignificant earthquake										
Fault name	V ₁ (mm/a)	V ₂ (mm/a)	$L_1(km)$	$L_2(km)$	μ (Gpa)	t	S (m)	Ms	T (a)	
JQHF	3.5	/	34	20	34.5	675	1.5	7.1	424	
MMSF	3.9	/	51	20	34.5	952	2.2	7.3	571	
LHSF	4.1	2.5	70	20	34.5	133	3.1	6.6	1910	
MSLPSF, SSLPSF	2.5	/	80	23	34.5	570	3.5	7.2	1397	
GG-BJF	0.7	/	70	23	34.5	1400	3.1	7.1	4365	

Table 4. Earthquake magnitude and recurrence interval of each fault based on the energy accumulated

 V_1 is the modeled average slip rate of the fault in this study; V_2 is the aseismic creep rate of the fault (Y. Li, et al., 2021); L_1 is the length of the fault (Xu et al., 2016); L_2 is the depth of the seismogenic, which refers to the locking depth (Y. Li, et al., 2017, 2021); μ is the shear modulus of the rocks (Aki et al., 2002); t is the time that has elapsed since the most recent remarkable earthquake (Gan et al., 2002; Shi et al., 2013, 2014; Wang et al., 2001); S is the largest maximum coseismic displacement, calculated using the method of Gan et al. (2002); M_s is the earthquake magnitude corresponding to the energy accumulated by the fault between recurrences (Purcaru et al., 1978); and T is the recurrence interval of the fault, where T = S/(V₁-V₂) (Shen et al., 2009). The fault names are defined in Fig. 1 and Fig. 13.

middle-southern segments of the Liupanshan and Guguan-Baoji faults have high slip rate deficits, implying this region accumulates strain. However, in terms of seismic activity, only the northern partsegment of the Liupanshan Fault has a history of major earthquakes, including an M 7 earthquake in 1219, M 6.5 earthquake in 1306, and M 6.5 earthquake in 1921 (Fig. 13b). Earthquakes stronger than M 6.0 have not been recorded in the middle-southern parts of Liupanshan Fault. Their seismic activity mainly manifests as small and sparse earthquakes, and the most recent remarkablesignificant activation was recorded ~570 years ago (Shi et al., 2014). Minor earthquakes related to the Guguan-Baoji Fault are scarce, and the only notable earthquakes that have occurred near this fault arewere an M6.0 earthquake in 1704 and the 600 AD Qinlong M 6.75 earthquake (Shi et al., 2013). It has been estimated that ~1400 Approximately1400 years have elapsed since the last M~7 earthquake.

- 365 BaseBased on the above analysis, we suggest that the southern segments of the Liupanshan and Guguan-Baoji faults are in prime locations for stress/strain accumulation and constitute a seismic gap at the end of the large-scale Haiyuan strike-slip fault zone. Since Because this region has a history of strong earthquakes, it is necessary to assess the seismic hazard and its urgency-in this region. Based on the fault slip rates obtained from our model and fault data in the literature, we estimated that the energy accumulated on the middle-southern Liupanshan and Guguan-Baoji 370 faults during the elapsed time is sufficient to generate M_S 7.2 and M_S 7.1 earthquakes, with recurrence intervals of 1397 and 4365 years, respectively (Table 4). Obviously, the elapsed time on the middle-southern Liupanshan (570 years) and Guguan-Baoji faults (1400 years) (see the column "t" in Table 4) are much shorter than their typical recurrence intervals. Therefore, we inferinferred that the middle-southern Liupanshan fault and the Guguan-Baoji fault are most likely in a state of stress accumulation, and the likelihood of a large earthquake on these fault segments in 375 the next few decades is thought to be low.

360

4.2.3 Maxianshan–Zhanglanghe fault zone

The Maxianshan Fault near Lanzhou city is a large Holocene strike-slip fault with a thrust component-of thrusting and acts as an important earthquake-controlling fault that affects and constrains the seismicity of this region (Yuan et al.,

2003). Different left-lateral strike-slip rates have been reported for this fault—3.73 mm/a (Yuan et al., 2002a), 0.5– 380 1.72 mm/a (Song et al., 2006), and 0.93 mm/a (Liang et al., 2008). These discrepancies in fault slip rate may be attributed to the loess that covers the extension of the fault, which obscures the fault traces in many segments and makes it difficult to track its activity. The modeled results in this study indicate indicated that the left-lateral strike-slip rates of the Maxianshan Fault range from 0.2 to 0.4 mm/a, and that the vertical slip rates vary from 0.1 to 0.4 mm/a (Fig. 13c, Table 3). Therefore, the left-lateral strike-slip rates of the Maxianshan Fault may not be as large as 385 previously thought, but they have a relatively large thrust component. The Zhanglanghe Fault is predominantly a rightlateral strike-slip fault with slip rates ranging from 0.6 to 0.8 mm/a (Fig. 13c, Table 3). These slip rates are significantly greater than the left-lateral strike-slip rates of the Maxianshan Fault. Note that the slip rate on the junction between the Maxianshan fault and Zhuanglanghe faultfaults is almost practically zero. It can be inferred that Thus, the junction area would accumulate high concentrations of stress under the continuous eastward movement of the Oilian Block. 390 SomePrevious studies have suggested that the 1125 Lanzhou M 7.0 earthquake occurred in such a tectonic setting (He et al., 1997; Fig. 13c). Given that the recurrence interval of this region is 2250–3590 years and the last event was only 896 years ago (Liang et al., 2008), the near-term risk of a large earthquake in this region is low. Therefore, we speculate that the junction area of the Maxianshan fault and Zhuanglanghe faultfaults is currently in a state of stress accumulation.

395 4.2.4 Isolated uplift areas and earthquakes

As mentioned above, we considered that earthquakes are less likely to occur on the Laohushan, Liupanshan and Haiyuan faults in the short term from the perspective of owing to the earthquake recurrence cycle and the elapsed time from the previous earthquake. However, the Haiyuan, Liupanshan, Lajishan and Daotanghe-Linxia faults are all located near the isolated rapid uplift areas of the Qilian block (Fig. 10a). Many studies have also found that low-400 velocity bodies are widely distributed in the middle-lower crust of the Qilian block (Bao et al., 2013; Wang et al., 2018; Ye et al., 2016). The spatial coupling of active faults, isolated uplift areas, and low-velocity bodies is highly similar to the seismogenic conditions elaborated by the "seismic source cavity" model recently proposed by Zeng et al. (2021). That is, during the rapid uplift of the isolated areas (Fig. 10a), the low-velocity bodies in the middle-lower crust easily intruded into the weak space of the crust under the action of differential pressure to form a "seismic source 405 cavity". If the isolated uplift areas keepcontinue to rise, the "seismic source cavity" may rise to the shallow part of the crust to intersect with brittle faults, causing strong earthquakes (Yang et al., 2009; Zeng et al., 2021). Therefore, in addition to the Jingianghe and Maomaoshan faults mentioned above, the Haiyuan-fault, Liupanshan-fault, Lajishan fault, and the Daotanghe-Linxia fault faults also have favorable structural conditions for strong earthquakes although some a number of areas have not experienced events in recorded history.

410 **4.3 Implication for deformation mechanism of NETP**

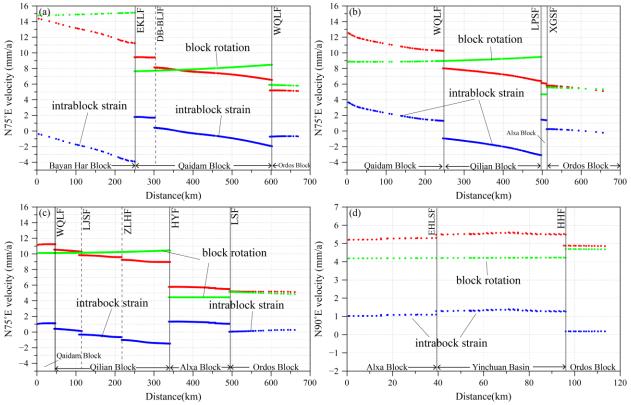
The deformation of NETP is the result of the combined action of block rotation, faulting, and the-intrablock strainingstrain (Meade and Loveless, 2009). We analyzed four velocity profiles to compare the contributions of block rotation, faulting, and intrablock strainingstrain to determine the total deformation of NETP (Fig. 14). It is noted that

the<u>The</u> rigid displacements caused by block rotation were calculated according to the Euler pole locations and rotation rates with respect to the <u>EurasiaEurasian</u> plate (Wang et al., 2017; Y. Li et al., 2022), as shown in Fig. 14 a–d. The velocity gradient caused by block rotation <u>accountsaccounted</u> for more than 80% of that on the profiles. Obviously, the block rotation should be the primary mechanism for the deformation of the NETP, which is similar to the southeastern Tibet (Z. Zhang et al., 2013). However, the intrablock <u>strainingstrain</u> of <u>the</u> Bayan Har and Qaidam blocks <u>contributecontributed</u> approximately 4 mm/a and 3 mm/a shortening in profiles of AA'₇ and BB' (Fig. 14a–b).

420 The Qilian block also hasexhibited a contribution of 2 mm/a shortening in profile BB' but decreasesdecreased to about approximately 1mm/a in profile CC' (Fig. 14b-c). Therefore, the intrablock strainingstrain is still significant for regional deformation. The boundary faults of the blocks, such as the East Kunlun-fault, Haiyuan-fault, and West Qinling faultfaults, also play an important role in regulating the deformation differences between blocks.

425

The D–D' profile shows that the tectonic deformations of the Yinchuan Basin structural belt slightly differ from those in other profiles. The NE expansion of the TP leads to near-N–S compression on the Yinchuan Basin (Yang, 2018), which causes it to move eastwards faster than the Alxa Block. This manifests as an eastward extension in the Yinchuan Basin. The crustal deformations caused by this process are accommodated by the right-lateral strike-slip of Huanghe Fault (Fig. 14d).



430 Figure 14. Modeled velocity profiles across the study area with <u>profile</u> orientation-<u>of profiles</u>. The profiles in (a)–(d) correspond to the AA', BB', CC', and DD' in Fig. 11, respectively. The red dots indicate the components along the profiles of the node motion velocity within 2 km on both sides of the profile. The green dots represent the velocity component along the profiles due to plate rotation. The blue dots indicate the differences between the red and green dots. Fault names are defined in Fig. 1.

435 **5** Conclusions

In this study, a detailed 3D geomechanical model of the NETP was constructed based on geophysical, geodetic, and geological data. This model accountsaccounted for 3D fault geometries, variational rock properties, a reasonable initial crustal stress, and gravity. Special attention has been paidgiven to the evaluation of fault friction coefficients and initial stress to ensure that the model is consistent with the real-geological conditions as much as possible. After thatIn

440 <u>addition</u>, we extracted particular data from the model and obtained the horizontal and vertical crustal velocities of the study area as well as the horizontal and vertical slip rates of the major faults. The results <u>can be mutually confirmedare</u> <u>consistent</u> with the conclusions obtained by geodesy, geology, paleomagnetism, etc.

Based on the analysis of the kinematics of major faults, we suggest that the Jinqianghe–Maomaoshan Fault will probably causelikely experience a M_S 7.1–7.3 earthquake in the following decades dueowing to its relatively high slip rates with an elapsed time close to the recurrence interval. In contrast, the Laohushan and middle–southern Liupanshan faults, as well as the Guguan–Baoji and the junction area–of the Maxianshan and Zhuanglanghe faults, are inferredthought to have a low seismic hazard in the near future on account of theirowing to the very short elapsed time since the last significant event, although stress is easily accumulated in these areas. The model also provided information on the deformation mechanism of the NETP. Because of velocity differences between the opposing sides

450 of the Haiyuan, West Qinling, and East Kunlun faults, as well as the relative stability of the Alxa and Ordos blocks, the NE expansion of the TP has caused the fault-separated Qilian, Qaidam, and Bayan Har blocks to extrude in the SEE direction and rotate in the clockwise direction. The block rotation is the primary mechanism for the deformation of the NETP even though the intrablock strainingstrain and faulting are non-negligible.

Data Availability

The GPS data displayed in Fig. 4 and Fig. 11 are available through Wang and Shen (2020). The fault traces were obtained from Xu et al. (2016). The CRUST1.0 was obtained from Laske et al. (2013).

Author contribution

LL and XL contributed to the model building. LL <u>carried outconducted</u> the analysis, wrote the paper, and prepared the figures. FY, LP₂ and JT reviewed and edited the paper.

460 **Competing interests**

The authors have no competing interests to declare.

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